

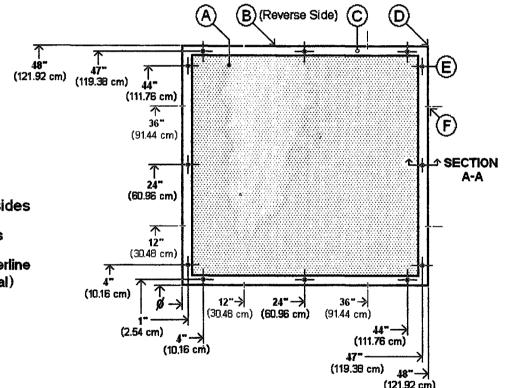


## All Weather Sound Panel 4' x 4'

- A Front Face: Perforated
  .040" 5052-H32 aluminum alloy
  3/32" holes staggered 5/32" OC
- B Back Face: Solid .032" 5052-H32 aluminum alloy
- Frame:
  .125" 6063-T5 aluminum alloy
  Custom C-channel extrusion
  Rotary sanded machine finish
- D Welded at all corners; front, back & sides
- (E) (12) 3/8" dia. reinforced mounting points
- F 3/16" Drain holes are located along centerline of all 4 sides Marked In Red (8 total)

Gross Weight: aprox. 45 lbs.

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Section A-A								
0.125" → <b>(</b> 0.375" dia i.D.								
C-channel Perf. Alum. sheet Core Material								
Acoustiblok								
Solid Alum. sheet								
ACOUSTIBLOK Inc. REV. B 6900 Interbay Blvd. Tampa. Fl. 33616 © LJ Avaion LLC 2009								
Part name: 4' × 4' Industrial Panel								
Part Number: AWSPIND44 ©								
For: Specifications for customer's review								
Drn by: V. Miko Date: 12.17.2009								
Chk by: Date:								
Appr. by: Date:								
SPECIFICATIONS SUBJECT TO CHANGE WITHOUT NOTICE								

B1303994 40 151979 Aug

CFFICE COPY
CITY OF MIAMI BEACH
APPROVED FOR PERMIT BY
THE FOLLOWING:

BUILDING:

ZONING: DRB/HPB:

CONCURRENCY:

PLUMBING:

ELECTRICAL:

MECHANICAL:

FIRE PREVENTION:

ENGINEERING:

PUBLIC WORKS:

STRUCTURAL: ELEVATOR.

100

M. SCHAD 5.8.13 5/8/13

96413

City or winding of the party of



## NOTICE TO THE CITY OF MIAMI BEACH BUILDING DEPARTMENT OF EMPLOYMENT AS SPECIAL INSPECTOR UNDER THE FLORIDA BUILDING CODE

			Standard Hotel	to perform special inspecto	r services under the
Florid	da Building (	Code at tl	he 40 Island Aven	ue project on the below lis	ted structures as of
				ineer licensed in the State of Florida.	
Proce	ess Number:	RI	306508	Master Permit (มีผู้APPLICABLE):	•
_	oo mambon	<u> </u>	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	emit there may all	
O	Spec	cial Inspect	or for Pilings, FBC 18	1 This that may be lover is	•
0	Spec	cial Inspect	or for Lightwelling	washing Coattiell FBC 1917.2	
0	Spec	ial (nspect	af for Soil of magetto	HE ES 4820.3.1	••••
0	NSpec	ial Inspect	or for Precast Unities	nd Auschments FBC 1927.12.2 (By P.E. or	R.A)••••
<b>⊗</b> k	Spec	cial inspect	or for Reinforced Mas	SERPON FBC 2422.4 (By.P.E or R.A)	
8	ijii i Spec	υ <i>πότη υ</i> ishecti	ion for Steel Bolted &	Master Permit (IF APPLICABLE):  This permit there found in that may be found in the found in the found in that is a found in the fo	or R.A)
	Cnob	C/2	or for Tricons avorish	5 feet long or 6 feet high, FBC 2319.17.2.4.2	/By DE or D A \
0					(Dy 1 .L. 01 13. A)
Ø	Spec	cial Inspect	or for <u>Con</u>	CRETE REPAIRS	· · · · · · · · · · · · · · · · · · ·
	E: Only the n				
The f	ollowing indivi	dual's emp	oloyed by this firm or n	me are authorized representatives to perform	inspections
1.	Youssef H	achem, P	h.D., P.E., S.I.	2.	
3.		·1		4.	
	-				
* Spec	ial inspectors util	izing authoriz	ed representatives shall in	sure the authorized representative is qualified by educa shall include: licensure as a professional engineer or a	ation or licensure to perform
engine	ering education p	orogram in ci	ispector. The qualifications il or structural engineering	; graduation from a rchitectural education program; s	uccessful completion of the
NCEE	S Fundamentals I	Examination;	or registration as a building	g inspector or general contractor.	
I will n	) otify the City of M	iami Beach E	Building Department of any	changes regarding authorized personnel performing ins	pection services.
				7	
i, under	stant that all mand	latory inspect	ons, as required by the Flori	ida Building Code shall be requested by the permit holder	and approved by the Building
De partu Bulling	o Department AS	pecial Inspect	ion Log for each building mus	pector hired by the Owner are in addition to the mandatory at be displayed in a convenient location on the site for inspect	on by the Building Department
Gg Peor	Is/dEnther woon	Completion of	the work under each building	permit, I will submit to the Building Department at the time o lge, belief and projessional judgment those portions outlined abo	final inspection the completed
Opplikting	Code and are in su	psequent acco	ordance with the approved plans	s.	to most the ment of the Florida
· /	10.43302	^			
	TE OF	上 Arch	itect/Engineer Signature:		
3//	SIAILO	<b>#</b>	Architect/Engineer	Value of Hasham Dh.D. D.E. C.I.	
<i>9</i> \$\$••	FUORID!		Name Printed:	Youssef Hachem, Ph.D., P.E., S.I. 12151 SW 128 Court, Suite 104, N	/iami El 22106
1,55	SIMMALE	1112	Address:		ilalili, FL. 33160
DE A	neolana Sealed 3 MM Met co	• 985061	Phone Number:	(305) 969-9423 / (786) 287-9120	
PE 43	cense Number		Owner/Agent Signature:	Certa Poliah	
		Ow	mer/Agent Name Printed: Building Department	cera - or an	
Date:	10/25/2013	3_	Accepted By:	N 2/12/14	<del></del>



#### **BUILDING DEPARTMENT**

1700 Convention Center Drive, 2<sup>nd</sup> Floor Miami Beach, FI, 33139 Phone: (305) 673-7610 Fax: (305) 673-7857

## Owner/ Qualifier / Contractor Estimate Construction Cost Affidavit (To be submitted for the main/master permits or the stand alone permits)

		•			
Permit Number: <u>B1306508</u>	Date: 10/08/2013				
Job Address: 40 ISLAND AVENUE	Folio No.: 02-32	233-004-0090			
•	· · · · · · · · · · · · · · · · · · ·				
The construction cost should include the work (	under the main Permit and all as	sociated permits.			
		••••			
Part I: FEMA 50% Related Construction Cost					
Items to be excluded from Estimate Construction Cost	st for Part I (FEMA 50% Related Cor	estruction Cost):			
Plan and Specification, Survey Cost, Permit Fees, Swimi	ming Pools, detached structures (gara				
Landscaping, Fences, Yard light , Not Built-ins Appliance Estimated Construction Cost	General Contractor Cost	Owner Cost			
Estimated Construction Cost	General Contractor Cost	Owner Cost			
Demolition & Removal	2,000				
Building & Structural Elements	20,000				
Roofing					
Doors & Windows	2,500				
Railing					
Interior Finish, Floor Covering, Painting	3,000				
Cabinets and Furniture-Built-Ins					
Appliances-Built-Ins					
Other Building related Items	2,000				
Electrical including Fixtures	4,000				
Elevator					
Mechanical-HVAC-equipments	5,500				
Plumbing including Fixtures	12,000				
Overhead and Profit	10,000	· ·			
Sub Total Construction Cost	\$ 61,000	\$			
Sub Total Construction Cost Estimate for	61	,000 -			
FEMA 50% Rule Purposes		,000			



#### **BUILDING DEPARTMENT**

1700 Convention Center Drive, 2<sup>nd</sup> Floor Miami Beach, FI, 33139

Phone: (305) 673-7610 Fax: (305) 673-7857

Estimated Construction Cost	General Contractor Cost	Owner Cost	•••
Swimming Pools		,	•
Fences, Pavers, Sidewalks, Site Improvements			•
Yard Light			
Other and detached: garages, storage and cabanas			•
Sub Total Cost	\$	\$	
Sub Total Construction Cost Estimate for non FEMA 50% Rule Purposes	\$		



Part III: Total Construction Cost (Note: The cons	truction cost will be	e validated by Plan Examiners)
Estimated Construction Cost		
Sub Total Construction Cost Estimate for FEMA 50% Rule Purposes-Part I	\$	61,000 2
Sub Total Construction Cost Estimate for Non FEMA 50% Rule Purposes- Part II	\$	1
Total Construction Cost Estimate. (Add Part I and Part II of Construction Cost)	\$	61,000 =

	and Part II of Construction Cost) \$ (\(\rho \lambda  \text{U} \text{U} \)
	Part IV: Signature Required
	If the improvements of will increase at any point during the proposed construction, It is Owner and the Contractor of
	Record responsibility to submit the revised improvements cost to the Building Department for review and approval.
$\subset$	Signature of Owner
	STATE OF FLORIDA
	COUNTY OF DAGE
	Sworn to and Subscribed before me this 10 day of February 2014, by:
bs	erepe'tena
	Personally known [] Produced Identification - Type of Commission # DD 968336
	LXPITES March 7, 2014
	Identification Bonded Thru Tray Fair Insurance 800-395 7019
	A
	Signature of Motar Public
	Page 2 of 3



#### **BUILDING DEPARTMENT**

1700 Convention Center Drive, 2<sup>nd</sup> Floor Miami Beach, FI, 33139

Phone: (305) 673-7610 Fax: (305) 673-7857

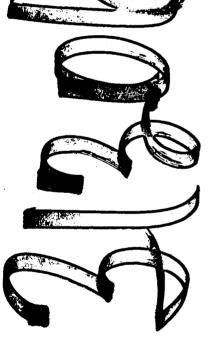
		••••
		_
Sign	ature of Qualifier / Contractor	
		•
	TE OF FLORIDA NTY OF <u>Miami</u> — Dode	
ı		
Swoi	n to and Subscribed before me this 5	day of February 2014, by:
ىـــ	tan Hayes	
I & Da	rsonally known [] Produced Identification - Typ	pe of South Notary Public State of Florida
		Yadianys Pino Yadianys Pino My Commission EE 198232
Ident	ification/ /	Expires 05/14/2016
	/ / / / / / /	
Sign	ature of Notary/Flub/c	
Part	V: Building Department Use Only	
	Vision Separation Company	
		6
Α	FEMA 50% Rule Purposes.	6/000=
В	Over Five Year Improvements	\$ 2.703727=
С	Total Improvements	\$ 7714222
D	Building Tax Assessed Value	\$ 7672 600 8
Е	Building Appraised Market Value	s
F	Improvements Cost Ratio (C/E or C/D)	% 3630
If imp Ratio.		ouilding appraised market Value is required for evaluation of Improvement Cost
	Check one box:	
	☐ New Construction and Substantial Improvem	nent Existing Building and Non Substantial Improvement
1	einina Pay	Q 02/14/4
Floo	d Plain Compliance Reviewer	Flood Plain Compl Reviewer signature and date
	Over \$1,000,000.00 Improvements Cost requires Chief Florequires Building Director Approval.	ood Plan Compliance Division Approval, over \$50,000,000.00 Improvements
Nam	е	Signature and Date

## THE STANDARD HOTEL

40 ISLAND AVENUE MIAMI BEACH, FL 33139

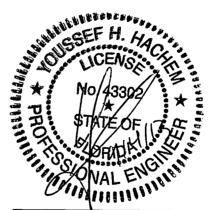
## **STRUCTURAL CALCULATIONS**

**NEW DOOR REINFORCEMENT DESIGN** 



Job. No. E130160 September 3, 2013





Youssef H. Hachem, Ph.D., P.E. P.E. License No. 43302 12151 SW 128 Ct., Suite 104 Miami, Florida 33186 (305) 969-YHCE yh@yhengineering.com

フ\ Pages



YHCE, Inc.
Youssef Hachem Consulting Engineering
12151 SW 128th Court, Suite 104
Miami, FL 33186
(305) 969-YHCE / www.yhengineering.com

JOB E130160	
SHEET NO.	OF
CALCULATED BY HH	DATE
CHECKED BY	DATE

SCALE	
EXIST TB RENFUELEMENT DESILON	
· ATTACH CIZX30 CHANNEL TO EXIST	1 1 1 5
LO ASTM A992 GRADE 50	<del>                                     </del>
LA PINNED @ BOTH ENDS WI CONNECT	TIONS EVERY 2.5'
LEJRESULT - OKAY!	
LOCHECK VISUAL ANALYSIS CALCS-	
	EXIST TIE BEAM
	EXIST TESC.
////	
	1
	2/-0/
21-0"	
	• • •
, Date	
OPENING.	
	MRUJUD LINE
	$\bigcup_{i=1}^{n} f_i \bigcup_{i=1}^{n} $
6-0"	
JSE	
TITED AD ANCHORS: ALLOWAGEE	DESIGN
3/4" \( \omega \omega / 5 \sqrt{2"}	
EMBEDMENT.(2) - 300 165x2=6000 >	2942.9 165
	E OLAY
STAMMERED @ 258	
7.5' M 12" SPACING. 3000 155 >	1012; 2391 165)

Total	.00	24630	236.45	.00	.00	.0 -7		.0
Roof	4.80	0	.00	.00	.00	.0	.0	.0
Roof	4.80	0	.00	.00	.00	.0	.0	.0
Roof	4.80	0	.00	.00	.00	.0	.0	.0

#### Notes - Along Ridge

- Note (1) Ref Fig 27.4-1, Parallel to Ridge (All), h/l= 0.27
- Note (2) X= Along Building ridge, Y = Normal to Building Ridge, Z = Vertical Note (3) MIN = Minimum pressures on Walls = 9.6 psf and Roof = 4.8 psf
- Note (4) Area\* = Area of the surface projected onto a vertical plane normal to wind.

#### Total Base Reaction Summary

Description	Fx Kip	Fy Kip	Fz Kip	Mx K-ft	My K-ft	Mz K-ft
Normal to Ridge Walls+Roof +GCpi	.0	733.1	3033.6	112980.9	.0	.0
Normal to Ridge Walls Only +GCpi	.0	733.1	.0	22722.8	.0	.0
Normal to Ridge Walls+Roof -GCpi	- 0	733.1	982.9	112980.9	.0	. 0
Normal to Ridge Walls Only -GCpi	.0	733.1	.0	22722.8	. 0	.0
Normal to Ridge Walls+Roof MIN	.0	129.6	. 0	3888.0	.0	.0
Along Ridge Walls+Roof +GCpi	1549.3	.0	3498.0	.0	-117172.5	.0
Along Ridge Walls Only +GCpi	1549.3	.0	.0	.0	-47810.4	.0
Along Ridge Walls+Roof -GCpi	1549.3	.0	1447.3	.0	-117172.5	.0
Along Ridge Walls Only -GCpi	1549.3	.0	.0	.0	-47810.4	.0
Along Ridge Walls+Roof MIN	236.4	.0	.0	.0	-7093.4	.0

#### Notes Applying to MWFRS Reactions:

- Note (1) Per Fig 27.4-1, Note 9, Use greater of Shear calculated with or without roof.

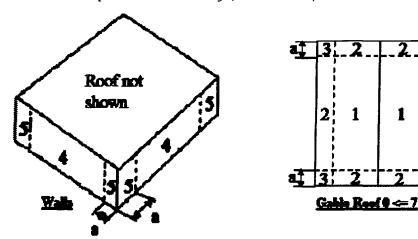
  Note (2) X= Along Building ridge, Y = Normal to Building Ridge, Z = Vertical

  Note (3) MIN = Minimum pressures on Walls = 9.6 psf and Roof = 4.8 psf

  Note (4) MIN area is the area of the surface onto a vertical plane normal to wind.

- Note (5) Total Roof Area (incl OH Top) = .00 sq. ft

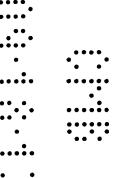
#### Wind Pressure on Components and Cladding (Ch 30 Part 1)



All pressures shown are based upon ASD Design, with a Load Factor of .6

Width of Pressure Coefficient Zone "a" = = 22.50 ft

Description	Width ft	Span ft	Area Zone ft <sup>2</sup>	Max GCp	Min GCp	Max P psf	Min P psf
Zone 1 Zone 2 Zone 3 Zone 4	1.00 1.00 1.00	1.00 1.00 1.00	1.0 1 1.0 2 1.0 3	0.30	-1.00 -1.80 -2.80 -0.99		-72.78 -122.12 -183.79 -72.16
Zone 5	1.00	1.00	1.0 5		-1.26	66.61	-88.81

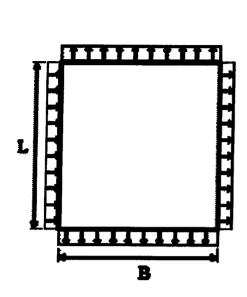


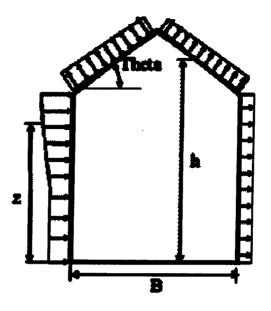
#### MecaWind Pro v2.2.1.3 per ASCE 7-10

Developed by MECA Enterprises, Inc. Copyright 2013 www.mecaenterprises.com

```
: H130940
               : 8/7/2013
                                                 Project No.
 Company Name : Youssef Hachem Consulting Engi
                                                 Designed By
                                                              : HH
 Address
             : 12151 SW 128 Ct, Suite: 104
                                                 Description
                                                              : The Standard
 City
              : Miami
                                                 Customer Name :
                                                 Proj Location : Miami Beach, FL
 State
              : FL
 File Location: 2:\2013\Beilinson and Gomez\E130160 (The Standard Hotel)\DESIGN PHASE\Calculations\WIND
CALC'S\New Spa Door Wind Calcs..wnd
 Input Parameters: Directional Procedure All Heights Building (Ch 27 Part 1)
                              = 175.00 mph
      Basic Wind Speed(V)
      Structural Category
                                      11
                                                    Exposure Category
                                   N/A
                                                    Flexible Structure
                                                                                 No
      Natural Frequency
                                                                               1.00
      Importance Factor
                                    1.00
                                                    Kd Directional Factor
                                   11.50
                                                                              700.00 ft
      Alpha
                                                    Za
                                    0.09
                                                                               1.07
      Αt
                                                                                0.80
      Αm
                                    0.11
                                                    Βm
                                    0.15
                                                   1
                                                                             650.00 ft
      Cc
                                                                               7.00 ft
      Epsilon
                                    0.13
                                                    Zmin
                                                   Slope of Roof(Theta)
      Slope of Roof
      Ht: Mean Roof Ht
                                   60.00 ft
                                                   Type of Roof
                                                                           = FLAT
                                   60.00 ft
                                                   Eht: Eave Height
                                                                              60.00 ft
      RHt: Ridge Ht
      OH: Roof Overhang at Eave=
                                     .00 ft
                                                   Overhead Type
                                                                          = No Overhang
      Bldg Length Along Ridge = 225.00 ft
                                                   Bldg Width Across Ridge= 410.50 ft
Gust Factor Calculations
      Gust Factor Category I Rigid Structures - Simplified Method
      Gustl: For Rigid Structures (Nat. Freq.>1 Hz) use 0.85
                                                                    = 0.85
      Gust Factor Category II Rigid Structures - Complete Analysis
                                                                    = 36.00 ft
             0.6*Ht
      2m:
             Cc*(33/Zm)^0.167
                                                                        0.15
      lzm:
             1*(Zm/33) Epsilon
(1/(1+0.63*((B+Ht)/Lzm)^0.63))^0.5
                                                                    = 657.11 ft
      Lzm:
                                                                       0.81
      0:
      Gust2: 0.925*((1+1.7*1zm*3.4*Q)/(1+1.7*3.4*1zm))
                                                                        0.85
      Gust Factor Summary
      Not a Flexible Structure use the Lessor of Gustl or Gust2
                                                                    = 0.85
Table 26.11-1 Internal Pressure Coefficients for Buildings, GCpi
                                                                    = +/~0.18
     GCPi : Internal Pressure Coefficient
```

Wind Pressurs Main Wind Force Resisting System (MWFRS) - Ref Figure 27.4-1





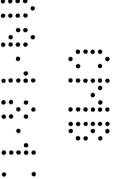
Kh: 2.91\*(Ht/Zg)^(2/Alpha)
Kht: Topographic Factor (Figure 6-4)
Qh: .00256\*(V)^2\*I\*Kh\*Kht\*Kd
Cpww: Windward Wall Cp(Ref Fig 6-6)
Roof Area
Reduction Factor based on Roof Area

= 1.31 = 1.00 = 61.67 psf = 0.80 = .00 ft^2 = 1.00

MWFRS-Wall Pressures for Wind Normal to 225 ft Wall (Normal to Ridge) All pressures shown are based upon ASD Design, with a Load Factor of .6

Wall	Ср	Pressure +GCpi (psf)	Pressure -GCpi (psf)
Leeward Wall	-0.34	-28.58	-6.37
Side Walls	-0.70	-47.61	-25.40

Wall	Elev ft	Kz	Kzt	Ср	qz psf	Press +GCpi	Press -GCpi	Total +/-GCpi
Windward	60.00	1.31	1.00	0.80	61.67	30.62	52.82	59.20
Windward	59.00	1.31	1.00	0.80	61.49	30.50	52.70	59.08
Windward	58.00 1	1.30	1.00	0.80	61.31	30.37	52.58	58.95
Windward	57.00 1	.30	1.00	0.80	61.13	30.25	52.45	58.83
Windward	56.00 1	.30	1.00	0.80	60.94	30.12	52.32	58.70
Windward	55.00 1	.29	1.00	0.80	60.75	29.99	52.20	58.57
Windward	54.00 1	.29	1.00	0.80	60.55	29.86	52.06	58.44
Windward	53.00 1	.28	1.00	0.80	60.36	29.73	51.93	58.31
Windward	52.00 1	.28	1.00	0.80	60.16	29.59	51.80	58.17
Windward	51.00 1	.27	1.00	0.80	59.96	29.46	51.66	58.03
Windward	50.00 1	.27	1.00	0.80	59.75	29.32	51.52	57.90
Windward	49.00 1	.27	1.00	0.80	59.54	29.18	51.38	57.75
Windward	48.00 1	.26	1.00	0.80	59.33	29.03	51.23	57.61
Windward	47.00 1	.26	1.00	0.80	59.11	28.88	51.09	57.46
Windward	46.00 1	.25	1.00	0.80	58.89	28.74	50.94	57.31
Windward	45.00 1	.25	1.00	0.80	58.66	28.58	50.79	57.16
Windward	44.00 1	.24	1.00	0.80	58.44	28.43	50.63	57.01
Windward	43.00 1	.24	1.00	0.80	58.20	28.27	50.47	56.85
Windward	42.00 1	.23	1.00	0.80	57.97	28.11	50.31	56.69
Windward	41.00 1	.23	1.00	0.80	57.72	27.95	50.15	56.52
Windward	40.00 1	. 22	1.00	0.80	57.48	27.78	49.98	56.36
Windward	39.00 1	.22	1.00	0.80	57.22	27.61	49.81	56.19
Windward	38.00 1	.21	1.00	0.80	56.97	27.43	49.64	56.01
Windward	37.00 1	.21	1.00	0.80	56.70	27.26	49.46	55.83
Windward	36.00 1	.20	1.00	0.80	56.43	27.07	49.28	55.65
Windward	35.00 1	.19	1.00	0.80	56.16	26.89	49.09	55.46
Windward	34.00 1	. 19	1.00	0.80	55.87	26.70	48.90	55.27
Windward	33.00 1	.18	1.00	0.80	55.58	26.50	48.70	55.08

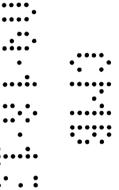


Windward	32.00	1.18	1.00	0.80	55.29	26.30	48.50	54.88
Windward	31.00	1.17	1.00	0.80	54.98	26.09	48.30	54.67
Windward	30.00	1.16	1.00	0.80	54.67	25.88	48.08	54.46
Windward	29.00	1.16	1.00	0.80	54.35	25.66	47.87	54.24
Windward	28.00	1.15	1.00	0.80	54.02	25.44	47.64	54.02
Windward	27.00	1.14	1.00	0.80	53.68	25.21	47.41	53.79
Windward	26.00	1.13	1.00	0.80	53.33	24.97	47.18	53.55
Windward	25.00	1.13	1.00	0.80	52.96	24.73	46.93	53.31
Windward	24.00	1.12	1.00	0.80	52.59	24.47	46.68	53.05
Windward	23.00	1.11	1.00	0.80	52.20	24.21	46.41	52.79
Windward	22.00	1.10	1.00	0.80	51.80	23.94	46.14	52.52
Windward	21.00	1.09	1.00	0.80	51.38	23.66	45.86	52.24
Windward	20.00	1.08	1.00	0.80	50.95	23.36	45.57	51.94
Windward	19.00	1.07	1.00	0.80	50.50	23.06	45.26	51.64
Windward	18.00	1.06	1.00	0.80	50.02	22.74	44.94	51.32
Windward	17.00	1.05	1.00	0.80	49.53	22.40	44.61	50.98
Windward	16.00	1.04	1.00	0.80	49.01	22.05	44.25	50.63
Windward	15.00	1.03	1.00	0.80	48.46	21.68	43.88	50.26
Windward	14.00	1.03	1.00	0.80	48.46	21.68	43.88	50.26
Windward	13.00	1.03	1.00	0.80	48.46	21.68	43.88	50.26
Windward	12.00	1.03	1.00	0.80	48.46	21.68	43.88	50.26
Windward	11.00	1.03	1.00	0.80	48.46	21.68	43.88	50.26
Windward	10.00	1.03	1.00	0.80	48.46	21.68	43.88	50.26
Windward	9.00	1.03	1.00	0.80	48.46	21.68	43.88	50.26
Windward	8.00	1.03	1.00	0.80	48.46	21.68	43.88	50.26
Windward	7.00	1.03	1.00	0.80	48.46	21.68	43.88	50.26
Windward	6.00	1.03	1.00	0.80	48.46	21.68	43.88	50.26
Windward	5.00	1.03	1.00	0.80	48.46	21.68	43.88	50.26
Windward	4.00	1.03	1.00	0.80	48.46	21.68	43.88	50.26
Windward	3.00	1.03	1.00	0.80	48.46	21.68	43.88	50.26
Windward	2.00	1.03	1.00	0.80	48.46	21.68	43.88	50.26
Windward	1.00	1.03	1.00	0.80	48.46	21.68	43.88	50.26

Roof - Dist from Windward Edge	Cp	Pressure +GCpi(psf)	Pressure -GCpi(psf)
Roof: 0.0 ft to 30.0 ft	-C.90	-58.04	-35.83
Roof: 30.0 ft to 60.0 ft	-0.90	-58.04	-35.83
Roof: 60.0 ft to 120.0 ft	-0.50	-37.18	-14.97
Roof: 120.0 ft to 410.5ft	-0.30	-26.75	-4.54

Normal to Ridge - Base Reactions - Walls+Roof +GCpi

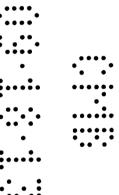
Description	Press psf	Area ft^2	Fx Kip	Fy Kip	Fz Kip	Mx K-ft	My K-ft	Mz K-ft
Leeward Wall	-28.58	13500	.00	385.80	.00	11574.1	. 0	. 0
Side Wall	-47.61		-1172.57	.00	.00	.0	35177.0	.0
Side Wall	-47.61		1172.57	.00	.00	.0-	-35177.0	.0
Windward Wall	30.62	225	.00	6.89	.00	409.9	. 0	.0
Windward Wall	30.50	225	.00	6.86	.00	401.4	.0	. 0
Windward Wall	30.37	225	.00	6.83	.00	393.0	.0	.0
Windward Wall	30.25	225	.00	6.81	.00	384.5	. 0	. 0
Windward Wall	30.12	225	.00	6.78	.00	376.1	.0	.0
Windward Wall	29.99	225	.00	6.75	.00	367.8	.0	.0
Windward Wall	29.86	225	.00	6.72	.00	359.5	.0	.0
Windward Wall	29.73	225	.00	6.69	.00	351.2	.0	.0
Windward Wall	29.59	225	.00	6.66	.00	342.9	. 0	.0
Windward Wall	29.46	225	.00	6.63	.00	334.7	.0	.0
Windward Wall	29.32	225	.00	6.60	.00	326.5	.0	.0
Windward Wall	29.18	225	.00	6.56	.00	318.4	.0	.0
Windward Wall	29.03	225	.00	6.53	.00	310.3	.0	.0
Windward Wall	28.88	225	.00	6.50	.00	302.2	.0	.0
Windward Wall	28.74	225	.00	6.47	.00	294.2	.0	.0
Windward Wall	28.58	225	.00	6.43	.00	286.2	. 0	.0
Windward Wall	28.43	225	.00	6.40	.00	278.2	. 0	.0
Windward Wall	28.27	225	.00	6.36	.00	270.3	. 0	.0
Windward Wall	28.11	225	.00	6.32	.00	262.5	. 0	.0
Windward Wall	27.95	225	.00	6.29	.00	254.7	.0	.0
Windward Wall	27.78	225	.00	6.25	.00	246.9	.0	.0
Windward Wall	27.61	225	.00	6.21	.00	239.2	.0	.0
Windward Wall	27.43	225	.00	6.17	.00	231.5	.0	.0
Windward Wall	27.26	225	.00	6.13	.00	223.8	.0	.0
Windward Wall	27.07	225	.00	6.09	.00	216.2	.0	.0
Windward Wall	26.89	225	.00	6.05	.00	208.7	.0	.0
Windward Wall	26.70	225	.00	6.01	.00	201.2	.0	.0
Windward Wall	26.50	225	.00	5.96	.00	193.8	.0	.0



Windward Wall	26.30	225	.00	5.92	.00	186.4	- 0	.0
Windward Wall	26.09	225	.00	5.87	.00	179.1	. 0	.0
Windward Wall	25.88	225	.00	5.82	.00	171.8	.0	.0
Windward Wall	25.66	225	.00	5.77	.00	164.6	.0	.0
Windward Wall	25.44	225	.00	5.72	.00	157.4	.0	.0
Windward Wall	25.21	225	.00	5.67	.00	150.3	.0	.0
Windward Wall	24.97	225	.00	5.62	.00	143.3	.0	.0
Windward Wall	24.73	225	.00	5.56	.00	136.3	. 0	.0
Windward Wall	24.47	225	.00	5.51	.00	129.4	.0	.0
Windward Wall	24.21	225	.00	5.45	.00	122.6	.0	.0
Windward Wall	23.94	225	.00	5.39		115.8	.0	.0
Windward Wall	23.66	225	.00	5.32	.00	109.1	.0	.0
Windward Wall	23.36	225	.00	5.26	.00	102.5	.0	.0
Windward Wall	23.06	225	.00	5.19		96.0	.0	.0
Windward Wall	22.74	225	.00	5.12	.00	89.5	.0	.0
Windward Wall	22.40	225	.00	5.04	.00	83.2	. 0	.0
Windward Wall	22.05	225	.00	4.96	.00	76.9	- 0	.0
Windward Wall	21.68	225	.00	4.88	.00	70.7	.0	.0
Windward Wall	21.68	225	.00	4.88	.00	65.9	. 0	.0
Windward Wall	21.68	225	.00	4.88	.00	61.0	.0	.0
Windward Wall	21.68	225	.00	4.88	.00	56.1	.0	.0
Windward Wall	21.68	225	.00	4.88	.00	51.2	.0	.0
Windward Wall	21.68	225	.00	4.88	.00	46.3	. 0	.0
Windward Wall	21.68	225	.00	4.88	.00	41.5	.0	.0
Windward Wall	21.68	225	.00	4.88	.00	36.6	.0	.0
Windward Wall	21.68	225	.00	4.88	.00	31.7	. 0	.0
Windward Wall	21.68	225	.00	4.88	.00	26.8	.0	.0
Windward Wall	21.68	225	.00	4.88	.00	22.0	- 0	.0
Windward Wall	21.68	225	.00	4.88	.00	17.1	.0	.0
Windward Wall	21.68	225	.00	4.88	.00	12.2	.0	.0
Windward Wall	21.68	225	.00	4.88	.00	7.3	.0	.0
Windward Wall	21.68	225	.00	4.88	.00	2.4	.0	.0
Roof (0 to h/2)	-58.04	6750	.00	.00	391.75	74531.1	.0	.0
Roof (h/2 to h)	-58.04	6750	.00	.00	391.75	2778.5	.0	.0
Roof (h to 2h)	-37.18	13500	.00	.00	501.89	7842.9	.0	.0
Roof (>2h)	-26.75	65363	.00	.00	1748.24-1	04894.3	.0	.0
Total	.00	168623	.00	733.12	3033.6411	2980.9	.0	.0

Normal to Ridge - Base Reactions - Walls Only +GCpi

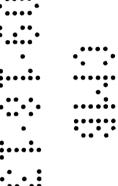
Description	Press psf	Area ft^2	Fx Kip	Fy Kip	Fz Kip	Mx K-ft	My K-ft	Mz K-ft
Leeward Wall	-28.58	13500	.00	385.80	.00	11574.1	.0	.0
Side Wall	-47.61	24630-	-1172.57	.00	.00	.0	35177.0	.0
Side Wall	-47.61	24630	1172.57	.00	.00	. 0-	-35177.0	.0
Windward Wall	30.62	225	.00	6.89	.00	409.9	. 0	.0
Windward Wall	30.50	225	.00	6.86	.00	401.4	.0	.0
Windward Wall	30.37	225	.00	6.83	.00	393.0	.0	.0
Windward Wall	30.25	225	.00	6.81	.00	384.5	. 0	. 0
Windward Wall	30.12	225	.00	6.78	.00	376.1	.0	.0
Windward Wall	29.99	225	.00	6.75	.00	367.8	.0	.0
Windward Wall	29.86	225	.00	6.72	-00	359.5	.0	.0
Windward Wall	29.73	225	.00	6.69	.00	351.2	.0	.0
Windward Wall	29.59	225	.00	6.66	.00	342.9	.0	.0
Windward Wall	29.46	225	.00	6.63	.00	334.7	.0	.0
Windward Wall	29.32	225	.00	6.60	.00	326.5	.0	.0
Windward Wall	29.18	225	.00	6.56	.00	318.4	. 0	.0
Windward Wall	29.03	225	.00	6.53	.00	310.3	. 0	.0
Windward Wall	28.88	225	.00	6.50	.00	302.2	. 0	.0
Windward Wall	28.74	225	.00	6.47	.00	294.2	.0	.0
Windward Wall	28.58	225	.00	6.43	.00	286.2	.0	.0
Windward Wall	28.43	225	.00	6.40	.00	278.2	.0	.0
Windward Wall	28.27	225	.00	6.36	.00	270.3	. 0	.0
Windward Wall	28.11	225	.00	6.32	.00	262.5	.0	.0
Windward Wall	27.95	225	.00	6.29	.00	254.7	.0	.0
Windward Wall	27.78	225	.00	6.25	.00	246.9	.0	.0
Windward Wall	27.61	225	.00	6.21	.00	239.2	.0	.0
Windward Wall	27.43	225	.00	6.17	.00	231.5	.0	.0
Windward Wall	27.26	225	.00	6.13	.00	223.8	.0	.0
Windward Wall	27.07	225	.00	6.09	.00	216.2	.0	.0
Windward Wall	26.89	225	.00	6.05	.00	208.7	.0	.0
Windward Wall	26.70	225	.00	6.01	.00	201.2	.0	.0
Windward Wall	26.50	225	.00	5.96	.00	193.8	.0	.0
Windward Wall	26.30	225	.00	5.92	.00	186.4	.0	.0
Windward Wall	26.09	225	.00	5.87	.00	179.1	.0	.0
Windward Wall	25.88	225	.00	5.82	.00	171.8	.0	.0



		205						
Windward Wall	25.66		.00	5.77	.00			-
Windward Wall	25.44		.00	5.72	.00		. 0	
Windward Wall	25.21		.00	5.67	.00		.0	
Windward Wall	24.97		.00	5.62	.00			
Windward Wall	24.73		.00	5.56	.00			
Windward Wall	24.47		.00	5.51	.00		.0	
Windward Wall	24.21		.00	5.45	.00		.0	
Windward Wall	23.94	225	.00	5.39	.00	115.8	.0	.0
Windward Wall	23.66	225	.00	5.32	.00	109.1	.0	.0
Windward Wall	23.36	225	.00	5.26	.00	102.5	.0	.0
Windward Wall	23.06	225	.00	5.19	.00	96.0	.0	.0
Windward Wall	22.74	225	.00	5.12	.00	89.5	.0	.0
Windward Wall	22.40	225	.00	5.04	.00	83.2	.0	.0
Windward Wall	22.05	225	.00	4.96	.00	76.9	.0	.0
Windward Wall	21.68	225	.00	4.88	.00	70.7	.0	.0
Windward Wall	21.68	225	.00	4.88	.00	65.9	.0	.0
Windward Wall	21.68	225	.00	4.88	.00	61.0	.0	. 0
Windward Wall	21.68	225	.00	4.88	.00	56.1	.0	.0
Windward Wall	21.68	225	.00	4.88	.00	51.2	.0	.0
Windward Wall	21.68	225	.00	4.88	.00	46.3	.0	.0
Windward Wall	21.68	225	.00	4.88	.00	41.5	.0	.0
Windward Wall	21.68	225	.00	4.88	.00	36.6	.0	.0
Windward Wall	21.68	225	.00	4.88	.00	31.7	.0	.0
Windward Wall	21.68	225	.00	4.88	.00	26.8	.0	.0
Windward Wall	21.68	225	.00	4.88	.00	22.0	. 0	. 0
Windward Wall	21.68	225	.00	4.88	.00	17.1	.0	.0
Windward Wall	21.68	225	.00	4.88	.00	12.2	.0	.0
Windward Wall	21.68	225	.00	4.88	.00	7.3	. 0	.0
Windward Wall	21.68	225	.00	4.88	.00	2.4	. 0	.0
Total	-00	76260	.00	733.12	.00	22722.8	. 0	. 0

Normal to Ridge - Base Reactions - Walls+Roof -GCpi

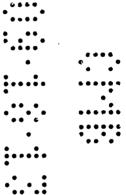
Description	Press psf	Area ft^2	Fx Kip	Fy Kip	Fz Kip	Mx K-ft	My K-ft	Mz K-ft
Leeward Wall	-6.37	13500	.00	86.06	.00	2581.9	.0	.0
Side Wall	-25.40	24630	-625.71	.00	.00	.0	18771.3	.0
Side Wall	-25.40	24630	625.71	.00	.00		-18771.3	.0
Windward Wall	52.82	225	.00	11.89	.00	707.2	.0	. 0
Windward Wall	52.70	225	.00	11.86	.00	693.7	.0	.0
Windward Wall	52.58	225	.00	11.83	.00	680.2	.0	.0
Windward Wall	52.45	225	.00	11.80	.00	666.8	.0	.0
Windward Wall	52.32	225	.00	11.77	.00	653.4	.0	.0
Windward Wall	52.20	225	.00	11.74	.00	640.1	.0	.0
Windward Wall	52.06	225	.00	11.71	.00	626.7	.0	.0
Windward Wall	51.93	225	.00	11.68	.00	613.4	.0	.0
Windward Wall	51.80	225	.00	11.65	.00	600.2	.0	.0
Windward Wall	51.66	225	.00	11.62	.00	587.0	.0	.0
Windward Wall	51.52	225	.00	11.59	.00	573.8	.0	.0
Windward Wall	51.38	225	.00	11.56	.00	560.7	.0	.0
Windward Wall	51.23	225	.00	11.53	.00	547.6	.0	.0
Windward Wall	51.09	225	.00	11.49	.00	534.5	. 0	.0
Windward Wall	50.94	225	.00	11.46	.00	521.5	. 0	.0
Windward Wall	50.79	225	.00	11.43	.00	508.5	. 0	.0
Windward Wall	50.63	225	.00	11.39	.00	495.6	.0	.0
Windward Wall	50.47	225	.00	11.36	.00	482.7	. 0	. 0
Windward Wall	50.31	225	.00	11.32	.00	469.8	.0	.0
Windward Wall	50.15	225	.00	11.28	.00	457.0	. С	. 0
Windward Wall	49.98	225	.00	11.25	.00	444.2	.0	.0
Windward Wall	49.81	225	.00	11.21	.00	431.5	.0	.0
Windward Wall	49.64	225	.00	11.17	.00	418.8	.0	.0
Windward Wall	49.46	225	.00	11.13	.00	406.2	.0	.0
Windward Wall	49.28	225	.00	11.09	.00	393.6	.0	. 0
Windward Wall	49.09	225	.00	11.05	.00	381.1	.0	.0
Windward Wall	48.90	225	.00	11.00	.00	368.6	.0	.0
Windward Wall	48.70	225	.00	10.96	.00	356.1	.0	.0
Windward Wall	48.50	225	.00	10.91	.00	343.8	.0	.0
Windward Wall	48.30	225	.00	10.87	.00	331.4	.0	.0
Windward Wall	48.08	225	.00	10.82	.00	319.2	.0	.0
Windward Wall	47.87	225	.00	10.77	.00	306.9	.0	.0
Windward Wall	47.64	225	.00	10.72	.00	294.8	. 0	.0
Windward Wall	47.41	225	.00	10.67	.00	282.7	.0	.0
Windward Wall	47.18	225	.00	10.61	.00	270.7	.0	.0
Windward Wall	46.93	225	.00	10.56	.00	258.7	. 0	.0
Windward Wall	46.68	225	.00	10.50	.00	246.8	.0	.0
Windward Wall	46.41	225	.00	10.44	.00	235.0	.0	.0



Windward Wall	46.14	. 225	.00	10.38	.00	223.2	. 0	.0
Windward Wall	45.86	225	.00	10.32	.00	211.5	.0	.0
Windward Wall	45.57	225	.00	10.25	.00	199.9	.0	.0
Windward Wall	45.26	225	.00	10.18	.00	188.4	. 0	.0
Windward Wall	44.94	225	.00	10.11	.00	177.0	. 0	.0
Windward Wall	44.61	225	.00	10.04	.00	165.6	.0	.0
Windward Wall	44.25	225	.00	9.96	.00	154.3	.0	.0
Windward Wall	43.88	225	.00	9.87	.00	143.2	.0	.0
Windward Wall	43.88	225	.00	9.87	.00	133.3	.0	.0
Windward Wall	43.88	225	.00	9.87	.00	123.4	.0	.0
Windward Wall	43.88	225	.00	9.87	.00	113.6	.0	.0
Windward Wall	43.88	225	.00	9.87	.00	103.7	.0	.0
Windward Wall	43.88	225	.00	9.87	.00	93.8	.0	.0
Windward Wall	43.88	225	.00	9.87	.00	83.9	.0	.0
Windward Wall	43.88	225	.00	9.87	.00	74.1	.0	.0
Windward Wall	43.88	225	-00	9.87	.00	64.2	.0	.0
Windward Wall	43.88	225	.00	9.87	.00	54.3	.0	.0
Windward Wall	43.88	225	.00	9.87	.00	44.4	.0	.0
Windward Wall	43.88	225	.00	9.87	.00	34.6	.0	.0
Windward Wall	43.88	225	.00	9.87	.00	24.7	.0	.0
Windward Wall	43.88	225	.00	9.87	.00	14.8	.0	.0
Windward Wall	43.88	225	.00	9.87	.00	4.9	.0	.0
Roof (0 to h/2)	-35.83	6750	.00	.00	241.88	46018.4	.0	.0
Roof (h/2 to h)	-35.83	6750	.00	.00	241.88	38761.9	.0	.0
Roof (h to 2h)	-14.97	13500	.00	.00	202.15	23297.9	.0	.0
Roof (>2h)	-4.54	65363	.00	.00	297.00-	17820.1	.0	.0
Total	.00	168623	.00	733.12	982.921	12980.9	.0	

Normal to Ridge - Base Reactions - Walls Only -GCpi

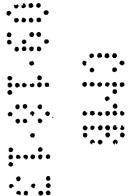
Description	Press psf	Area ft <sup>2</sup>	Fx Kip	Fy Kip	Fz Kip	Mx K-ft	My K-ft	M2 K-ft
Leeward Wall	-6.37	13500	.00	86.06	.00	2581.9	.0	.0
Side Wall	-25.40		-625.71	.00	.00		18771.3	.0
Side Wall	-25.40	24630	625.71	.00	.00		18771.3	.0
Windward Wall	52.82	225	.00	11.89	.00	707.2	.0	.0
Windward Wall	52.70	225	.00	11.86	.00	693.7	. 0	. 0
Windward Wall	52.58	225	.00	11.83	.00	680.2	.0	.0
Windward Wall	52.45	225	.00	11.80	.00	666.8	.0	.0
Windward Wall	52.32	225	.00	11.77	.00	653.4	.0	.0
Windward Wall	52.20	225	.00	11.74	.00	640.1	.0	.0
Windward Wall	52.06	225	.00	11.71	.00	626.7	.0	.0
Windward Wall	51.93	225	.00	11.68	.00	613.4	.0	.0
Windward Wall	51.80	225	.00	11.65	.00	600.2	.0	.0
Windward Wall	51.66	225	.00	11.62	.00	587.0	.0	.0
Windward Wall	51.52	225	.00	11.59	.00	573.8	.0	.0
Windward Wall	51.38	225	.00	11.56	.00	560.7	.0	.0
Windward Wall Windward Wall	51.23	225 225	.00	11.53	.00	547.6	.0	.0
Windward Wall	51.09 50.94	225	.00	11.49 11.46	.00	534.5	.0	.0
Windward Wall	50.79	225	.00	11.46	.00	521.5 508.5	.0	.0
Windward Wall	50.79	225	.00	11.43	.00	495.6	.0	.0
Windward Wall	50.47	225	.00	11.39	.00	493.6	.0	.0
Windward Wall	50.31	225	.00	11.30	.00	469.8	.0	.0
Windward Wall	50.15	225	.00	11.28	.00	457.0	.0	.0
Windward Wall	49.98	225	.00	11.25	.00	444.2	.0	.0
Windward Wall	49.81	225	.00	11.21	.00	431.5	.0	.0
Windward Wall	49.64	225	.00	11.17	.00	418.8	.0	.0
Windward Wall	49.46	225	.00	11.13	.00	406.2	.0	.0
Windward Wall	49.28	225	.00	11.09	.00	393.6	. 0	.0
Windward Wall	49.09	225	.00	11.05	.00	381.1	.0	.0
Windward Wall	48.90	225	.00	11.00	.00	368.6	.0	.0
Windward Wall	48.70	225	.00	10.96	.00	356.1	.0	.0
Windward Wall	48.50	225	.00	10.91	.00	343.8	. 0	.0
Windward Wall	48.30	225	.00	10.87	.00	331.4	.0	. 0
Windward Wall	48.08	225	.00	10.82	.00	319.2	. 0	. 0
Windward Wall	47.87	225	.00	10.77	.00	306.9	. 0	.0
Windward Wall	47.64	225	.00	10.72	.00	294.8	.0	.0
Windward Wall	47.41	225	.00	10.67	.00	282.7	.0	.0
Windward Wall	47.18	225	.00	10.61	.00	270.7	.0	.0
Windward Wall	46.93	225	.00	10.56	.00	258.7	.0	.0
Windward Wall	46.68	225	.00	10.50	.00	246.8	.0	.0
Windward Wall	46.41	225	.00	10.44	.00	235.0	. C	.0
Windward Wall	46.14	225	.00	10.38	.00	223.2	.0	.0
Windward Wall	45.86	225	.00	10.32	.00	211.5	.0	.0
Windward Wall	45.57	225	.00	10.25	.00	199.9	.0	.0



Total		.00	76260	.00	733.12	.00	22722.8	. 0	.0
Windward	Wall	43.88	225	.00	9.87	.00	4.9	.0	.0
Windward	Wall	43.88	225	.00	9.87	.00	14.8	.0	.0
Windward		43.88	225	.00	9.87	.00	24.7	.0	.0
Windward	Wall	43.88	225	.00	9.87	.00	34.6	.0	.0
Windward	Wall	43.88	225	.00	9.87	.00	44.4	. 0	.0
Windward	Wall	43.88	225	.00	9.87	.00	54.3	.0	.0
Windward	Wall	43.88	225	.00	9.87	.00	64.2	.0	.0
Windward	Wall	43.88	225	.00	9.87	.00	74.1	. 0	.0
Windward	Wall	43.88	225	.00	9.87	.00	83.9	.0	.0
Windward	Wall	43.88	225	.00	9.87	.00	93.8	.0	.0
Windward	Wall	43.88	225	.00	9.87	.00	103.7	.0	.0
Windward	Wall	43.88	225	.00	9.87	.00	113.6	.0	.0
Windward	Wall	43.88	225	.00	9.87	.00	123.4	.0	.0
Windward	Wall	43.88	225	.00	9.87	.00	133.3	.0	.0
Windward	Wall	43.88	225	.00	9.87	.00	143.2	.0	.0
Windward	Wall	44.25	225	.00	9.96	.00	154.3	.0	.0
Windward	Wall	44.61	225	.00	10.04	.00	165.6	.0	.0
Windward	Wall	44.94	225	.00	10.11	.00	177.0	.0	.0
Windward	Wall	45.26	225	.00	10.18	.00	188.4	.0	.0

Normal to Ridge - Base Reactions - Walls+Roof MIN

Description	Press psf	Area* ft^2	Fx Kip	Fy Kip	Fz Kip	Mx K-ft	My K-ft	Mz K-ft
Windward Wall	9.60	225	.00	2.16	.00	128.5	.0	.0
Windward Wall	9.60	225	.00	2.16	.00	126.4	. 0	.0
Windward Wall	9.60	225	.00	2.16	.00	124.2	.0	.0
Windward Wall	9.60	225	.00	2.16	.00	122.0	.0	.0
Windward Wall	9.60	225	.00	2.16	.00	119.9	.0	.0
Windward Wall	9.60	225	.00	2.16	.00	117.7	.0	.0
Windward Wall	9.60	225	.00	2.16	.00	115.6	. 0	.0
Windward Wall .	9.60	225	.00	2.16	.00	113.4	.0	.0
Windward Wall	9.60	225	.00	2.16	.00	111.2	. 0	. 0
Windward Wall	9.60	225	.00	2.16	.00	109.1	. 0	. 0
Windward Wall	9.60	225	.00	2.16	.00	106.9	.0	.0
Windward Wall	9.60	225	.00	2.16	.00	104.8	.0	.0
Windward Wall	9.60	225	.00	2.16	.00	102.6	.0	.0
Windward Wall	9.60	225	.00	2.16	.00	100.4	.0	.0
Windward Wall	9.60	225	.00	2.16	.00	98.3	. 0	.0
Windward Wall	9.60	225	.00	2.16	.00	96.1	. 0	.0
Windward Wall	9.60	225	.00	2.16	.00	94.0	. 0	. 0
Windward Wall	9.60	225	.00	2.16	.00	91.8	. 0	.0
Windward Wall	9.60	225	.00	2.16	.00	89.6	.0	.0
Windward Wall	9.60	225	.00	2.16	.00	87.5	. 0	.0
Windward Wall	9.60	225	.00	2.16	.00	85.3	. 0	.0
Windward Wall	9.60	225	.00	2.16	.00	83.2	.0	-0
Windward Wall	9.60	225	.00	2.16	.00	81.0	.0	.0
Windward Wall	9.60	225	.00	2.16	.00	78.8	.0	.0
Windward Wall	9.60	225	.00	2.16	.00	76.7	.0	.0
Windward Wall	9.60	225	.00	2.16	.00	74.5	.0	.0
Windward Wall	9.60	225	.00	2.16	.00	72.4	. 0	.0
Windward Wall	9.60	225	.00	2.16	.00	70.2	.0	.0
Windward Wall	9.60	225	.00	2.16	.00	68.0	.0	.0
Windward Wall	9.60	225	.00	2.16	.00	65.9	. 0	.0
Windward Wall	9.60	225	.00	2.16	.00	63.7	.0	.0
Windward Wall	9.60	225	.00	2.16	.00	61.6	. 0	.0
Windward Wall	9.60	225	.00	2.16	.00	59.4	. 0	.0
Windward Wall	9.60	225	.00	2.16	.00	57.2	.0	.0
Windward Wall	9.60	225	.00	2.16	.00	55.1	.0	. 0
Windward Wall	9.60	225	.00	2.16	.00	52.9	.0	.0
Windward Wall	9.60	225	.00	2.16	.00	50.8	.0	.0
Windward Wall	9.60	225	.00	2.16	.00	48.6	.0	.0
Windward Wall	9.60	225	.00	2.16	.00	46.4	. C	.0
Windward Wall	9.60	225	.00	2.16	.00	44.3	.0	.0
Windward Wall	9.60	225	.00	2.16	.00	42.1	.0	.0
Windward Wall	9.60	225	.00	2.16	.00	40.0	.0	.0
Windward Wall	9.60	225	.00	2.16	.00	37.8	.0	.0
Windward Wall	9.60	225	.00	2.16	.00	35.6	. 0	.0
Windward Wall	9.60	225	.00	2.16	.00	33.5	.0	.0
Windward Wall	9.60	225	.00	2.16	.00	31.3	. 0	. 0
Windward Wall	9.60	225	.00	2.16	.00	29.2	. 0	.0
Windward Wall	9.60	225	.00	2.16	.00	27.0	.0	.0
Windward Wall	9.60	225	.00	2.16	.00	24.8	.0	.0
Windward Wall	9.60	225	.00	2.16	.00	22.7	.0	.0
Windward Wall	9.60	225	.00	2.16	.00	20.5	.0	.0



Total	00	13500	0.0	120 60	0.0	3888 0	۸	0
Roof (>2h)	4.80	0	.00	.00	.00	.0	.0	.0
Roof (h to 2h)	4.80	0	.00	.00	.00	.0	. 0	.0
Roof $(h/2 to h)$	4.80	0	.00	.00	.00	.0	.0	.0
Roof (0 to $h/2$ )	4.80	0	.00	.00	.00	.0	.0	.0
Windward Wall	9.60	225	.00	2.16	.00	1.1	.0	.0
Windward Wall	9.60	225	.00	2.16	.00	3.2	.0	.0
Windward Wall	9.60	225	.00	2.16	.00	5.4	.0	.0
Windward Wall	9.60	225	.00	2.16	.00	7.6	.0	.0
Windward Wall	9.60	225	.00	2.16	.00	9.7	.0	.0
Windward Wall	9.60	225	.00	2.16	.00	11.9	.0	.0
Windward Wall	9.60	225	.00	2.16	.00	14.0	.0	.0
Windward Wall	9.60	225	.00	2.16	.00	16.2	. 0	.0
Windward Wall	9.60	225	.00	2.16	.00	18.4	.0	.0

#### Notes - Normal to Ridge

Wall

- Note (1) Per Fig 27.4-1 Note 7, Since Theta<= 10 Deg base calcs on Eave Ht Note (2) Wall & Roof Pressures = Qh\*(G\*Cp GCPi)

- Note (2) Wall & Roof Pressures = Qh\*(6°CP GCP1)

  Note (3) +GCpi = Positive Internal Bldg Press, -GCPi = Negative Internal Bldg Press

  Note (4) Total Pressure = Leeward Press + Windward Press (For + or GCPi)

  Note (5) Ref Fig 27.4-1, Normal to Ridge (Theta<10), Theta= .0 Deg, h/l= 0.15

  Note (6) X= Along Building ridge, Y = Normal to Building Ridge, Z = Vertical

  Note (7) MIN = Minimum pressures on Walls = 9.6 psf and Roof = 4.8 psf

  Note (8) Area\* = Area of the surface projected onto a vertical plane normal to wind.

Pressure +GCpi (psf)

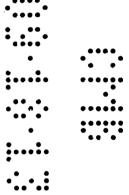
-GCpi (psf)

MWFRS-Wall Pressures for Wind Normal to 410.5 ft wall (Along Ridge) All pressures shown are based upon ASD Design, with a Load Factor of .6

Сp

Leeward Wall	-0	.50	-37	.18	-	14.97		
Side Walls	-0	.70	-47	.61	-	25.40		
Wall	Elev ft	Κz	Kzt	Ср	qz psf	Press +GCpi	Press -GCpi	Total +/-GCpi
Windward	60.00	1.31	1.00	0.80	61.67	30.62	52.82	67.8
Windward	59.00	1.31	1.00	0.80	61.49	30.50	52.70	67.6
Windward	58.00	1.30	1.00	0.80	61.31	30.37	52.58	67.5
Windward	57.00	1.30	1.00	0.80	61.13	30.25	52.45	67.4
Windward	56.00	1.30	1.00	0.80	60.94	30.12	52.32	67.3
Windward	55.00	1.29	1.00	0.80	60.75	29.99	52.20	67.1
Windward	54.00	1.29	1.00	0.80	60.55	29.86	52.06	67.0
Windward	53.00	1.28	1.00	0.80	60.36	29.73	51.93	66.9
Windward	52.00	1.28	1.00	0.80	60.16	29.59	51.80	66.7
Windward	51.00	1.27	1.00	0.80	59.96	29.46	51.66	66.6
Windward	50.00	1.27	1.00	0.80	59.75	29.32	51.52	66.49
Windward	49.00	1.27	1.00	0.80	59.54	29.18	51.38	66.3
Windward	48.00	1.26	1.00	0.80	59.33	29.03	51.23	66.2
Windward	47.00	1.26	1.00	0.80	59.11	28.88	51.09	66.06
Windward	46.00	1.25	1.00	0.80	58.89	28.74	50.94	65.91

Windward	60.00 1	.31 1.00	0.80	61.67	30.62	52.82	67.80
Windward	59.00 1	.31 1.00	0.80	61.49	30.50	52.70	67.67
Windward	58.00 1	.30 1.00	0.80	61.31	30.37	52.58	67.55
Windward	57.00 1	.30 1.00	0.80	61.13	30.25	52.45	67.43
Windward	56.00 1	.30 1.00	0.80	60.94	30.12	52.32	67.30
Windward	55.00 1	.29 1.00	0.80	60.75	29.99	52.20	67.17
Windward	54.00 1	.29 1.00	0.80	60.55	29.86	52.06	67.04
Windward	53.00 1	.28 1.00	0.80	60.36	29.73	51.93	66.91
Windward	52.00 1	.28 1.00	0.80	60.16	29.59	51.80	66.77
Windward	51.00 1	.27 1.00	0.80	59.96	29.46	51.66	66.63
Windward			0.80	59.75	29.32	51.52	66.49
Windward	49.00 1	.27 1.00	0.80	59.54	29.18	51.38	66.35
Windward			0.80	59.33	29.03	51.23	66.21
Windward	47.00 1	.26 1.00	0.80	59.11	28.88	51.09	66.06
Windward			0.80	58.89	28.74	50.94	65.91
Windward			0.80	58.66	28.58	50.79	65.76
Windward			0.80	58.44	28.43	50.63	65.61
Windward			0.80	58.20	28.27	50.47	65.45
Windward			0.80	57.97	28.11	50.31	65.29
Windward			0.80	57.72	27.95	50.15	65.12
Windward			0.80	57.48	27.78	49.98	64.96
Windward		.22 1.00		57.22	27.61	49.81	64.79
Windward		.21 1.00		56.97	27.43	49.64	64.61
Windward			0.80	56.70	27.26	49.46	64.43
Windward			0.80	56.43	27.07	49.28	64.25
Windward			0.80	56.16	26.89	49.09	64.06
Windward		.19 1.00	0.80	55.87	26.70	48.90	63.87
Windward		.18 1.00	0.80	55.58	26.50	48.70	63.68
Windward		18 1.00	0.80	55.29	26.30	48.50	63.48
Windward		.17 1.00		54.98	26.09	48.30	63.27
Windward		16 1.00		54.67	25.88	48.08	63.06
Windward		16 1.00		54.35	25.66	47.87	62.84
Windward		15 1.00		54.02	25.44	47.64	62.62
Windward		14 1.00		53.68	25.21	47.41	62.39
Windward		13 1.00		53.33	24.97	47.18	62.15
Windward		13 1.00		52.96	24.73	46.93	61.90
Windward			0.80	52.59	24.47	46.68	61.65
Windward	23.00 1.	11 1.00	0.80	52.20	24.21	46.41	61.39

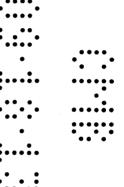


Windward	22.00	1.10	1.00	0.80	51.80	23.94	46.14	61.12
Windward	21.00	1.09	1.00	0.80	51.38	23.66	45.86	60.83
Windward	20.00	1.08	1.00	0.80	50.95	23.36	45.57	60.54
Windward	19.00	1.07	1.00	0.80	50.50	23.06	45.26	60.23
Windward	18.00	1.06	1.00	0.80	50.02	22.74	44.94	59.91
Windward	17.00	1.05	1.00	0.80	49.53	22.40	44.61	59.58
Windward	16.00	1.04	1.00	0.80	49.01	22.05	44.25	59.23
Windward	15.00	1.03	1.00	0.80	48.46	21.68	43.88	58.86
Windward	14.00	1.03	1.00	0.80	48.46	21.68	43.88	58.86
Windward	13.00	1.03	1.00	0.80	48.46	21.68	43.88	58.86
Windward	12.00	1.03	1.00	0.80	48.46	21.68	43.88	58.86
Windward	11.00	1.03	1.00	0.80	48.46	21.68	43.88	58.86
Windward	10.00	1.03	1.00	0.80	48.46	21.68	43.88	58.86
Windward	9.00	1.03	1.00	0.80	48.46	21.68	43.88	58.86
Windward	8.00	1.03	1.00	0.80	48.46	21.68	43.88	58.86
Windward	7.00	1.03	1.00	0.80	48.46	21.68	43.88	58.86
Windward	6.00	1.03	1.00	0.80	48.46	21.68	43.88	58.86
Windward	5.00	1.03	1.00	0.80	48.46	21.68	43.88	58.86
Windward	4.00	1.03	1.00	0.80	48.46	21.68	43.88	58.86
Windward	3.00	1.03	1.00	0.80	48.46	21.68	43.88	58.86
Windward			1.00	0.80	48.46	21.68	43.88	58.86
Windward	1.00	1.03	1.00	0.80	48.46	21.68	43.88	58.86

Roof - Dist from Windward Edge	-		Pressure -GCpi(psf)
Roof: 0.0 ft to 30.0 ft	-0.90	-58.04	-35.83
Roof: 30.0 ft to 60.0 ft	-0.90	-58.04	-35.83
Roof: 60.0 ft to 120.0 ft	-0.50	-37.18	-14.97
Roof: 120.0 ft to 225.0 ft	-0.30	-26.75	-4.54

Along Ridge - Base Reactions - Walls+Roof +GCpi

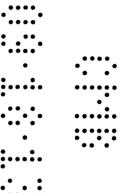
psf ft^2 Kip Kip K-ft K-ft K	-ft
Leeward Wall -37.18 24630 915.67 .00 .00 .0-27470.1	. 0
Side Wall -47.61 13500 .00 642.70 .00 19281.0 .0	. 0
Side Wall -47.61 13500 .00 -642.70 .00-19281.0 .0	.0
Windward Wall 30.62 411 12.57 .00 .00 .0 -747.9	.0
Windward Wall 30.50 411 12.52 .00 .00 .0 -732.4	. 0
Windward Wall 30.37 411 12.47 .00 .00 .0 -716.9	.0
Windward Wall 30.25 411 12.42 .00 .00 .0 -701.6	. 0
Windward Wall 30.12 411 12.37 .00 .00 .0 -686.3	. 0
Windward Wall 29.99 411 12.31 .00 .00 .0 -671.0	. 0
Windward Wall 29.86 411 12.26 .00 .00 .0 -655.8	. 0
Windward Wall 29.73 411 12.20 .00 .00 .0 -640.7	. 0
Windward Wall 29.59 411 12.15 .00 .00 .0 -625.6	.0
Windward Wall 29.46 411 12.09 .00 .00 .0 -610.6	.0
Windward Wall 29.32 411 12.03 .00 .00 .0 -595.7	. 0
Windward Wall 29.18 411 11.98 .00 .00 .0 -580.9	. 0
Windward Wall 29.03 411 11.92 .00 .00 .0 -566.1	. 0
Windward Wall 28.88 411 11.86 .00 .00 .0 -551.4	.0
Windward Wall 28.74 411 11.80 .00 .00 .0 -536.7	.0
Windward Wall 28.58 411 11.73 .00 .00 .0 -522.1	. 0
Windward Wall 28.43 411 11.67 .00 .00 .0 -507.6	. 0
Windward Wall 28.27 411 11.61 .00 .00 .0 -493.2	. 0
Windward Wall 28.11 411 11.54 .00 .00 .0 -478.9	. 0
Windward Wall 27.95 411 11.47 .00 .00 .0 -464.6	. 0
Windward Wall 27.78 411 11.40 .00 .00 .0 -450.4	. 0
Windward Wall 27.61 411 11.33 .C0 .00 .0 -436.3	.0
Windward Wall 27.43 411 11.26 .00 .00 .0 -422.3	.0
Windward Wall 27.26 411 11.19 .00 .00 .0 -408.4	.0
Windward Wall 27.07 411 11.11 .00 .00 .0 -394.5	.0
Windward Wall 26.89 411 11.04 .00 .00 .0 -380.8	.0
Windward Wall 26.70 411 10.96 .00 .00 .0 -367.1	.0
Windward Wall 26.50 411 10.88 .00 .00 .0 -353.5	.0
Windward Wall 26.30 411 10.80 .00 .00 .0 -340.1	.0
Windward Wall 26.09 411 10.71 .00 .00 .0 -326.7	.0
Windward Wall 25.88 411 10.62 .00 .00 .0 -313.4	.0
Windward Wall 25.66 411 10.54 .00 .00 .0 -300.3	.0
Windward Wall 25.44 411 10.44 .00 .00 .0 -287.2	.0
Windward Wall 25.21 411 10.35 .00 .00 .0 -274.2	.0
Windward Wall 24.97 411 10.25 .00 .00 .0 -261.4	.0
Windward Wall 24.73 411 10.15 .00 .00 .0 -248.7	.0
Windward Wall 24.47 411 10.05 .00 .00 .0 -236.1	.0
Windward Wall 24.21 411 9.94 .00 .00 .0 -223.6	.0



Windward	Wall	23.94	411	9.83	.00	.00	.0	-211.3	.0
Windward	Wall	23.66	411	9.71	.00	.00	.0	-199.1	.0
Windward	Wall	23.36	411	9.59	.00	.00	.0	-187.0	.0
Windward	Wall	23.06	411	9.47	.00	.00	.0	-175.1	.0
Windward	Wall	22.74	411	9.33	.00	.00	.0	-163.3	٠0
Windward	Wall	22.40	411	9.20	.00	.00	.0	-151.7	.0
Windward	Wall	22.05	411	9.05	.00	.00	.0	-140.3	.0
Windward	Wall	21.68	411	8.90	.00	.00	.0	-129.1	. 0
Windward	Wall	21.68	411	8.90	.00	.00	.0	-120.2	.0
Windward	Wall	21.68	411	8.90	.00	.00	.0	-111.3	.0
Windward	Wall	21.68	411	8.90	.00	.00	.0	-102.4	. 0
Windward	Wall	21.68	411	8.90	.00	.00	. 0	-93.5	.0
Windward	Wall	21.68	411	8.90	.00	.00	. 0	-84.6	.0
Windward 1	Wall	21.68	411	8.90	.00	.00	.0	-75.7	.0
Windward W	Wall	21.68	411	8.90	.00	.00	. 0	-66.8	.0
Windward N	Wall	21.68	411	8.90	.00	.00	. 0	-57.9	.0
Windward N	Wall	21.68	411	8.90	.00	.00	.0	-49.0	.0
Windward W	Wall	21.68	411	8.90	.00	.00	.0	-40.1	.0
Windward W	Wall	21.68	411	8.90	.00	.00	.0	-31.2	.0
Windward W	Wall	21.68	411	8.90	.00	.00	.0	-22.3	. 0
Windward W	Wall	21.68	411	8.90	.00	.00	.0	-13.4	.0
Windward V	√all	21.68	411	8.90	.00	.00	.0	-4.5	.0
Roof		-58.C4	12315	.00	.00	714.73	.0-	69686.4	.0
Roof		-58.04	12315	.00	.00	714.73	-0-	48244.4	.0
Roof		-37.18	24630	.00	.00	915.67	.0-	20602.6	.0
Roof		-26.75	43103	.00	.00	1152.86	. 0	69171.3	. 0
Total		.00	168623	1549.33	.00	3497.99	. 0-	117172.5	.0
10001		.00	100063						

Along Ridge - Base Reactions - Walls Only +GCpi

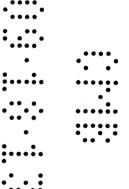
Description	Press psf			Fy Kip	Fz Kip	Mx K-ft	My K-ft	Mz K-ft
Leeward Wall	-37.18	24630	915.67	.00	.00	.0.	-27470.1	.0
Side Wall	-47.61	13500	.00	642.70	.00	19281.0	.0	.0
Side Wall	-47.61	13500	.00	-642.70		19281.0	.0	.0
Windward Wall	30.62	411	12.57		.00		-747.9	- 0
Windward Wall		411	12.52		.00		~732.4	.0
Windward Wall	30.37	411	12.47		.00		-716.9	.0
Windward Wall	30.25	411	12.42		.00		-701.6	- 0
Windward Wall	30.12	411	12.37	.00	.00	.0	-686.3	.0
Windward Wall	29.99	411	12.31		.00	.0	-671.0	.0
Windward Wall	29.86	411	12.26	.00	.00	.0		.0
Windward Wall	29.73	411	12.20	.00	.00	.0	-640.7	.0
Windward Wall	29.59	411	12.15	.00	.00		-625.6	.0
Windward Wall	29.46	411	12.09	.00	.00	.0	-610.6	.0
Windward Wall	29.32	411	12.03	.00	.00		-595.7	.0
Windward Wall	29.18	411	11.98	.00	.00		-580.9	.0
Windward Wall	29.03	411	11.92	.00	.00	.0	-566.1	.0
Windward Wall	28.88	411	11.86	.00	.00	.0	-551.4	.0
Windward Wall	28.74	411	11.80	.00	.00		-536.7	.0
Windward Wall	28.58	411	11.73	.00	.00	.0	-522.1	.0
Windward Wall	28.43	411	11.67	.00	.00	.0		.0
Windward Wall	28.27	411	11.61	.00	.00	.0	-493.2	.0
Windward Wall	28.11	411	11.54	.00	.00	.0		. 0
Windward Wall	27.95	411	11.47	.00	.00		-464.6	.0
Windward Wall	27.78	411	11.40	.00	.00		-450.4	.0
Windward Wall	27.61	411	11.33	.00	.00		-436.3	.0
Windward Wall	27.43	411	11.26	-00			-422.3	.0
Windward Wall	27.26	411	11.19	.00	.00		-408.4	.0
Windward Wall	27.07	411	11.11	.00			-394.5	.0
Windward Wall	26.89	411	11.04	.00	.00		-380.8	.0
Windward Wall	26.70	411	10.96	.00	.00		-367.1	.0
Windward Wall	26.50	411	10.88	.00	.00			.0
Windward Wall	26.30	411	10.80	.00	.00		-340.1	.0
Windward Wall	26.09	411	10.71	.00	.00			.0
Windward Wall	25.88	411	10.62	.00	.00		-313.4	. 0
Windward Wall	25.66	411	10.54	.00	.00			.0
Windward Wall	25.44	411	10.44	.00	.00	.0	-287.2	.0
Windward Wall	25.21	411	10.35	.00	.00	.0		.0
Windward Wall	24.97	411	10.25	.00	.00			.0
Windward Wall	24.73	411	10.15	.00	.00		-248.7	. 0
Windward Wall	24.47	411	10.05	.00	.00	. 0		.0
Windward Wall	24.21	411	9.94	.00	.00			.0
Windward Wall	23.94	411	9.83	.00	.00	.0		. 0
Windward Wall	23.66	411	9.71	.00	.00			.0
Windward Wall	23.36	411	9.59	.00	.00	.0	-187.0	.0



Total		.00	76260	1549.33	.00	.00	.0-	47810.4	.0
Windward	Wall	21.68	411	8.90	.00	.00	.0	-4.5	.0
Windward	Wall	21.68	411	8.90	.00	.00	.0	-13.4	. 0
Windward	Wall	21.68	411	8.90	.00	.00	.0	-22.3	.0
Windward	Wall	21.68	411	8.90	.00	.00	.0	-31.2	.0
Windward	Wall	21.68	411	8.90	.00	.00	.0	-40.1	.0
Windward	Wall	21.68	411	8.90	.00	.00	.0	-49.0	.0
Windward	Wall	21.68	411	8.90	.00	.00	.0	-57.9	.0
Windward	Wall	21.68	411	8.90	.00	.00	.0	-66.8	.0
Windward	Wall	21.68	411	8.90	.00	.00	.0	-75.7	.0
Windward	Wall	21.68	411	8.90	.00	.00	.0	-84.6	.0
Windward	Wall	21.68	411	8.90	.00	.00	.0	-93.5	.0
Windward	Wall	21.68	411	8.90	.00	.00	.0	-102.4	.0
Windward	Wall	21.68	411	8.90	.00	.00	.0	-111.3	.0
Windward	Wall	21.68	411	8.90	.00	.00	.0	-120.2	.0
Windward	Wall	21.68	411	8.90	.00	.00	.0	-129.1	.0
Windward	Wall	22.05	411	9.05	.00	.00	.0	-140.3	.0
Windward	Wall	22.40	411	9.20	.00	.00	.0	-151.7	.0
Windward	Wall	22.74	411	9.33	.00	.00	.0	-163.3	.0
Windward	Wall	23.06	411	9.47	.00	.00	.0	-175.1	.0

Along Ridge - Base Reactions - Walls+Roof -GCpi

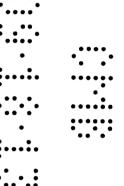
Description	Press psf	Area ft'2	Fx Kip	Fy Kip	Fz Kip	Mx K-ft	My K-ft	Mz K-ft
Leeward Wall	-14.97	24630	368.81	.00	.00	. 0	-11064.4	.0
Side Wall	-25.40	13500	.00	342.96	.00	10288.8	. 0	.0
Side Wall	-25.40	13500	.00	-342.96	.00-	10288.8	.0	.0
Windward Wall	52.82	411	21.68	.00	.00	.0	-1290.2	.0
Windward Wall	52.70	411	21.63	.00	.00	.0	-1265.6	.0
Windward Wall	52.58	411	21.58	.00	.00	.0	+1241.0	.0
Windward Wall	52.45	411	21.53	.00	.00	.0	-1216.5	.0
Windward Wall	52.32	411	21.48	.00	.00	.0	-1192.1	.0
Windward Wall	52.20	411	21.43	.00	.00	.0	-1167.7	.0
Windward Wall	52.06	411	21.37	.00	.00	.0	-1143.4	.0
Windward Wall	51.93	411	21.32	.00	.00	.0	-1119.2	.0
Windward Wall	51.80	411	21.26	.00	.00	.0	-1095.0	.0
Windward Wall	51.66	411	21.21	.00	.00	.0	-1070.9	.0
Windward Wall	51.52	411	21.15	-00	.00	.0	-1046.9	.0
Windward Wall	51.38	411	21.09	.00	.00	.0	-1022.9	.0
Windward Wall	51.23	411	21.03	.00	.00	.0	-999.0	.0
Windward Wall	51.09	411	20.97	.00	.00	.0	-975.2	.0
Windward Wall	50.94	411	20.91	.00	.00	.0	-951.4	.0
Windward Wall	50.79	411	20.85	.00	.00	.0	-927.7	.0
Windward Wall	50.63	411	20.78	.00	.00	- 0	~904.1	.0
Windward Wall	50.47	411	20.72	.00	.00	.0		.0
Windward Wall	50.31	411	20.65	.00	.00	.0		.0
Windward Wall	50.15	411	20.59	.00	.00	.0	-833.7	.0
Windward Wall	49.98	411	20.52	.00	.00	.0		. 0
Windward Wall	49.81	411	20.45	.00	.00	.0		. 0
Windward Wall	49.64	411	20.38	.00	.00	.0	-764.1	.0
Windward Wall	49.46	411	20.30	.00	.00	.0	-741.0	.0
Windward Wall	49.28	411	20.23	.00	.00	.0	-718.1	.0
Windward Wall	49.09	411	20.15	.00	.00	.0	-695.2	.0
Windward Wall	48.90	411	20.07	.00	.00	.0	~672.4	.0
Windward Wall	48.70	411	19.99	.00	.00	.0	-649.8	.0
Windward Wall	48.50	411	19.91	.00	.00	.0	-627.2	.0
Windward Wall	48.30	411	19.83	.00	.00	.0	-604.7	.0
Windward Wall	48.08	411	19.74	.00	.00	.0	-582.3	.0
Windward Wall	47.87	411	19.65	.00	.00	.0	-560.0	.0
Windward Wall	47.64	411	19.56	.00	.00	.0	-537.8	.0
Windward Wall	47.41	411	19.46	.00	.00	.0	-515.8	.0
Windward Wall	47.18	411	19.37	.00	.00	.0	-493.8	.0
Windward Wall	46.93	411	19.26	.00	.00	.0	-472.0	.0
Windward Wall	46.68	411	19.16	.00	.00	.0	-450.3	.0
Windward Wall	46.41	411	19.05	.00	.00	.0	~428.7	. 0
Windward Wall	46.14	411	18.94	.00	.00	.0	-407.2	.0
Windward Wall	45.86	411	18.83	.00	.00	.0	-385.9	.0
Windward Wall	45.57	411	18.70	.00	.00	.0	-364.7	.0
Windward Wall	45.26	411	18.58	.00	.00	.0	-343.7	.0
Windward Wall	44.94	411	18.45	.00	.00	.0	-322.8	.0
Windward Wall	44.61	411	18.31	.00	.00	.0	-302.1	.0
Windward Wall	44.25	411	18.17	.00	.00	.0	-281.6	.0
Windward Wall	43.88	411	18.01	-00	.00	.0	-261.2	.0
Windward Wall	43.88	411	18.01	.00	.00	.0	-243.2	.0
Windward Wall	43.88	411	18.01	.00	.00	.0	-225.2	.0



Windward Wall	43.88	411	18.01	.00	.00	.0	-207.2	.0
Windward Wall	43.88	411	18.01	.00	.00	.0	-189.2	.0
Windward Wall	43.88	411	18.01	.00	.00	.0	-171.1	.0
Windward Wall	43.88	411	18.01	.00	.00	.0	-153.1	.0
Windward Wall	43.88	411	18.01	.00	.00	.0	-135.1	.0
Windward Wall	43.88	411	18.01	.00	.00	.0	-117.1	.0
Windward Wall	43.88	411	18.01	.00	.00	.0	-99.1	.0
Windward Wall	43.88	411	18.01	.00	.00	.0	-81.1	.0
Windward Wall	43.88	411	18.01	.00	.00	.0	-63.1	.0
Windward Wall	43.88	411	18.01	.00	.00	.0	-45.0	.0
Windward Wall	43.88	411	18.01	.00	.00	.0	-27.0	.0
Windward Wall	43.88	411	18.01	.00	.00	.0	-9.0	.0
Roof	-35.83	12315	.00	.00	441.30	.0-4	3027.1	.0
Roof	-35.83	12315	.00	.00	441.30	.0-2	9788.0	.0
Roof	-14.97	24630	.00	.00	368.81	.0 -	8298.3	.0
Roof	-4.54	43103	.00	.00	195.85	.0 1	1751.2	.0
Total	.00	168623	1549.33	.00	1447.27	.0-1	17172.5	.0

Along Ridge - Base Reactions - Walls Only -GCpi

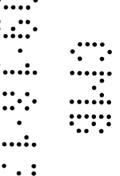
Description	Press psf			Fy Kip	Fz Kip	Mx K-ft	My K-ft	Mz K-ft
Leeward Wall	-14.97	24630	368.81	.00	.00	.0	-11064.4	.0
Side Wall	-25.40	13500	.00	342.96		10288.8	.0	.0
Side Wall	-25.40	13500	.00	-342.96	.00-	10288.8	.0	.0
Windward Wall	52.82	411	21.68	.00	.00	.0	-1290.2	.0
Windward Wall	52.70	411	21.63	.00	.00	.0	-1265.6	.0
Windward Wall	52.58	411	21.58		.00	.0	-1241.0	.0
Windward Wall	52.45	411		.00	.00		-1216.5	.0
Windward Wall	52.32	411	21.48		.00		-1192.1	.0
Windward Wall	52.20	411	21.43	.00	.00		-1167.7	.0
Windward Wall	52.06	411	21.37		.00		-1143.4	
Windward Wall	51.93	411		.00	.00		-1119.2	.0
Windward Wall	51.80	411	21.26	-00	.00		-1095.0	.0
Windward Wall	51.66	411		.00	-00		-1070.9	
Windward Wall	51.52		21.15	.00	.00		-1046.9	
Windward Wall	51.38	411		.00	.00		-1022.9	
Windward Wall	51.23		21.03	.00	.00		-999.0	
Windward Wall	51.09		20.97	.00	.00		-975.2	
Windward Wall Windward Wall	50.94		20.91	.00	.00		-951.4	
Windward Wall	50.79		20.85	.00	.00		-927.7	.0
Windward Wall	50.63 50.47		20.78	.00	.00		-904.1	
Windward Wall	50.47	411	20.72	.00			-880.6	.0
Windward Wall	50.15	411	20.65 20.59	.00	.00		-857.1 -833.7	
Windward Wall	49.98	411	20.52	.00	.00		-810.4	
Windward Wall	49.81		20.45	.00	.00		-787.2	
Windward Wall	49.64		20.38	.00			-764.1	.0
Windward Wall	49.46	411	20.30	.00	.00	۰۰	-741.0	.0
Windward Wall	49.28	411	20.23	.00	.00		-718.1	.0
Windward Wall	49.09	411	20.15	.00	.00		-695.2	.0
Windward Wall	48.90	411	20.07	.00	.00		-672.4	.0
Windward Wall	48.70		19.99	.00	.00		-649.8	.0
Windward Wall	48.50		19.91	.00	.00		-627.2	.0
Windward Wall	48.30	411	19.83	.00	.00	.0	-604.7	.0
Windward Wall	48.08	411	19.74	.00	.00 .00 .00	. 0	-582.3	.0
Windward Wall	47.87	411	19.65	.00	.00	.0	-560.0	. 0
Windward Wall	47.64	411	19.56	.00	.00	.0	-537.8	.0
Windward Wall	47.41	411	19.46	.00	.00	.0	-515.8	.0
Windward Wall	47.18	411	19.37	.00	.00	.0	-493.8	.0
Windward Wall	46.93	411	19.26	.00	.00		-472.0	.0
Windward Wall	46.68	411	19.16	.00	.00	.0	-450.3	.0
Windward Wall	46.41	411	19.05	.00			-428.7	. 0
Windward Wall	46.14	411	18.94	.00	.00	.0	-407.2	.0
Windward Wall	45.86		18.83	.00	.00	.0	-385.9	.0
Windward Wall	45.57		18.70	.00	.00		-364.7	.0
Windward Wall	45.26		18.58	.00	.00		-343.7	.0
Windward Wall	44.94		18.45	.00	.00		-322.8	.0
Windward Wall	44.61		18.31	.00	.00		-302.1	.0
Windward Wall	44.25		18.17	.00	.00		-281.6	.0
Windward Wall	43.88		18.01	.00	.00		-261.2	.0
Windward Wall	43.88		18.01	.00	.00		-243.2	.0
Windward Wall	43.88		18.01	.00	.00		-225.2	.0
Windward Wall Windward Wall	43.88 43.88		18.01	.00	.00		-207.2	.0
Windward Wall	43.88	411	18.01	.00	.00		-189.2	.0
mindward wall	43.68	411	10.01	.00	.00	. 0	-171.1	.0



Windward Wall	43.88	411	18.01	.00	.00	.0	-153.1	.0
Windward Wall	43.88	411	18.01	.00	.00	.0	-135.1	.0
Windward Wall	43.88	411	18.01	.00	.00	.0	-117.1	.0
Windward Wall	43.88	411	18.01	.00	.00	.0	-99.1	.0
Windward Wall	43.88	411	18.01	.00	.00	.0	-81.1	-0
Windward Wall	43.88	411	18.01	.00	.00	.0	-63.1	.0
Windward Wall	43.88	411	18.01	.00	.00	.0	-45.0	.0
Windward Wall	43.88	411	18.01	.00	.00	.0	-27.0	.0
Windward Wall	43.88	411	18.01	.00	.00	. 0	-9.0	.0
Total	.00	76260	1549.33	.00	.00	.0-	47810.4	.0

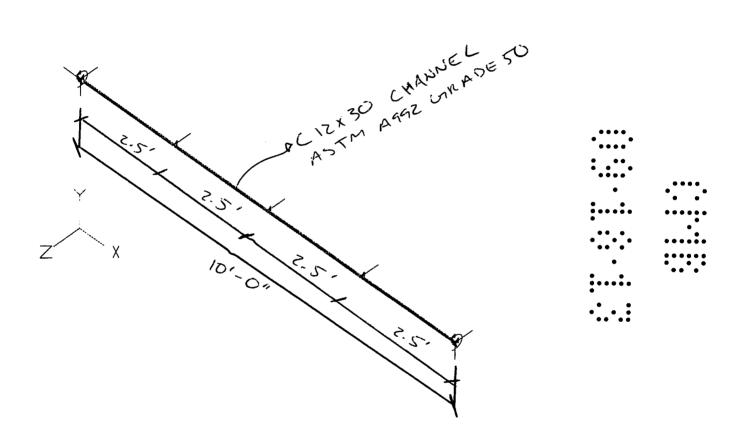
Along Ridge - Base Reactions - Walls+Roof MIN

Description	psf	Area* ft'2	Fx Kip	Fy Kip	Fz Kip	Mx K-ft	My K-ft	Mz K-ft
Windward Wall	9.60	411	3.94	.00	.00	.0	-234.5	.0
Windward Wall	9.60	411	3.94	.00	.00	.0	-230.5	.0
Windward Wall	9.60	411	3.94	.00	.00	.0	-226.6	.0
Windward Wall	9.60	411	3.94	.00	.00	.0	-222.7	.0
Windward Wall	9.60	411	3.94	.00	.00	.0	-218.7	.0
Windward Wall	9.60	411	3.94	.00	.00	.0	-214.8	.0
Windward Wall	9.60	411	3.94	.00	.00	.0	-210.8	.0
Windward Wall Windward Wall	9.60	411	3.94	.00	.00	.0	-206.9	.0
Windward Wall	9.60	411	3.94	.00	.00	٠.	-199 0	.0
Windward Wall	9.60	411	3.94	.00	.00	.0	-195.1	.0
Windward Wall	9.60	411	3.94	.00	.00	.0	-191.1	.0
Windward Wall	9.60	411	3.94	.00	.00	.0	-187.2	.0
Windward Wall	9.60	411	3.94	.00	.00	.0	-183.2	.0
Windward Wall	9.60	411	3.94	.00	.00	.0	-179.3	.0
Windward Wall	9.60	411	3.94	.00	.00	. 0	-175.4	.0
Windward Wall	9.60	411	3.94	.00	.00	.0	-171.4	.0
Windward Wall	9.60	411	3.94	.00	.00	• 0	-167.5	.0
Windward Wall Windward Wall	9.60	411	3.94	.00	.00	.0	-163.5	.0
Windward Wall	9.60	411	3.94	.00	.00	.0	-155 7	.0
Windward Wall	9.60	411	3.94	.00	.00	. 0	-151.7	.0
Windward Wall	9.60	411	3.94	.00	.00	.0	-147.8	.0
Windward Wall	9.60	411	3.94	.00	.00	.0	-143.8	.0
Windward Wall	9.60	411	3.94	.00	.00	.0	-139.9	.0
Windward Wall	9.60	411	3.94	.00	.00	.0	-136.0	.0
Windward Wall	9.60	411	3.94	.00	.00	.0	-132.0	.0
Windward Wall	9.60	411	3.94	.00	.00	. 0	-128.1	- 0
Windward Wall	9.60	411	3.94	.00	.00	.0	-124.1	.0
Windward Wall	9.60	411	3.94	.00	.00	.0	-120.2	.0
Windward Wall Windward Wall	9.60	411	3.94	.00	.00	. 0	-110.3	.0
Windward Wall	9.60	411	3.94	.00	.00	.0	-112.3	.0
Windward Wall	9.60	411	3.94	.00	.00	.0	-100.4	.0
Windward Wall	9.60	411	3.94	.00	.00	.0	-100.5	.0
Windward Wall	9.60	411	3.94	.00	.00	. 0	-96.5	.0
Windward Wall	9.60	411	3.94	.00	.00	.0	-92.6	.0
Windward Wall	9.60	411	3.94	.00	.00	.0	-88.7	.0
Windward Wall	9.60	411	3.94	.00	.00	.0	-84.7	.0
Windward Wall	9.60	411	3.94	.00	.00	.0	-80.8	.0
Windward Wall	9.60	411	3.94	.00	.00	.0	-76.8	.0
Windward Wall Windward Wall	9.60	411	3.94	.00	.00	.0	-72.9	.0
Windward Wall	9.60	411	3.94	.00	.00	. 0	-65.0	.0
Windward Wall	9.60	411	3.94	.00	.00	. 0	-61.1	.0
Windward Wall	9.60	411	3.94	.00	.00	. 0	-57.1	.0
Windward Wall	9.60	411	3.94	.00	.00	.0	-53.2	.0
Windward Wall	9.60	411	3.94	.00	.00	.0	-49.3	.0
Windward Wall	9.60	411	3.94	.00	.00	.0	-45.3	.0
Windward Wall	9.60	411	3.94	.00	.00	.0	-41.4	.0
Windward Wall	9.60	411	3.94	.00	.00	.0	-37.4	.0
Windward Wall Windward Wall	9.60	411	3.94	.00	.00	.0	-33.5	.0
Windward Wall	9.00	411	3.94	.00	.00	. 0	-25.6	.0
Windward Wall	9.60	411	3.94	.00	.00	. 0	-23.0	n
Windward Wall	9.60	411	3.94	.00	.00	.0	-17.7	.0
Windward Wall	9.60 9.60 9.60 9.60	411	3.94	.00	.00	.0	-13.8	.0
Windward Wall	9.60	411	3.94	.00	.00	.0	-9.9	.0
Windward Wall	9.60	411	3.94	.00	.00	.0	-5.9	.0
Windward Wall	9.60	411	3.94	.00	.00	.0	-2.0	.0
Roof	4.80	0	.00	.00	.00	.0	. 0	.0



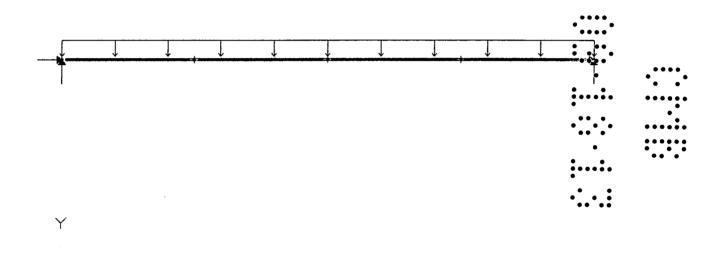
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## CIZX30 DESIGN

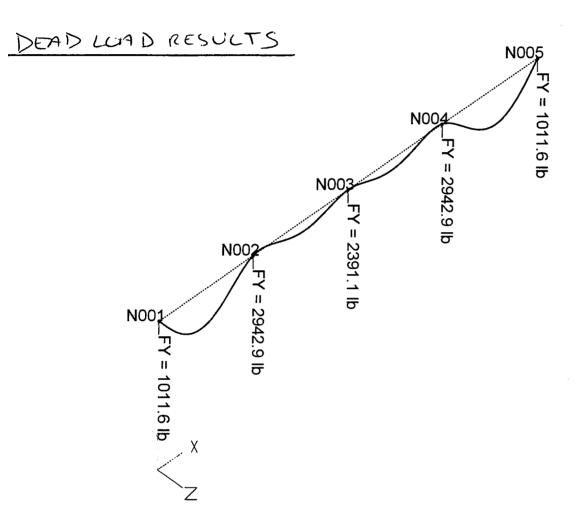


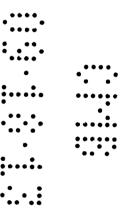
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YHCE Consulting Engineers, Youssef Hachem
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Load Case: D
IES VisualAnalysis 10.00.0008

DEAD LOAD



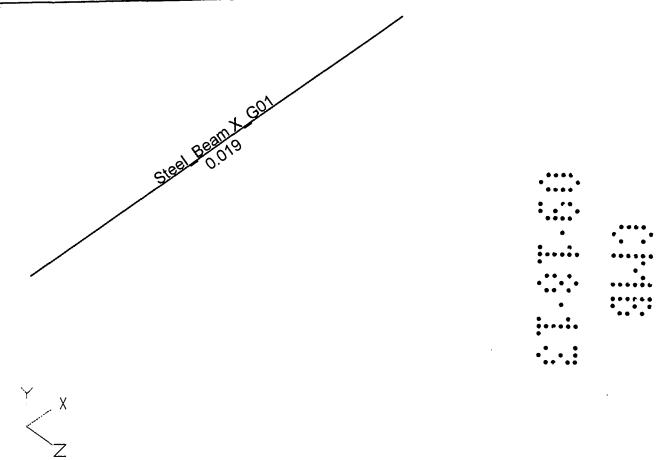
channel YHCE Consulting Engineers, Youssef Hachem Sep 03, 2013; 04:31 PM Result Case: D IES VisualAnalysis 10.00.0008

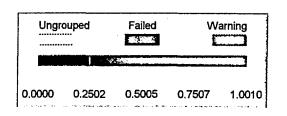




channel YHCE Consulting Engineers, Youssef Hachem Sep 03, 2013; 04:31 PM Design View, Unity Checks IES VisualAnalysis 10.00.0008

## DEAD LOAD DESIGN VIEW





Project: channel

Youssef Hachem, YHCE Consulting Engineers September 03, 2013

\\Win-server2008\d\2013\Beilinson and Gomez\E130160 (The Standard Hotel)\DESIGN PHASE\Calculations\Visual Analysis\

Design Criteria
Vertical Direction: Y, Ground Elevation = 0.00 ft

Occupancy Category: II

Seismic Data:

Spectral Acceleration (SDS) = 0.150 Seismic Design Category: A

Overstrength Omega0:X=2.5, Z=2.5 Seismic Redundancy Rho: X=1, Z=1

#### **Load Cases**

Load Case	Design Checks	Seismic Type	Results	Analyze?	Envelope?
( 1)D	-NA-	-NA-	Yes	Yes	No
(34)0.9D+Di	Strength (LRFD)	-NA-	Yes	Yes	No
(35)1.2D+0.5L+Lpa+0.5S+Di	Strength (LRFD)	-NA-	Yes	Yes	No
(36)1.4D+0.9H	Strength (LRFD)	-NA-	Yes	Yes	No
(37)D+L	Defl. 'Other'	-NA-	Yes	Yes	No

#### Member Extreme Results

Member	Fx (lc)	Vy (lc)	Vz (lc)	Mx (lc)	My (lc)	Mz (lc)
	lb	lb	lb	lb-ft	lb-ft	lb-ft
BmX005	0.0000 ( 1)	-2118.1141 (36)	-0.0000 (36)	0.0000 (1)	-0.0000 (36)	-695.4942 (36)
BmX005	0.0000 ( 1)	2188.8020 (36)	0.0000 (36)	0.0000 (1)	0.0000 (36)	965.6480 (36)

Member Unity Checks

Memb er	Unity Controlling Case	Check	Model Shape	Design Shape	Material	Referenc e	Specification	
BmX0 05	0.018 1.4D+0.9H 7	Strong Flexure Check	C12x30	C12x30	ASTM A992 Grade 50	F2-2	AISC LRFD (2005)	

**Nodal Extreme Displacements** 

Node	DX	DY	DZ
	in	in	• • in
N001	-NA-	-NA-	•••• -NA-
N001	-NA-	-NA-	-NA-
N002	0.0000 ( 1)	-NA-	-0.0000 (35)
N002	0.0000 ( 1)	-NA-	-0.0000 (36)
N003	0.0000 ( 1)	-NA-	-0.0000 (36)
N003	0.0000 ( 1)	-NA-	-0.0000 (35)
N004	0.0000 ( 1)	-NA-	-0.0000 (35)
N004	0.0000 ( 1)	-NA-	-0.0000 (36)
N005	-NA-	-NA-	-NA-
N005	-NA-	-NA-	-NA-

#### **Nodal Extreme Reactions**

Node	FX	FY	FZ	MX	MY	MZ
	lb	lb	lb	lb-ft	lb-ft	lb-ft
N001	0.0000 ( 1)	910.4681 (34)	-0.0000 (36)	0.0000 (1)	-NA-	-NA-
N001	0.0000 ( 1)	1416.2837 (36)	0.0000 ( 1)	0.0000 (1)	-NA-	-NA-
N002	-NA-	2648.6344 (34)	-NA-	-NA-	-NA-	-NA-
N002	-NA-	4120.0979 (36)	-NA-	-NA-	-NA-	-NA-
N003	-NA-	2152.0154 (34)	-NA-	-NA-	-NA-	-NA-
Ñ003	-NA-	3347.5796 (36)	-NA-	-NA-	-NA-	-NA-
N004	-NA-	2648.6344 (34)	-NA-	-NA-	-NA-	-NA-
N004	-NA-	4120.0979 (36)	-NA-	-NA-	-NA-	-NA-
N005	0.0000 ( 1)	910.4681 (34)	-0.0000 (36)	0.0000 ( 1)	-NA-	-NA-

Project: channel
Youssef Hachem, YHCE Consulting Engineers

September 03, 2013

\\Win-server2008\d\2013\Beilinson and Gomez\E130160 (The Standard Hotel)\DESIGN PHASE\Calculations\Visual

Analysis\

N005

0.0000 (1)

1416.2837 (36)

0.0000 (1)

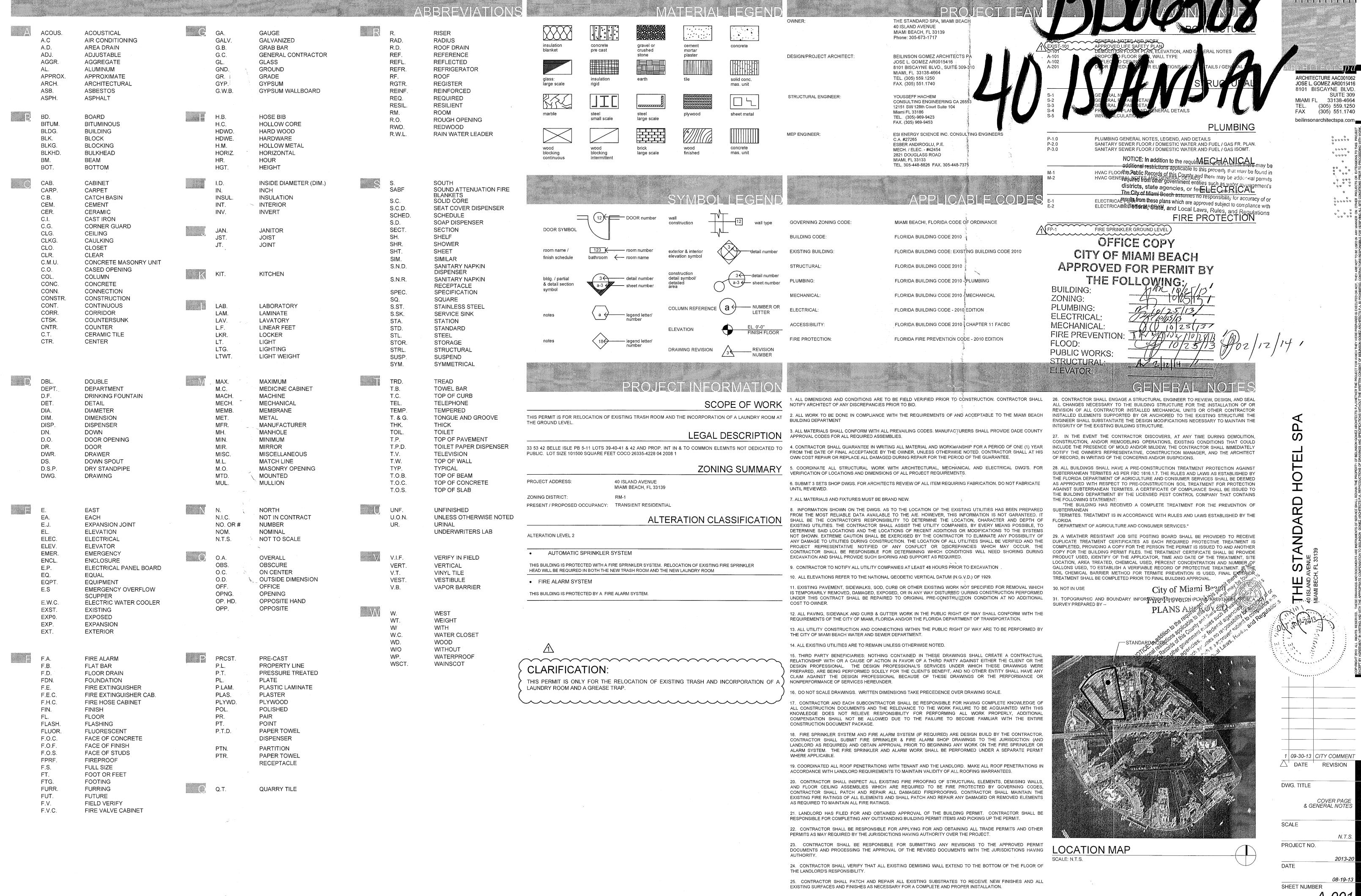
0.0000 (1)

-NA-

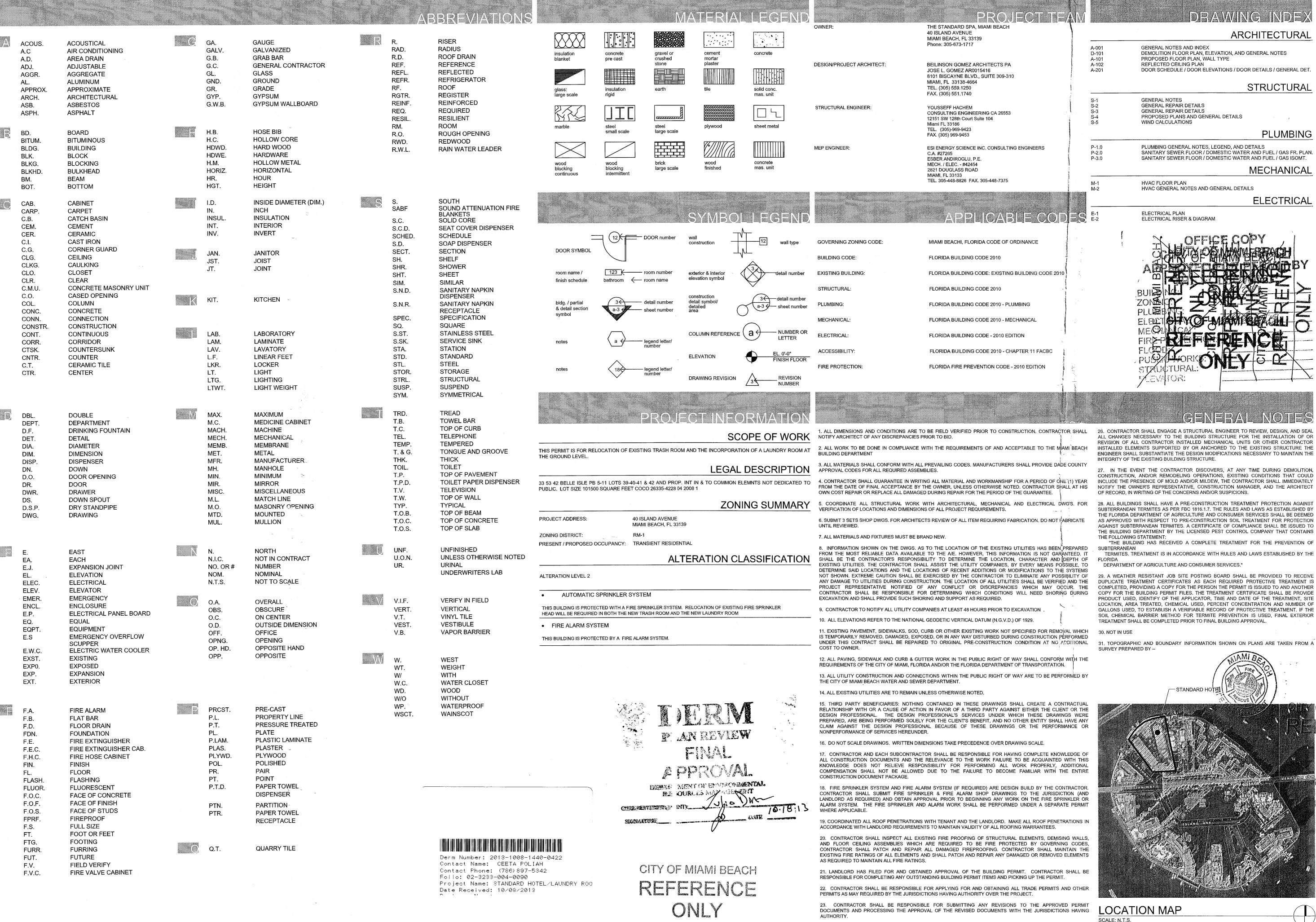
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WODAL EXTREME RESULTS

NOOZ JOU! 910 165 4170 165



8101 BISCAYNE BLVD. MIAMI FL 33138-4664 (305) 559.1250 (305) 551.1740



, , , GOME,Z

**ARCHITECTURAL** 

STRUCTURAL

PLUMBING

**MECHANICAL** 

**ELECTRICAL** 

ARCHITECTURE AAC001062 JOSE L. GOMEZ AR0015416 8101 BISCAYNE BLVD. MIAMI FI 33138-4664 TEL.

SUITE 309 (305) 559.1250 (305) 551.1740 beilinsonarchitectspa.com

TERMITES. TREATMENT IS IN ACCORDANCE WITH RULES AND LAWS ESTABLISHED BY THE DEPARTMENT OF AGRICULTURE AND CONSUMER SERVICES." 29. A WEATHER RESISTANT JOB SITE POSTING BOARD SHALL BE PROVIDED TO RECEIVE

DUPLICATE TREATMENT CERTIFICATES AS EACH REQUIRED PROTECTIVE TREATMENT IS COMPLETED. PROVIDING A COPY FOR THE PERSON THE PERMIT IS ISSUED TO AND ANOTHER COPY FOR THE BUILDING PERMIT FILES. THE TREATMENT CERTIFICATE SHALL BE PROVIDE PRODUCT USED, IDENTIFY OF THE APPLICATOR, TIME AND DATE OF THE TREATMENT, SITE LOCATION, AREA TREATED, CHEMICAL USED, PERCENT CONCENTRATION AND NUMBER OF GALLONS USED, TO ESTABLISH A VERIFIABLE RECORD OF PROTECTIVE TREATMENT. IF THE SOIL CHEMICAL BARRIER METHOD FOR TERMITE PREVENTION IS USED, FINAL EXTERIOR TREATMENT SHALL BE COMPLETED PRIOR TO FINAL BUILDING APPROVAL.

31. TOPOGRAPHIC AND BOUNDARY INFORMATION SHOWN ON PLANS ARE TAKEN FROM A SURVEY PREPARED BY -

24. CONTRACTOR SHALL VERIFY THAT ALL EXISTING DEMISING WALL EXTEND TO THE BOTTOM OF THE FLOOR OF

25. CONTRACTOR SHALL PATCH AND REPAIR ALL EXISTING SUBSTRATES TO RECEIVE NEW FINISHES AND ALL

EXISTING SURFACES AND FINISHES AS NECESSARY FOR A COMPLETE AND PROPER INSTALLATION.



∠ DATE

DWG. TITLE

SCALE PROJECT NO.

DATE

REVISION

COVER PAGE & GENERAL NOTES

N.T.S

## GENERAL DEMOLITION NOTES:

#### 1 - SCOPF

FURNISH EQUIPMENT AND PERFORM LABOR REQUIRED TO EXECUTE THIS WORK AS INDICATED ON THE DRAWINGS, AS SPECIFIED AND NECESSARY TO COMPLETE THE CONTRACT, INCLUDING BUT NOT LIMITED TO, THESE MAJOR ITEMS.

A.- PROTECTION OF EXISTING WORK TO REMAIN.
B.- TEMPORARY BARRICADES.

C.- REMOVAL, STORAGE AND PROTECTION OF ITEMS TO BE REUSED.

D.- REMOVAL OF PARTITIONS, DOORS, FLOOR COVERINGS AND CEILINGS AS INDICATED.
E.- REMOVAL OF MECHANICAL AND ELECTRICAL FIXTURES AND SERVICES AS INDICATED.
F.- DEBRIS REMOVAL.

#### 2.- GENERAL REQUIREMENTS:

A- FIELD CONDITIONS: TAKE INTO CONSIDERATION AS NECESSARY WORK, ALL OBVIOUS EXISTING CONDITIONS AND INSTALLATIONS OF THE SITE AS THOUGH THEY WERE COMPLETELY SHOWN OR DESCRIBED.

B- ALL CONTRACTORS SUBMITTING PROPOSALS FOR THIS WORK SHALL FIRST EXAMINE THE SITE AND ALL CONDITIONS AND LIMITATIONS THEREON AND THEREABOUTS. ALL PROPOSALS SHALL TAKE INTO ACCOUNT ALL SUCH CONDITIONS AND LIMITATIONS WHETHER OR NOT THE SAME ARE SPECIFICALLY SHOWN OR MENTIONED IN ANY OF THE CONTRACT DOCUMENTS AND EVERY PROPOSAL SHALL BE CONSTRUED AS INCLUDING WHATEVER SUMS ARE NEEDED TO COMPLETE THE WORK IN EVERY PART AS SHOWN, DESCRIBED OR REASONABLY REQUIRED OR IMPLIED, AND ATTAIN THE COMPLETED CONDITIONS CONTEMPLATED BY THE CONTRACT.

C- CONFER WITH ON SITE PROPERTY MANAGER AS TO DISPOSITION OF MATERIALS WHICH S(HE) MAY WISH TO RETAIN. SPECIFICALLY INCLUDED EQUIPMENT AND DOORS OF ALL TYPES. IF ON SITE MANAGER ELECTS TO RETAIN ANY OF THE REMOVED ITEMS, PROTECT AND STORE AS DIRECTED BY MANAGER AT MANAGER'S EXPENSE.

D- CODES: PERFORM ALL WORK IN ACCORDANCE WITH THE BUILDING CODE OF THE GOVERNING BODY HAVING JURISDICTION, THE GOVERNING STATE INDUSTRIAL SAFETY ORDERS AND THE REQUIREMENTS OF THE OCCUPATIONAL SAFETY AND HEALTH ACT.

E- UNFORESEEN CONDITIONS: INCLUDE IN THE BASE BID MISCELLANEOUS CUTTING AND PATCHING NECESSITATED AS A RESULT OF UNFORESEEN CONDITIONS AND THE WORKING OF ABUTTING SURFACES AS REQUIRED TO MAKE NEW WORK JOIN AND MATCH EXISTING SURFACES TO REMAIN. NO EXTRA PAYMENTS BASED ON THE PLEA OF UNFORESEEN CONDITIONS WILL BE ALLOWED.

F- PHASING OF THE WORK: CONFER WITH THE ARCHITECT AS TO THE SEQUENCING AND THE PHASING OF VARIOUS PARTS OF THE WORK. COOPERATE FULLY TO THE END THAT CERTAIN FACILITIES AND SERVICES ARE MAINTAINED IN OPERATION UNTIL IMMEDIATELY BEFORE THEIR REMOVAL IS REQUIRED TO PERMIT INSTALLATION OF NEW WORK.

#### 3.- SITE PROTECTION:

A- BARRIERS: TEMPORARY BARRIERS ARE TO BE FURNISHED.

B- GLASS: PROVIDE SUCH PROTECTION AS MAY BE REQUIRED TO PREVENT GLASS
BREAKAGE. AT NO ADDITIONAL COST REPLACE ALL BROKEN GLASS.

CORRESPONDED TO THE PROPERTY OF THE PRO

C- PROTECTION OF PERSONNEL: ERECT SIGNS, BARRICADES AND SUCH OTHER FORMS OF WARNING AS MAY BE REQUIRED TO PREVENT PERSONNEL FROM PUTTING THEMSELVES IN THE WAY OF INJURY.

D- EXISTING WORK TO REMAIN: PROVIDE SUCH FORMS OF PROTECTION AS MAY BE NECESSARY TO PREVENT DAMAGE TO EXISTING WORK AND EQUIPMENT TO REMAIN. E- ITEMS TO BE REUSED: EXERCISE THE GREATEST POSSIBLE CARE WHEN REMOVING ITEMS SCHEDULED FOR REUSE. USE ONLY MECHANICS SKILLED IN THE APPROPRIATE TRADES. IDENTIFY POINT OF REUSE, STORE AND PROTECT AT LOCATIONS DIRECTED.

#### 4.- GENERAL DEMOLITION:

A- DOORS AND HARDWARE: REMOVE CAREFULLY TO AVOID DAMAGE. IN SO FAR AS POSSIBLE, LEAVE HARDWARE ATTACHED TO THE DOOR. WHERE THIS IS NOT PRACTICAL PLACE ITEMS OF HARDWARE IN A CLOTH BAG ATTACHED TO THE DOOR.

B- PARTITIONS: REMOVE PARTITION FINISH, STUDS, PLATES AND SILL, WHERE ONLY A PARTIAL RUN IS REMOVED, CUT BACK FINISH MATERIALS TO THE CENTERLINE OF THE NEXT ADJACENT SPACE SUPPORT TO REMAIN. LEAVE REMAINING MATERIALS WITH A CLEAN TERMINAL LINE WITH NO LOOSE MATERIAL ADHERING. WHERE PARTITIONS HAVE BEEN INSTALLED ON CURBS, REMOVE CURBS AND PATCH EXISTING FLOOR TO RECEIVE NEW

C- RESILIENT FLOOR TILE: REMOVE ALL FLOOR TILE. REMOVE ALL ADHESIVE USING SOLVENTS AND/OR GRINDING AS REQUIRED. LEAVE FLOOR READY TO RECEIVE NEW FINISH MATERIALS. PATCH AND REPAIR CONCRETE FLOOR.

D- CONCRETE AND MASONRY: CORE DRILL ONLY NOT LESS THAN 1 ½" AT LINES OF REMOVAL. BREAKOUT SECTIONS TO BE REMOVED. CHOP BACK FACE BEHIND SAW OUT LINES

E- ALL LIFE SAFETY COMPONENTS SHALL REMAIN IN PLACE & OPERATING THIS INCLUDES, FIRE SPRINKLERS, FIRE ALARM DEVICES, EMERGENCY LIGHTING, FIRE AND SMOKE

F- DO NOT REMOVE ANY STRUCTURAL WALLS (LOAD BEARING OR SHEAR WALLS) OR OTHER STRUCTURAL ELEMENTS UNLESS SPECIFICALLY AS NOTED AS STRUCTURAL ELEMENT TO BE REMOVED. NOTIFY >>>> PROJECT MANAGER IF ANY STRUCTURAL ELEMENTS ARE DISCOVERED AND NOTED TO BE REMOVED AND NOT NOTED AS STRUCTURAL ELEMENTS.

#### 5.- MECHANICAL AND ELECTRICAL:

6 - REMOVED MATERIALS AND OTHER DEBREE:

A- CAREFULLY REVIEW PLANS AND DETERMINE LINES TO BE REMOVED AND THOSE TO BE KEPT ACTIVE OR TO BE REACTIVATED. PROTECT LINES TO REMAIN. PROVIDE FOR MINIMUM SERVICE INTERRUPTION OF LINES TO REMAIN. (CONFER WITH ON SITE PROPERTY MANAGER).

B- REMOVE ALL LIGHT FIXTURES AND EQUIPMENT UNLESS OTHERWISE NOTED. WHEN INDICATED FOR REUSE, CLEAN, STORE AS DIRECTED AND PROTECT. IDENTIFY POINT OF REUSE

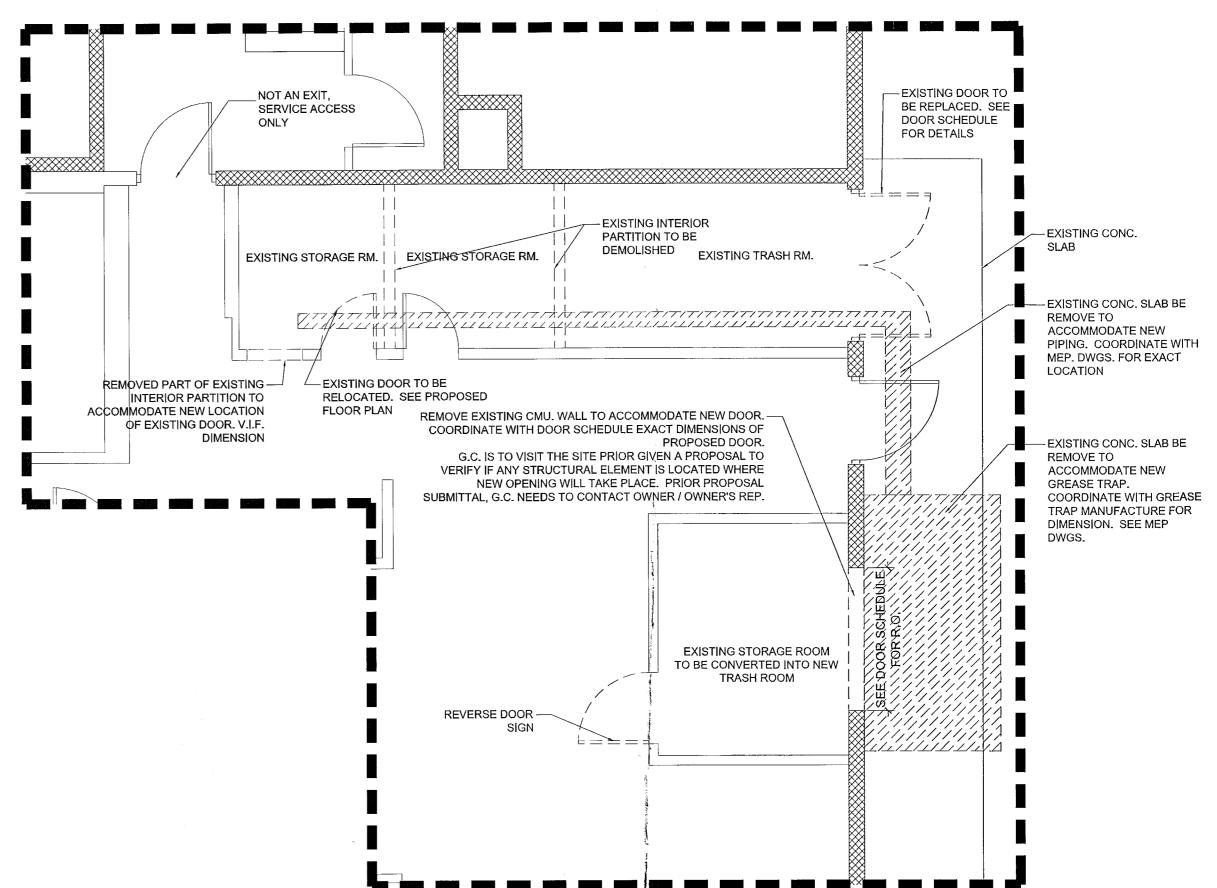
C- REMOVE LINES COMPLETELY WHEREVER POSSIBLE. CUT AND CAP OR PLUG IN A POSITIVE MANNER BEHIND THE RACK OF FINISH MATERIAL.

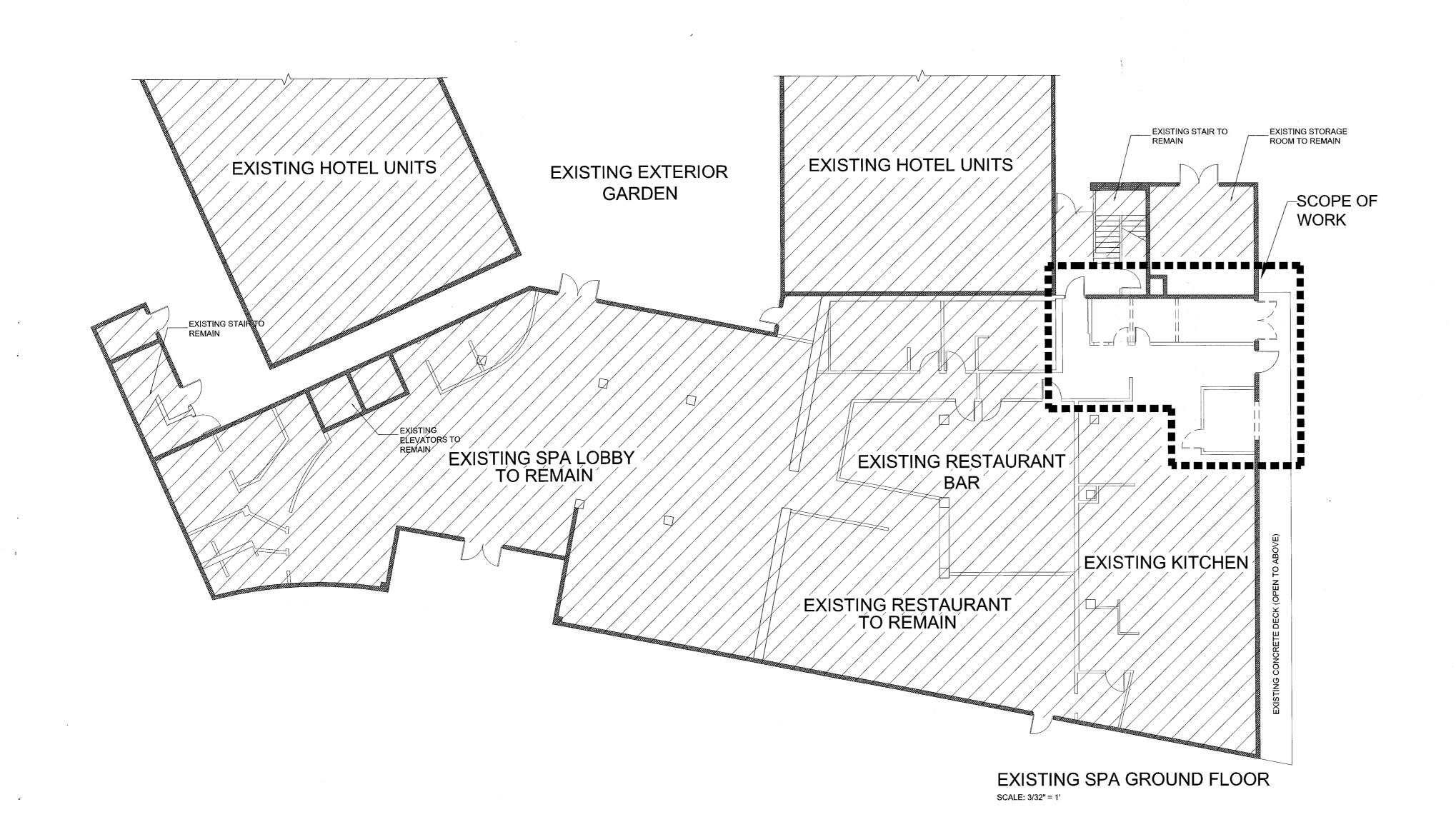
D- WHEN UTILITIES ARE REMOVED, CAP AND SEAL A MINIMUM OF 8" BELOW FINISH FLOOR OR A MINIMUM OF 6" ABOVE FINISH CEILING.

A- ALL REMOVED MATERIAL, NOT OTHERWISE DESIGNATED, AND ALL DEBRIS BECOMES THE PROPERTY OF THE CONTRACTOR WHO SHALL REMOVE IT FROM THE SITE.

B- DO NOT ALLOW MATERIALS AND DEBRIS GENERATED BY DEMOLITION ACTIVITIES TO ACCUMULATE. REMOVE DAILY AND DISPOSE OF IN A LEGAL MANNER.

C- LEAVE ALL SPACES BROOM CLEAN AND WITH ALL LEDGES AND CORNERS PROPERLY







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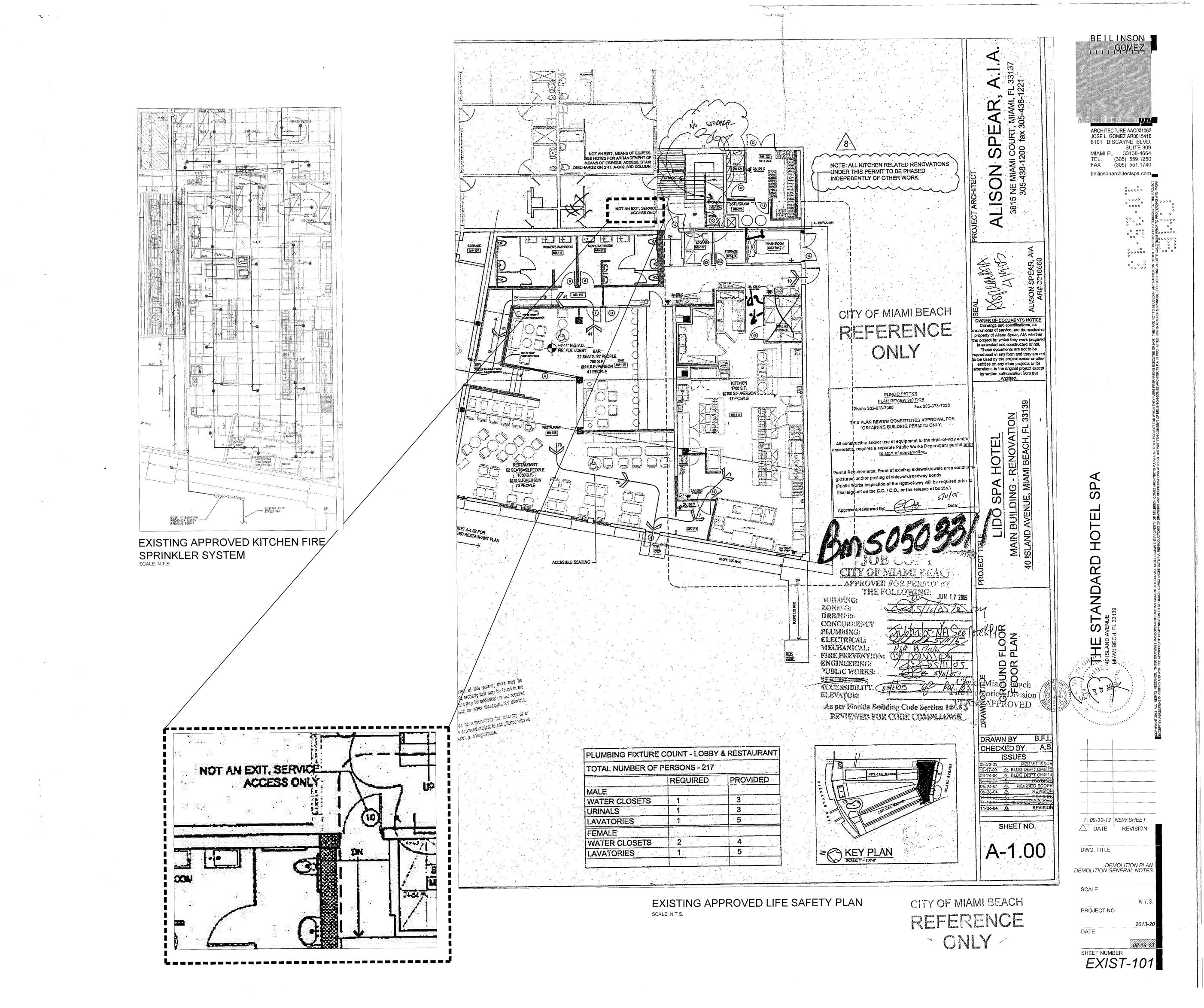
TEL.

FAX

SUITE 309

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(305) 551.1740



1. Floor and Ceiling Runners — (Not shown) — For use with Item 2 — Channel shaped, fabricated from min 25 MSG corrosion—protected steel, min depth to accommodate stud size, with min 1—1/4 in long legs, attached to floor and ceiling with fasteners 24 in OC max.

1A. Framing Members\* — Floor and Ceiling Runners — Not shown — In lieu of Item 1 — For use with Item 2A, proprietary channel shaped, min. 3—5/8 in. deep, fabricated from min. 0.015 in. (min bare mate) this latest at the state of the stat metal thickness) galvanized steel, attached to floor and celling with fasteners 24 in. OC max. Effective thickness is 0.034 in. CLARKWESTERN BUILDING SYSTEMS INC — UltraSTEEL®

DIETRICH INDUSTRIES INC - UItraSTEEL® The Frank House Res Not — Utros Ret. at 19. Frank House 19. Fr

DIETRICH INDUSTRIES INC — UltroSTEEL.©.

10. Framing Members\* — Floor and Celling Runner — Not shown — In lieu of item 1 — For use with item 2C, proprietary channel shaped runners, 3—5/8 in. deep attached to floor and celling with fasteners 24 in. OC max.

CALIFORNIA EXPANDED METAL PRODUCTS CO — ViperTrack™

CRACO MFG INC - SmartTrack™

F. C. L.

MARINO/WARE\_DIV\_OF\_WARE\_INDUSTRIES
INC — Viper25™ Track
IELLING INDUSTRIES L L C — Viper25™ Track
1D. Framing Members\* — Floor and Ceiling Runner — Not shown — in Ileu of Item 1 — For use with
Item 2D, proprietory channel shaped runners, 1—1/4 in, wide by 3—5/8 in, deep fabricated from min
0.020 in, thick gaiv steel, attached to floor and ceiling with fasteners spaced 24 in, OC max.

MARINO/WARE\_DIV\_OF\_WARE\_NDV\_Track
IELLING INDUSTRIES L L C — Viper200™ Track
IELLING INDUSTRIES L L C — Viper205™ Track, Viper200™ Track
IE. Framing Members\*—Floor and Ceiling Runners — (Not shown) — in Ileu of Item 1 — Channel
shoped, attached to floor and ceiling with fasteners 24 in, OC, max.

ALLSTEEL & GYPSUM PRODUCTS INC — Type SUPREME Framing System
CONSOLIDATED FABRICATORS CORP,
BUILDING PRODUCTS DIV — Type SUPREME Framing System
SCAFCO STEEL STUD MANUFACTURING CO — Type SUPREME Framing System
SCAFCO STEEL STUD MANUFACTURING CO — Type SUPREME Framing System
STEEL CONSTRUCTION SYSTEMS INC — Type SUPREME Framing System
UNITED METAL PRODUCTS INC — Type SUPREME Framing System
IF. Floor and Ceiling Runners — (Not shown)—For use with Item 2B— Channel shaped, fabricated from
min 20 MSG corrosion—protected or gaiv steel, min depth to accommodate stud size, with min 1 in.
long legs, attached to floor and ceiling with fasteners spaced max 24 in, OC,

1G. Framing Members\*— Floor and Ceiling Runners — (Not shown, As an alternate to Item 1) — For
use with Item 2F and 5F or 56 only, channel shaped, fobricated from min, 0.015 in, (min bare metal
thickness) gaivanized steel, attached to floor and ceiling with fasteners 24 in, OC, max.

DIETRICH INDUSTRIES INC — DIETRICH ProTRAK

MBA BUILDING SYSTEMS INC — DETRICH ProTRAK

MBA BUILDING SYSTEMS INC — DETRICH ProTRAK

SOUTHEASTERN BUILDING SYSTEMS INC — CW ProTRAK

SOUTHEASTERN BUILDING SYSTEMS INC — CW ProTRAK

1H. Framing Members\* — Floor and Ceiling Runner — Not shown — In Ileu of Item 1 — For use with Item 2G, proprietary channel shaped runners, minimum width to accommodate stud size, with 1— 1/8 in. long legs fabricated from min 0.015 in. (min bare metal thickness) gaiv steel, attached to floor and ceiling with fasteners spaced 24 in. OC max.

SUPER STUD BUILDING PRODUCTS — The Edge
2. Steel Stude — Channel shaped, fabricated from min 25 MSG corrosion—protected steel, min depth as indicated under item 5, spaced a max of 24 in. OC. Studs to be cut 3/8 to 3/4 in. less than assembly helaht. as intolated under item 5, spaced a max of 24 in. OC. Stude to be cut 3/8 to 3/4 in. less than assembly height.

2A. Framing Members\* — Steel Stude — in lieu of item 2 — Proprietary channel shoped stude, min. depth as indicated under item 5, fobricated from min. O(0.15 in. (min bare metal thickness) galvanized steel, spaced a max of 24 in. OC. Stude to be cut 3/4 in. less than assembly height. Allowable use of stude is shown in the table below. For direct attachment of gypsum board only. Effective thickness is 0.034 in.

CLARKWESTERN BUILDING SYSTEMS INC — UltraSTEFL®

DIETRICH INDUSTRIES INC — UltraSTEEL®,
2B. Steel Stude — (As an alternate to Item 2, For use with Items 58 & 5E) Channel shaped, fabricated from min 20 MSG corrosion—protected or galv steel, 3—1/2 in. min depth, spaced a max of 16 in. OC. Stude friction—fit into floor and ceiling runners. Stude to be cut 5/8 to 3/4 in. less than constribly balabit. of 16 in. OC. Stude friction—fit into floor and ceiling runners. Stude to be cut by a to by fin. less than assembly height.

2C. Framing Members\* — Steel Stude — (As an alternate to item 2, For use with item 5C) — Proprietary channel shaped stude, 3—5/8 in. deep spaced a max of 24 in. OC. Stude to be cut 3/4 in less than the assembly height and installed with a ½ in. gap between the end of the stud and track at the bottom of the wall. For direct attachment of gypsum board only.

CALIFORNIA EXPANDED METAL PRODUCTS CO — ViperStud M

CRACO MFG INC — SmartStud™

MARINO/WARE, DIV OF WARE INDUSTRIES INC — Viper25 TM

TELLING INDUSTRIES L L C --- Viper25™

2D. Framing Members\* — Metal Stude — Not shown — in lieu of item 2 — For use with item 1D, proprietary channel shaped steel stude, min depth as indicated under item 5, spaced a max if 24 in. CC, fabricated from min 0.020 in. thick galv steel. Stude cut 3/8 in. to 3/4 in. less in lengths than assembly heights. MARINO/WARE, DIV OF WARE INDUSTRIES INC — Viper20S™, Viper20D™

TELLING INDUSTRIES L L C — Viper20S™, Viper20D™

2E. Framing Members\*— Steel Studs — in lieu of Item 2 — For Use with Item 1E— Channel shaped studs, min depth as indicated under Item 5, spaced a max of 24 in. OC. Studs to be cut 3/4 in. less than assembly height.

ALLSTEEL & GPSUM PRODUCTS INC — Type SUPREME Framing System
CONSOLIDATED FABRICATORS CORP.
BUILDING PRODUCTS DIV — Type SUPREME Framing System
GUAIL RUN BUILDING MATERIALS INC — Type SUPREME Framing System
SCAFCO STEEL STUD MANUFACTURING CO — Type SUPREME Framing System
STEL. CONSTRUCTION SYSTEMS INC — Type SUPREME Framing System
UNITED METAL PRODUCTS INC — Type SUPREME Framing System
2F. Framing Members\*— Steel Studs — (Not shown, As an alternate to Item 2) —For use with Item 1G and 5F or 5G only, channel shaped studs, min depth as indicated under Item 5F, fabricated from min. 0.015 in. (min bare metal thickness) galaxiazed steel, spaced a max of 24 in. OC. Studs to be cut 3/4 in. less than assembly height. CLI 3/4 In. leas than assembly height.

CLARKWESTERN BUILDING SYSTEMS INC — CW ProSTUD

DIETRICH INDUSTRIES INC — DIETRICH PROSTUD

DIMFCWBS L L C — PROSTUD

MBA BUILDING SUPPLIES — PROSTUD

SOUTHEASTERN STUD & COMPONENTS INC — PROSTUD

TELLING INDUSTRIES L L C — TRUE-STUD THE

2G. Framing Members\* — Metal Stude — Not shown — In Ileu of Item 2 — For use with Item 1H, proprietary channel shaped steel stude, minimum width indicated under Item 5, 1—1/4 in, deep fabricated from min 0.015 in. (min bare metal thickness) galvanized steel. Stude 3/8 in, to 3/4 in, less in lengths than assembly heights.

SUPER STUD BUILDING PRODUCTS — The Edge
3. Wood Structural Panel Sheathing — (Optional, For use with Item 5 Only.)— (Not Shown) — 4 ft wide, 7/16 in, thick oriented strand board (OSB) or 15/32 in, thick structural 1 sheathing (plywood) complying with DOC PS1 or PS2, or APA Standard PRP—10B, manufactured with exterior glue, applied horizontally or vertically to the steel stude. Vertical joints centered on stude, and staggered one stud space from wellboard joints. Attached to stude with fifter-head self-drilling toping acrews with a min, head dlam, of 0.292 in, at maximum 6 in, OC, in the perimeter and 12 in, OC, in the field. When used, fastener lengths for gypsum panels increased by min, 1/2 in.

4. Batts and Blankets\* — (Required as indicated under Item 5) — Mineral wool batts, friction fitted between stude and runners. Min norm thickness as indicated under Item 5. See Batts and Blankets (BKNV or BZJZ) Categories for names of Classified companies.

4A. Batts and Blankets\* — (Optional) — Placed in stud cavities, any glass fiber or mineral wool insulation bearing the UL Classified too Marking as to Surface Burning Characteristics and/or Fire Resistance. See Batts and Blankets (BKNV or BZJZ) Categories for names of Classified companies.

5. Gypsum Board\* — Gypsum panels with beveled, equare or tapered edges, applied vertically or horizontally. Vertical joints centered over stude and staggered one stud cavity, opposite sides of stude. Vertical joints in adjacent layers (multilayer systems) staggered one stud cavity, horizontal butt joints on opposite sides of stude need not be staggered. Horizontal edge joints and horizontal butt joints on opposite sides of stude need not be staggered a min of 12

USE MOISTURE RESISTANCE GYPSUM BOARD ON WET LOCATIONS

	Wallboard Protect	ion on Each Side	e Wall	
Rating, Hr	Min stud Depth, in Items 2,2d,2E, and 2G	Min stud Depth, in Items 2A	No. of Layers & Thkns of Panel	Mi Thkn Insula (Item
1	3-1/2	3-5/8	1 layer, <sup>5</sup> in. thick	Optio
1	2-1/2	3-5/8	1 layer, 1/2 in. thick	1-1/2
1	1-5/8	3-5/8	1 layer, 3/4 in. thick	Optio
2	1-5/8	2-1/2	2 layer, 1/2 in. thick	Optio
2	1-5/8	2-1/2	2 layer, 5/8 in. thick	Optio
2	3-1/2	3-5/8	1 layer, 3/4 in. thick	3 in.
3	1-5/8	2-1/2	3 layers, 1/2 in. thick	Optio
3	1-5/8	2-1/2	2 layers, 3/4 in. thick	Optio
3	1-5/8	2-1/2	3 layers, 5/8 in. thick	Optio
4	1-5/8	2-1/2	4 layers, 5/8 in. thick	Optio
4	1-5/8	2-1/2	4 layers, 1/2 in. thick	Optio
4	2-1/2	2-1/2	2 layers, 3/4 in. thick	2 in.
ED STATES GYPS	OMPANY 1/2 in. thick Type C, IP-X2 or RX or WRC; 3/4 in. thick Type C, IP-X2 in DM CO 1/2 in. thick Type C, IP-X2, IPC L IPC-AR; 3/4 in. thick Type IP-X3 or C V 1/2 in. thick Type C, IP-X2, IPC-X	ULTRACODE -AR or WRC; 5/8 in. (	thick Type SCX, SHX, WRX, IP-X1,	AR, C, WE

SCX, SHX, WRX, WRC or; 3/4 in, thick Types IP-X3 or ULTRACODE 8. Joint Tape and Compound — Vinyl or casein, dry or premixed joint compound applied in two coats to joints and screw heads of outer layers. Paper tape, norn 2 in. wide, embedded in first layer of compound over all joints of auter layer panels. Paper tape and joint compound may be omitted when gypsum panels are supplied with a square edge.

IPC-AR, SCX, SHX, WRX or WRC; 3/4 in. thick Types IP-X3 or ULTRACODE UNITED STATES GYPSUM CO - 1/2 in. thick Type C, IP-X2, IPC-AR or WRC; 5/8 in. thick Type SCX, SHX, WRX, IP-X1, AR, C, WRC, FRX-G, IP-AR, IP-X2, IPC-AR; 3/4 in. thick Types IP-X3 or ULTRACODE

UNITED STATES GYPSUM CO — 1/2 in. thick Type C, IP—X2, IPC—AR or WRC; 5/8 in. thick Type SCX, SHX, WRX, IP—X1, AR, C, WRC, FRX—G, IP—AR, IP—X2, IPC—AR or WRC; 5/8 in. thick Type RP—X3 or ULTRACODE
USG MEXICO S A DE C V — 1/2 in. thick Type C, IP—X2, IPC—AR or WRC; 5/8 in. thick Type AR, C, IP—AR, IP—X1, IP—X2, IPC—AR, SCX, SHX, WRX, WRC or; 3/4 in. thick Types IP—X3 or ULTRACODE
When Item 78, Steel Framing Members\*, is used, Nonbearing Wall Rating is limited to 1 Hr. Min. stud depth is 3—1/2 in., min. thickness of insulation (item 4) is 3 in., and two layers of gypsum board panels (1/2 in. or 5/8 in. thick) shall be attached to furring channels as described in Item 6. One layer of gypsum board panels (1/2 in. or 5/8 in. thick) attached to opposite side of stud without furring channels as described in Item 6.

SA. Gypsum Board\* — (As an alternate to Item 5) — 5/8 in. thick, 24 to 54 in. wide, applied horizontally as the outer layer to one side of the assembly. Secured as described in Item 6.

SA. Gypsum Board\* — (Not Shown) — As an alternate to item 5 when used as the base layer on one or both sides of wall when 5/8 in or 7% in. thick products are specified. For direct attachment only to steel stude Item 25, inot to be used with Item 3 — Non 5/8 in. or 1% in. may be used as alternate to all 5/8 in. or 1% in. shown in Item 5, Wallboard Protection on Each Side of Wall table.

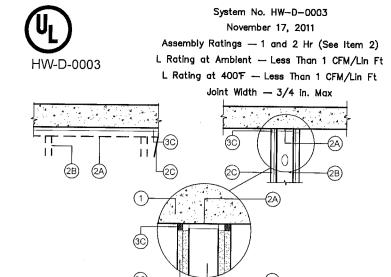
Non 5/8 in. or 1% in. thick lead backed gypsum panels with beveled, square or tapered edges, applied vertically. Vertical Joints centered over stude and staggered min 1 stud cavity on opposite sides of stude. Gypsum board secured to 20 MSG steel stude item 28 with 1—1/4 in. long Type 5—12 steel screws spaced 8 in. OC at primeter and 12 in. OC in the field. To be used with Ited Batten Strips (ase Item 11) or Lead Dilacs or Tabs (ase Item 12).

SAY—BAR ENGINEERING CORP — Type RB—LIEG

SC. Gypsum Board\* — (For Use With Item 2C) Rating Limited to 1 Hour. 5/8 in. thick, 48 in. wide, Gypsum panels with bevoled, square or tapered edges, applied vert

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WALL TYPE 1 (1HR RATED)



1. Floor Assembly - Min 4-1/2 in. (114 mm) thick steel-reinforced lightweight or normal weight (100-150 per or 1600-2400 kg/m3) structural concrete.

2. Wall Assembly — The 1 or 2 hr fire-rated gypsum board/stud wall assembly shall be constructed of the materials and in the manner described in the individual U400 or V400 Series Wall or Partition Design in the UL Fire Resistance Directory and shall include the following construction features:

A. Steel Floor and Celling Runners — Floor and celling runners of wall assembly shall consist of galv steel channels sized to accommodate steel studs (Item 2B) with min 1-1/4 in. (32 mm) to max 2 in. (51 mm) flanges. When deflection channel (Item 3A) is used, flange height of ceiling runner is to be equal to or greater than flange height of deflection channel and the ceiling runner is to nest within the deflection channel with a 1/2 in. to 3/4 in. (13 to 19 mm) gap maintained between the top of the ceiling runner and the top of the deflection channel. When deflection channel is not used, ceiling runner is secured to concrete floor with steel fasteners spaced max 24 in. (610 mm) OC.

in. (610 mm) OC.

A1. Light Gauge Framing\* — Slotted Celling Runner — As an alternate to the celling runner in Item 2A, celling runner to consist of galv steel channel with slotted flanges sized to accommodate steel studs (Items 2B). Celling runner secured to bottom of concrete floor with steel fasteners spaced max 24 in. (610 mm) OC. When slotted

concrete floor with steel fasteners spaced max 24 in. (610 mm) OC. When slotted celling runner is used, deflection channel (Item 3A) shall not be used.

CALIFORNIA EXPANDED METAL PRODUCTS

COMPANY — CST

SCAFCO STEEL STUD MANUFACTURING CO

SLIPTRACK SYSTEMS INC — SLP—TRK

METAL—LITE INC — The System

A2. Light Gauge Framing\* — Vertical Deflection Ceiling Runner — As an alternate to the ceiling runner in Item 2A, vertical deflection ceiling runner to consist of galv steel channel with slotted vertical deflection clips mechanically fastened within runner. Slotted clip provided with step bushings for permanent fastening of steel studs. Flanges sized to accommodate steel studs (Item 2B). Vertical deflection ceiling runner secured to floor with steel fasteners spaced max 24 in. (610 mm) OC. When vertical secured to floor with steel fasteners spaced max 24 in. (610 mm) OC. When vertical deflection ceiling runner is used, deflection channel (Item 3A) shall not be used. THE STEEL NETWORK INC — VertiTrack VTD362, VTD400, VTD600 and VTD800 A3. Light Gauge Framing\* — Clipped Ceiling Runner — As an alternate to the ceiling runner in Item 2A, clipped runner to consist of galv steel channel with clips preformed in teach of the ceiling runner in Item 2A, clipped runner to consist of galv steel channel with clips preformed in teach of the ceiling runner in Item 2A, clipped runner to consist of galv steel channel with clips preformed in teach of the ceiling runner in Item 2A, clipped runner to consist of galv steel channel with clips preformed in teach of the ceiling runner in Item 2A, clipped runner to consist of galv steel channel with clips preformed in the ceiling runner in Item 3A) shall not be used. in track flanges which positively engage the inside flange of the steel studs (Item 2B). Track sized to accommodate steel studs (Item 2B). Track flanges to be min 2-3/4 in. (70 mm) Clipped ceiling runner secured to floor with steel fasteners spaced max 2 in. (305 mm) OC. When clipped celling runner is used, deflection channel (Item 3A) shall not be used.

TOTAL STEEL SOLUTIONS L L C — Snap Trak

B. Studs — Steel studs to be min 3-1/2 in. (89 mm) wide. Studs cut 1/2 in. to 3/4 in. (13 to 19 mm) less in length than assembly height with bottom nesting in and secured to floor runner and with top nesting in ceiling runner without attachment. When deflection channel (Item 3A) is used, steel studs attached to ceiling runner with sheet metal screws located 1/2 in. (13 mm) below the bottom of the deflection channel. When slotted ceiling runner (Item 2A1) is used, steel studs secured to slotted ceiling runner with No. 8 by 1/2 in. (13 mm) less used, steel studs secured to slotted ceiling runner with No. 8 by 1/2 in. (13 mm) long wafer head steel screws at midhelght of slot on each side of wall. Stud spacing not to exceed 24 in. (610 mm) OC. When vertical deflection ceiling runner (item 2A2) is used, steel studs secured to slotted vertical deflection cilps, through bushings, with steel screws at midhelght of each slot.

C. Gypsum Board\* — Gypsum board sheets installed to a min total thickness of 5/8 in. and 1-1/4 in. (16 and 32 mm) on each side of wall for 1 and 2 hr fire rated assemblies, respectively. Wall to be constructed as specified in the individual Wall and Partition Design in the UL Fire Resistance Directory, except that a max 3/4 in. (19 mm) gap shall be maintained between the top of the gypsum board and the bottom surface of the floor. The screws attaching the gypsum board to the stude along the top of the wall shall be located 1 in. (25 mm) below the bottom of the ceiling runner. No gypsum board attachment screws shall be driven into the ceiling runner or into the optional deflection channel. optional deflection channel.

The hourly fire rating of the joint system is dependent on the hourly fire rating of the wall assembly in which it is installed.

Joint System Max separation between bottom of floor and top of wall is 3/4 in. (19) 3. Joint System Max separation between bottom of floor and top of wall is 3/4 in. (19 mm). The joint system is designed to accommodate a max 25 percent compression from its installed width. The joint system consists of the following:

A. Deflection Channel — (Optional, Not Shown) — Max 2 in. (51 mm) deep min 24 gauge galv steel channel sized to accommodate celling runner (item 2A). Deflection channel secured to bottom of concrete floor with steel fasteners spaced max 24 in. (610 mm) OC. The celling runner is installed within the deflection channel to maintain a 1/2 in. to 3/4 in. (13 to 19 mm) gap between the top of the celling runner and the top of the deflection channel. The celling runner is not fastened to the deflection channel.

channel.

B. Forming Material — (Optional, Not Shown) — In 2 hr fire rated wall assemblies, polyethylene backer rod, mineral wool batt insulation or fiberglass batt insulation friction fit into joint opening.

C. Fill, Void or Cavity Material\* — Sealant — Min 1/2 in. (13 mm) thickness of fill material applied within joint opening on both sides of wall, flush with both surfaces of wall. In 1 hr fire rated walls, bond breaker tape applied to ceiling channel (item 2A, 2A) are 2A3) prior to installation of fill material. 2A1, 2A2 or 2A3) prior to installation of fill material. SPECIFIED TECHNOLOGIES INC — SpecSeal 100, 101, 102, 105, 120 or 129 Sealant TOP JOINT

System No. BW-S-0006 August 12, 2008
Assembly Ratings — 1 and 2 Hr (See Item 2) Joint Width - 1 In. (25 mm) Max 4 4

1. Floor Assembly - Min 4-1/2 in. (114 mm) thick reinforced lightweight or normal weight (100 -150 pcf (1600-2400 kg/cu meter)) structural concrete. Floor may also be constructed of any 6 in. (152 mm) thick UL Classified nollow—core Precast Concrete Units\*. See Precast Concrete Units category in the Fire Resistance Directory for names of manufactures. 2. Wall Assembly — The 1 or 2 h fire-rated gypsum board/steel stud wall assembly shall be constructed of the materials and in the manner specified in the individual U400 or V400 Series Wall or Partition Design in the UL Fire Resistance Directory. In addition, the wall may incorporate a head—of—wall joint system constructed as specified in the HW Series Joint Systems in the UL Fire Resistance Directory. The wall shall include the following construction features. features:

A. Steel Floor Runner — Floor runners of wall assembly shall consist of min No. 25 gauge galv steel channels sized to accommodate steel studs (Item 2B). Floor runners to be provided with min 1-1/4 in. (32 mm) flanges. Runners secured with steel fasteners spaced 12 in. (305

B. Studs — Steel studs to be min 2-1/2 in. (64 mm) wide. Studs cut 1/2 to 3/4 in. (13 to 19 mm) less in length than assembly height with bottom nesting in, resting on and fastened to floor runner with sheet metal screws. Stud spacing not to exceed 24 in. (610 mm) Gypsum Board\* — Gypsum board installed to a min total thickness of 5/8 in. (16 mm) or 1-1/4 in. (32 mm) on each side of wall for a 1 or 2 hr rated wall, respectively. Wall to be constructed as specified in the individual U400 or V400 Series Design in the UL Fire Resistance Directory except that a max 1 in. ( 25 mm) gap shall be maintained between the bottom of the gypsum board and the top of the concrete floor. The hourly fire rating of the joint system is equal to the hourly fire rating of the wall.

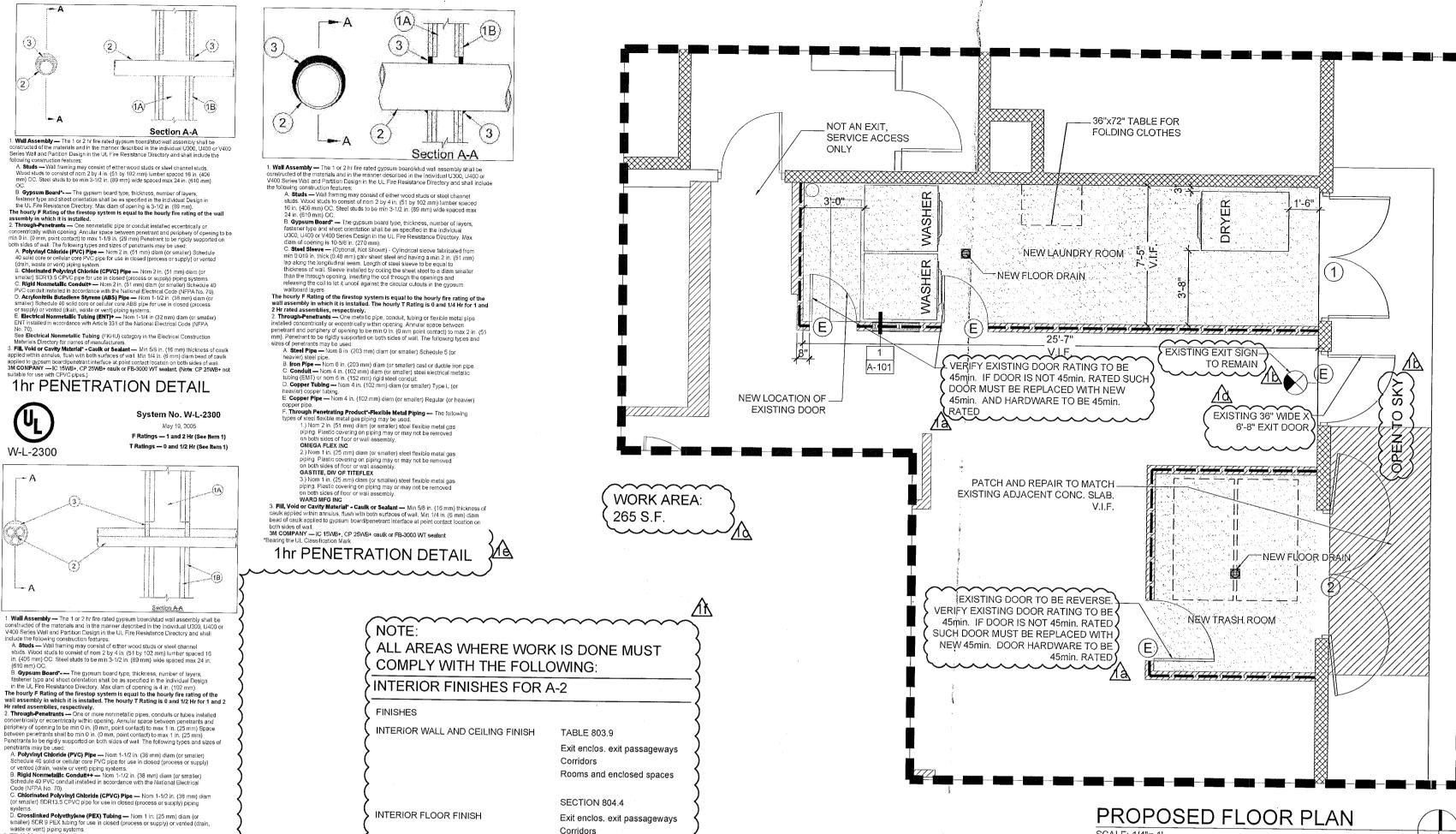
3. Joint System — Max separation between top of floor and bottom of

gypsum board is 1 in. (25 mm). The joint system consists of a packing material and a fill material, as follows: A. Packing Material — (Optional, Not Shown) — Foam backer rod firmly packed into the gap between the bottom of the gypsum board and the top of the concrete floor and recessed from each surface of the wall to accommodate the required thickness of fill material.

B. Fill, Void or Cavity Material\*—Sealant — Min 1/2 in. (13 mm) thickness of fill material installed on each side of the wall between the bottom of the gypsum board and the top of the concrete floor flush with each surface of the wall.

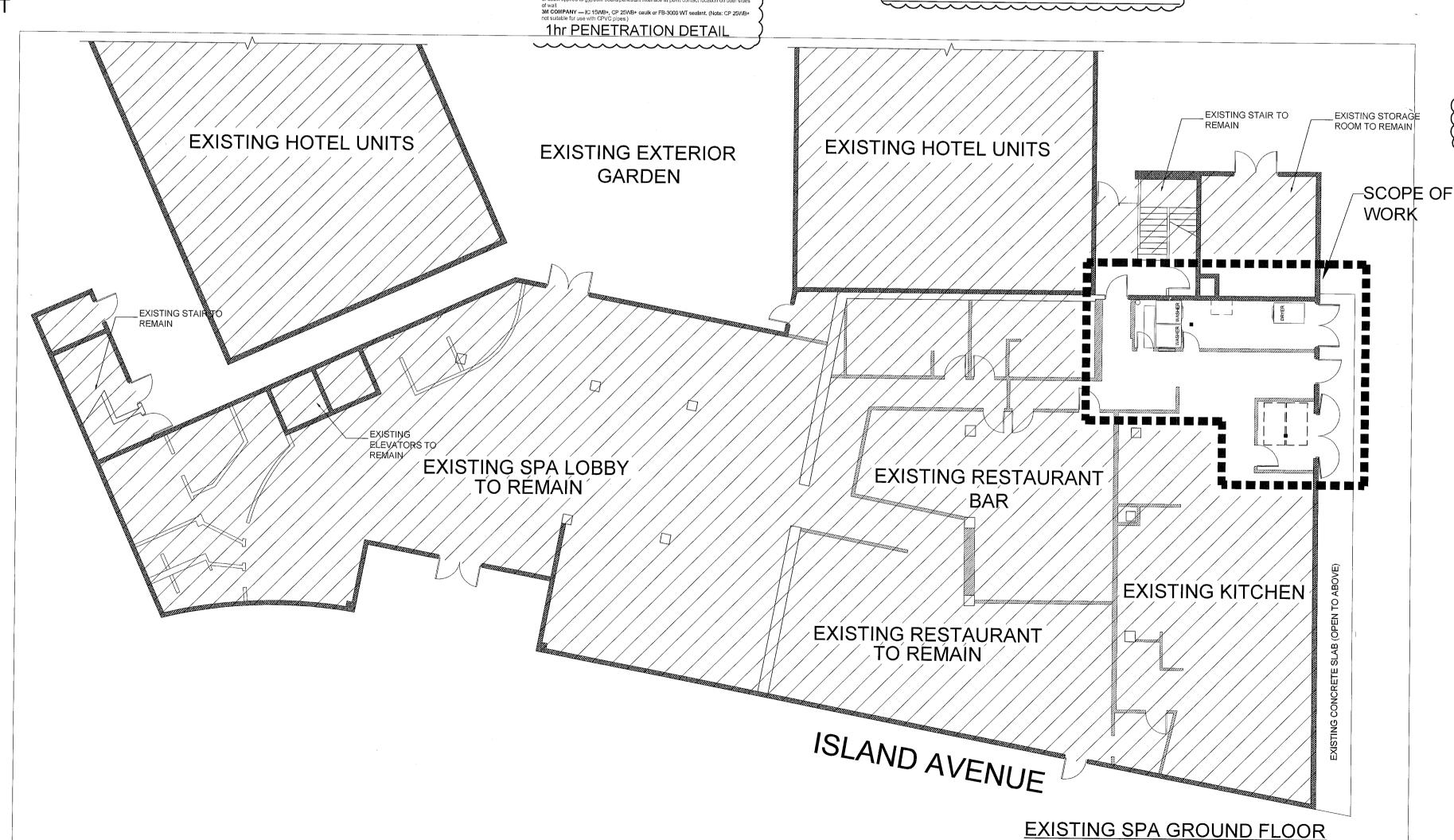
TREMCO INC — TREMstop Acrylic, TREMstop Intumescent Acrylic,
FyreCaulk, Fyre—Sil or TREMstop IA+

**BOTTOM JOINT** 



Rooms and enclosed spaces

SCALE: 3/32" = 1'



System No. W-L-2299

May 19, 2005

F Ratings - 1 & 2 Hr (See Item 1

W-L-2299

T Rating — 0 Hr

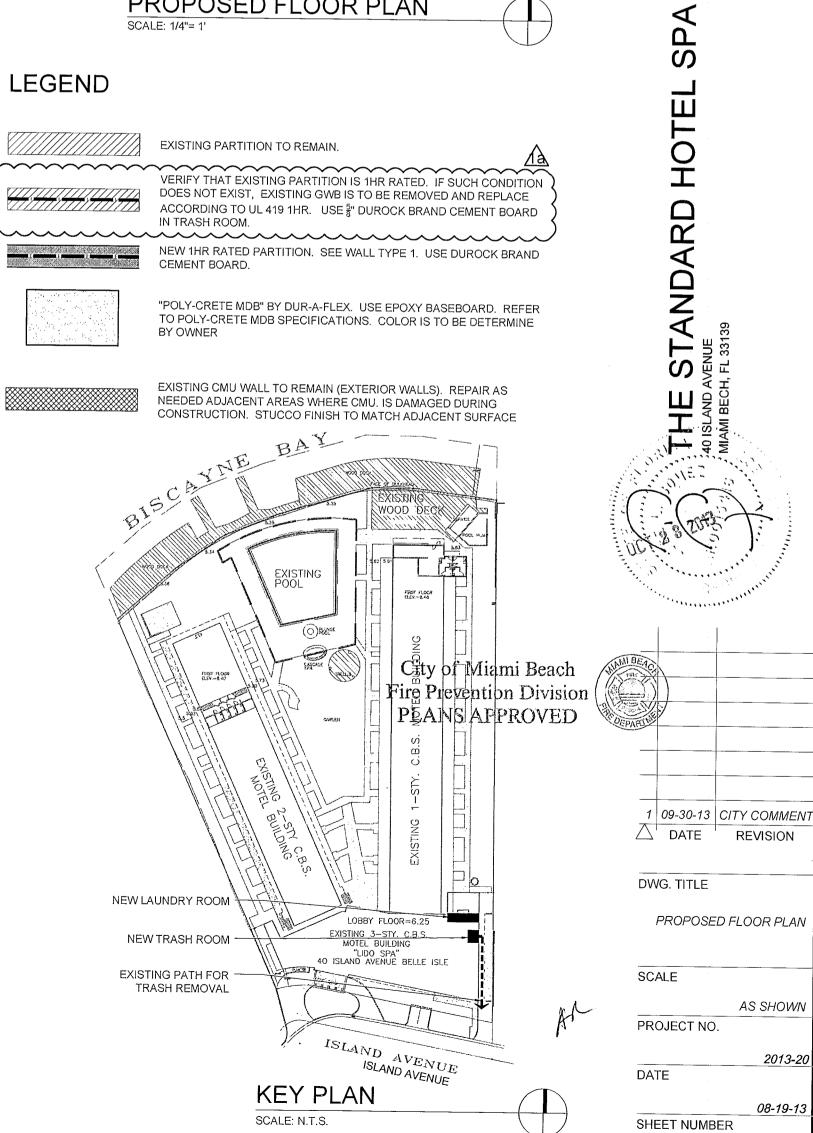
System No. W-L-1296

February 14, 2008

T Ratings — 0 and 1/4 Hr (See Item 1)

F Ratings - 1 and 2 Hr (See Item 1

W-L-1296



ARCHITECTURE AAC001062

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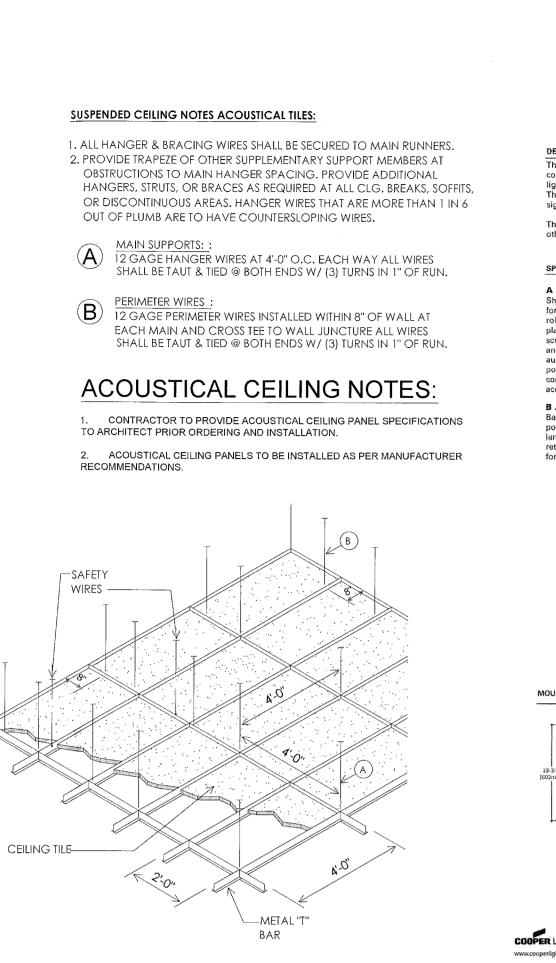
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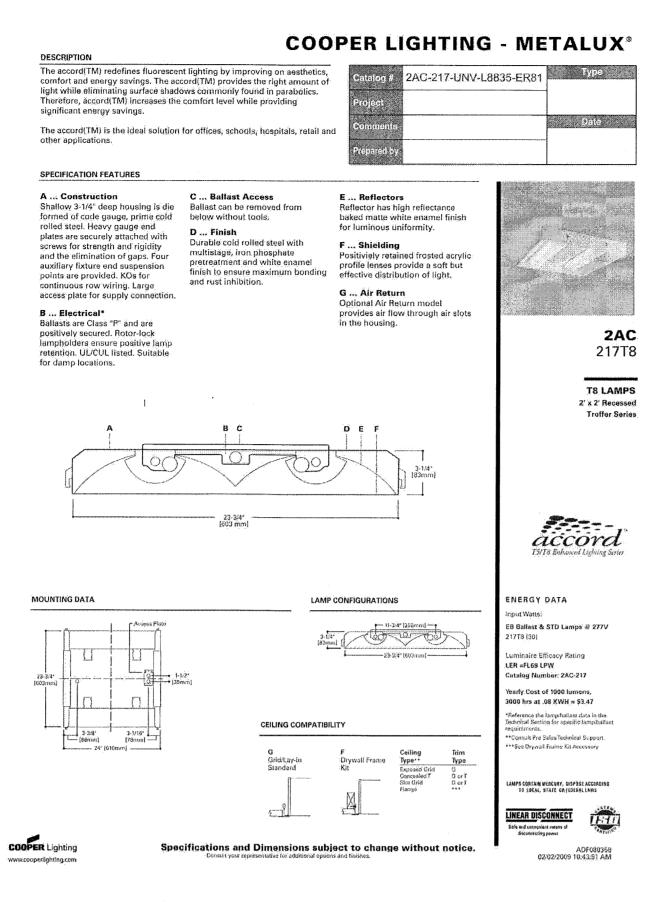
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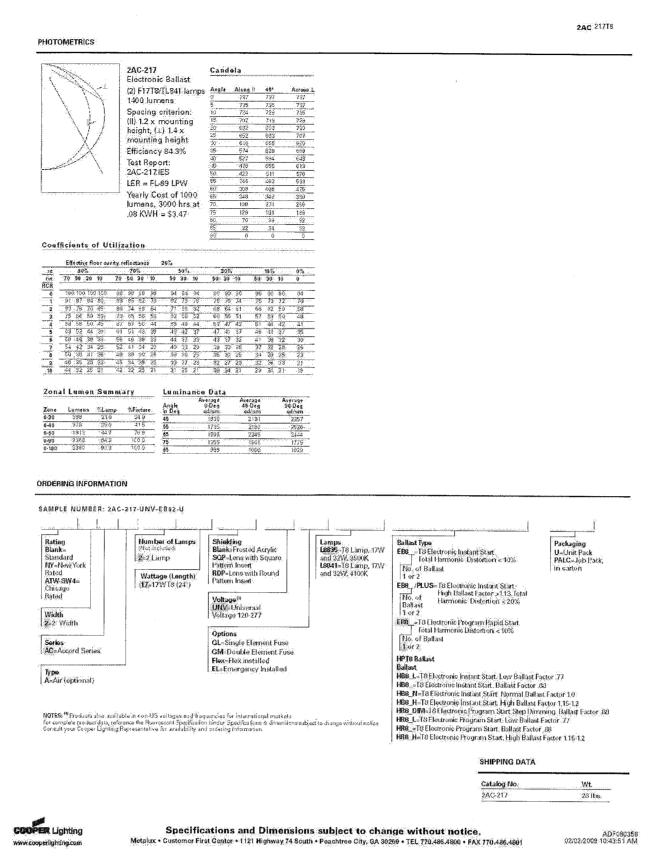
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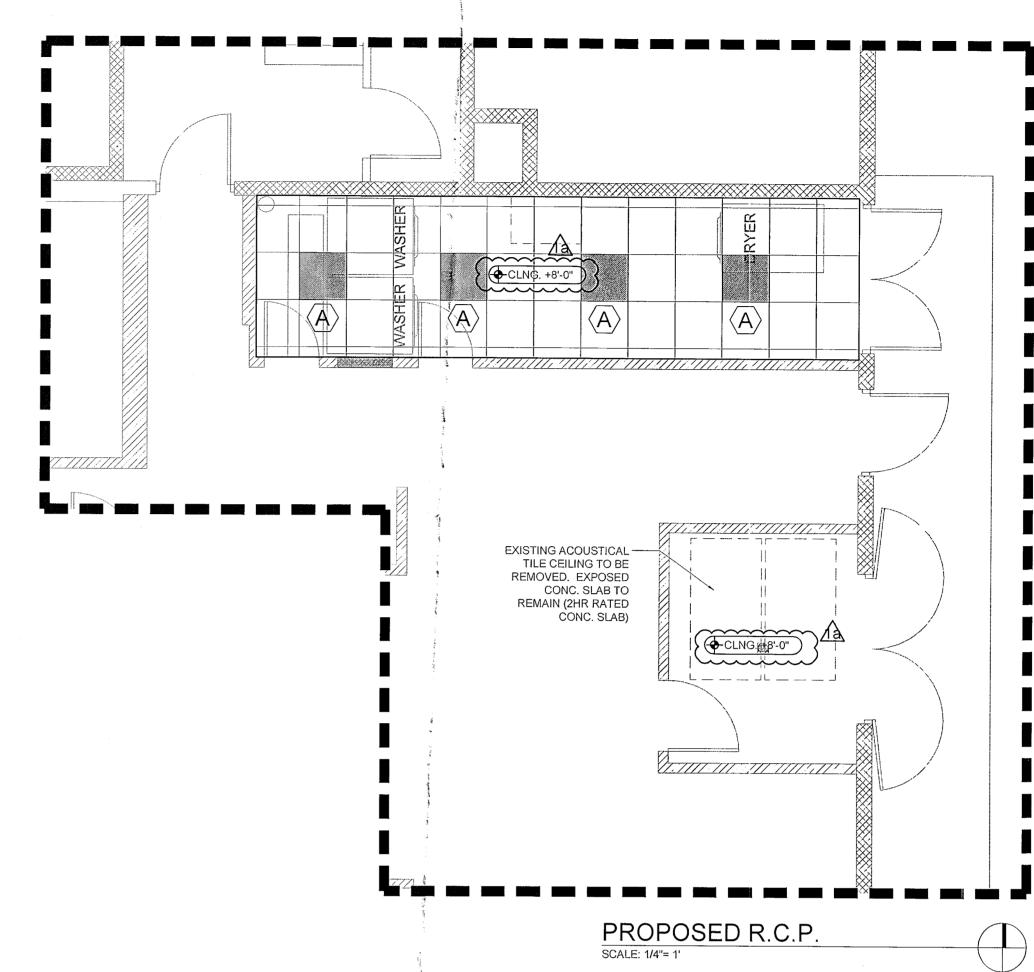
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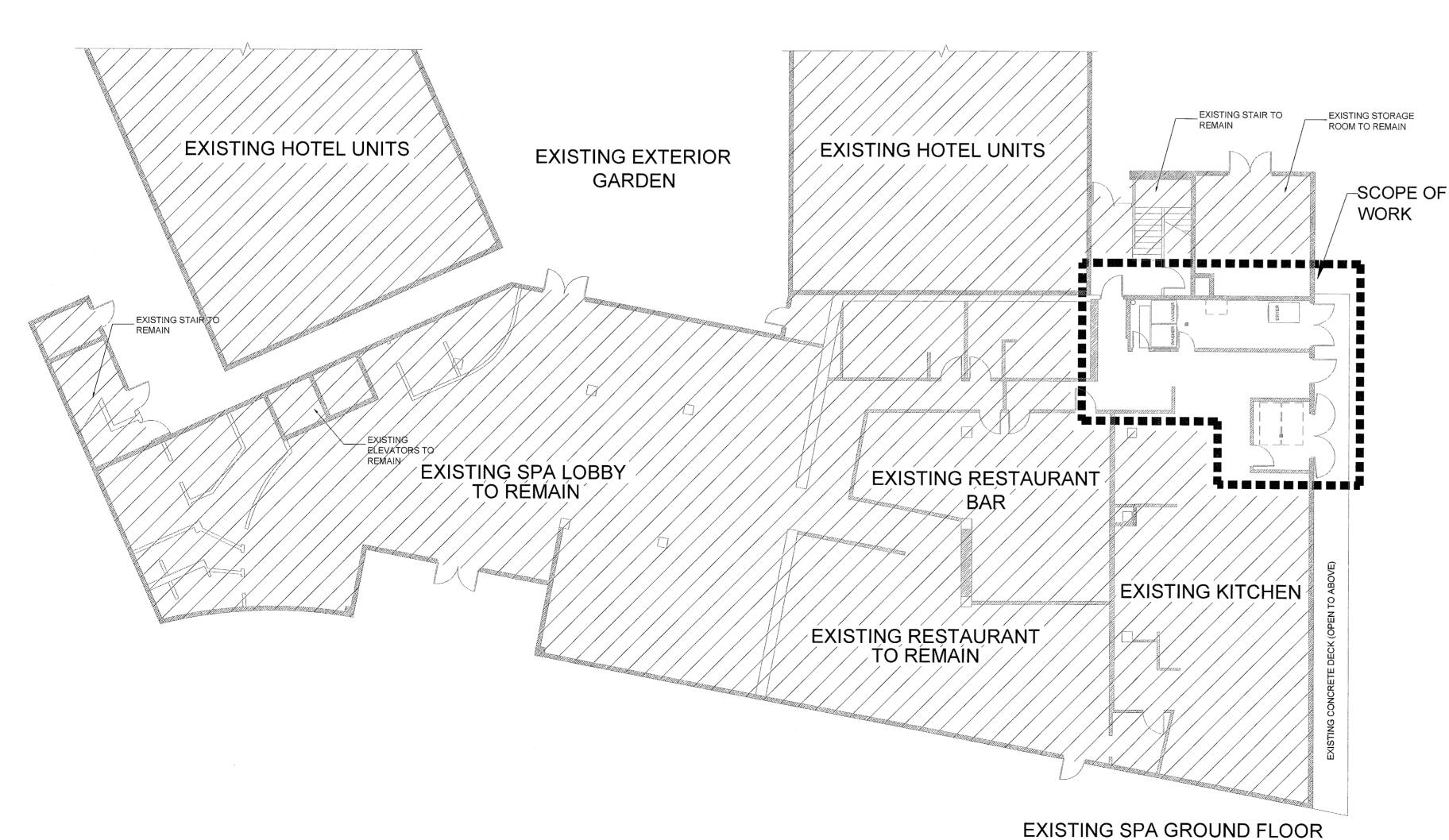
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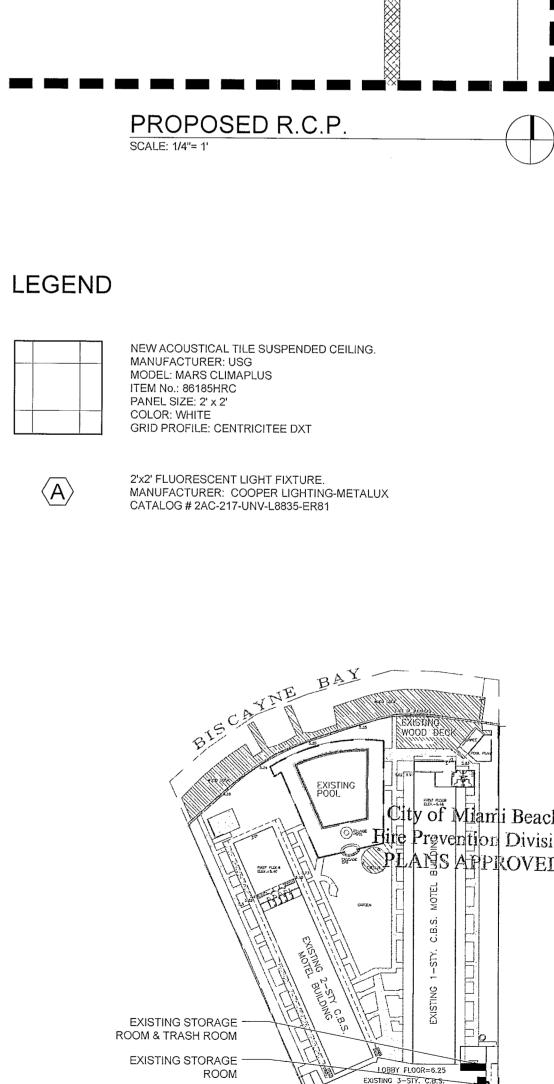




SCALE: 3/32" = 1'







**KEY PLAN** 

SCALE: N.T.S.

EXISTING PATH FOR TRASH REMOVAL

BEILLINSON GOMEZ ARCHITECTSPU

ARCHITECTURE AAC001062 JOSE L. GOMEZ AR0015416 8101 BISCAYNE BLVD. SUITE 309 MIAMI FL 33138-4664 TEL. (305) 559.1250 FAX (305) 551.1740 beilinsonarchitectspa.com

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THE STANDARD HOTEL SPA

1 09-30-13 CITY COMMENT

△ DATE REVISION

DWG. TITLE

PROPOSED

REFLECTED CEILING PLAN

AS SHOWN
PROJECT NO.

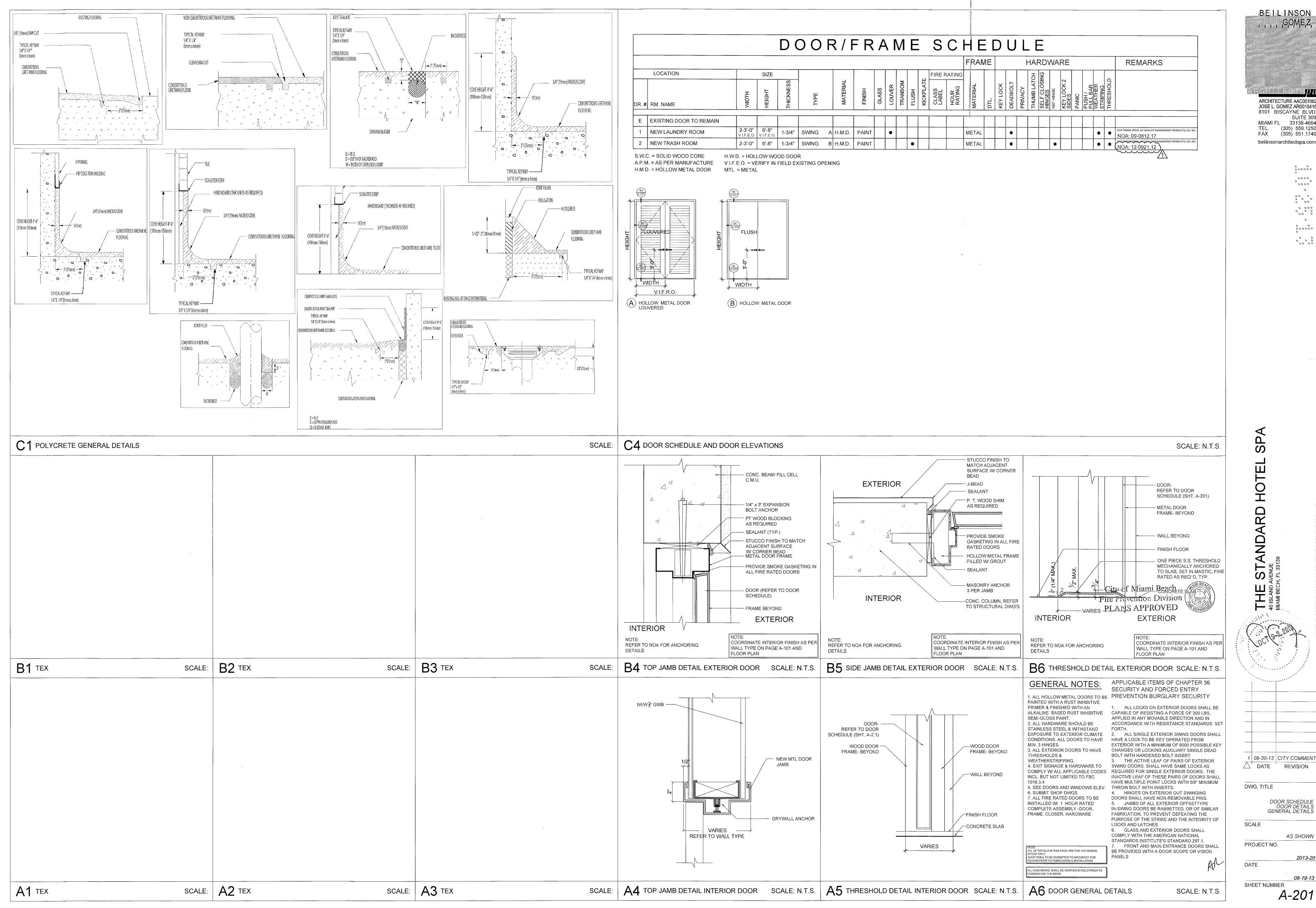
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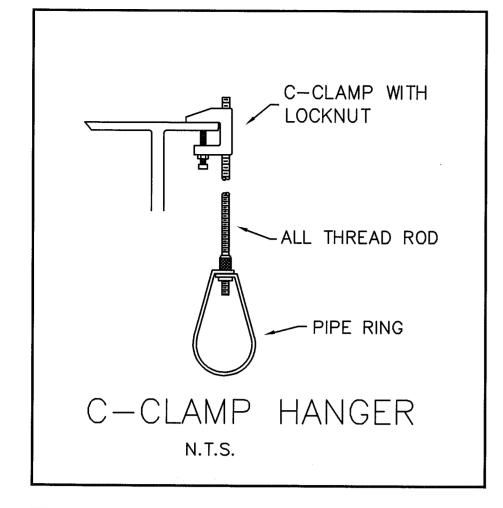
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SCALE

SHEET NUMBER

A-102



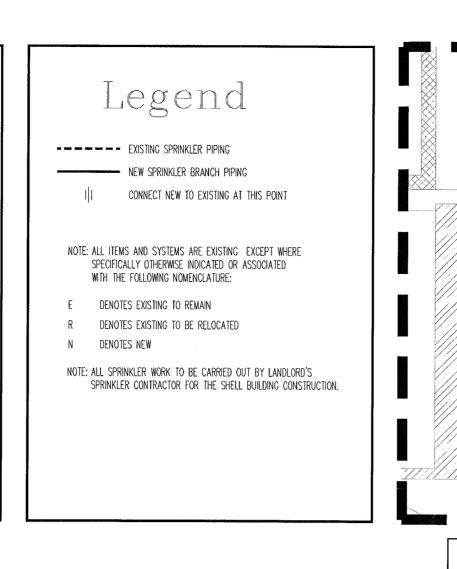


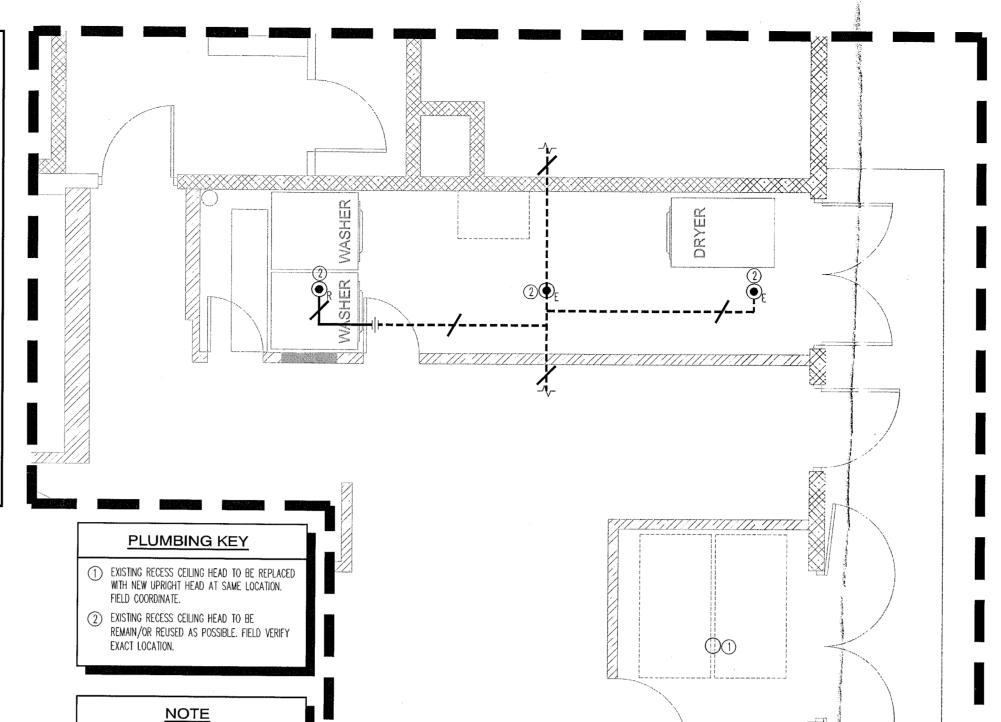
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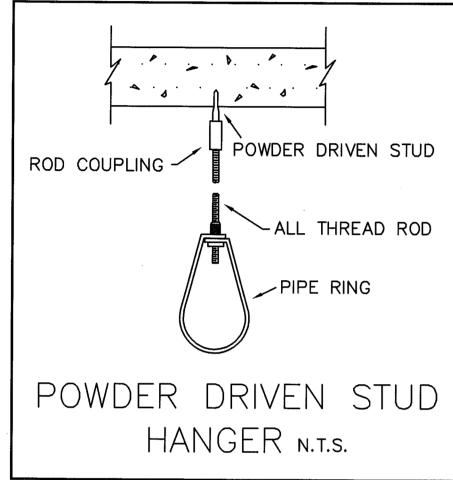
## FIRE SPRINKLER NOTES:

ALL FIRE SPRINKLER PIPING AND SPRINKLER HEAD DISTRIBUTION TO BE AS PER THE REQUIREMENTS OF THE NATIONAL FIRE CODE CHAPTER 13, THE STATE FIRE MARSHALL, AND THE AUTHORITIES HAVING LOCAL JURISDICTION. IT SHALL BE THE CONTRACTOR'S RESPONSIBILITY TO DESIGN THE SYSTEM HYDRAULICALLY, AND SUBMIT HYDRAULIC CLACS. FOR REVIEW & APPROVAL IN COMPLIANCE WITH ALL GOVERNING AGENCY CRITERIA, AND TO VERIFY THE PROPER WATER PRESSURES AND QUANTITIES TO INSURE THE PROPER OPERATION OF THE SYSTEM. THE SPRINKLER HEADS SHALL BE PENDANT TYPE, UPRIGHT HEADS ( OR SIDE WALL HEADS ONLY WHERE IMPRACTICAL TO USE UPRIGHT), CHROME PLATED IN ALL FINISHED AREAS, AND BRASS PLATED IN UNFINISHED AREAS ALL PIPING TO BE CONCEALED IN ALL FINISHED AREAS. ECUTCHEON PLATES ARE TO BE CHROME PLATED, AND BE FURNISHED AS TWO PIECE IN ALL LAY-IN CEILINGS TO FACILITATE REMOVAL OF CEILING TILES AFTER THE INSTALLATION.

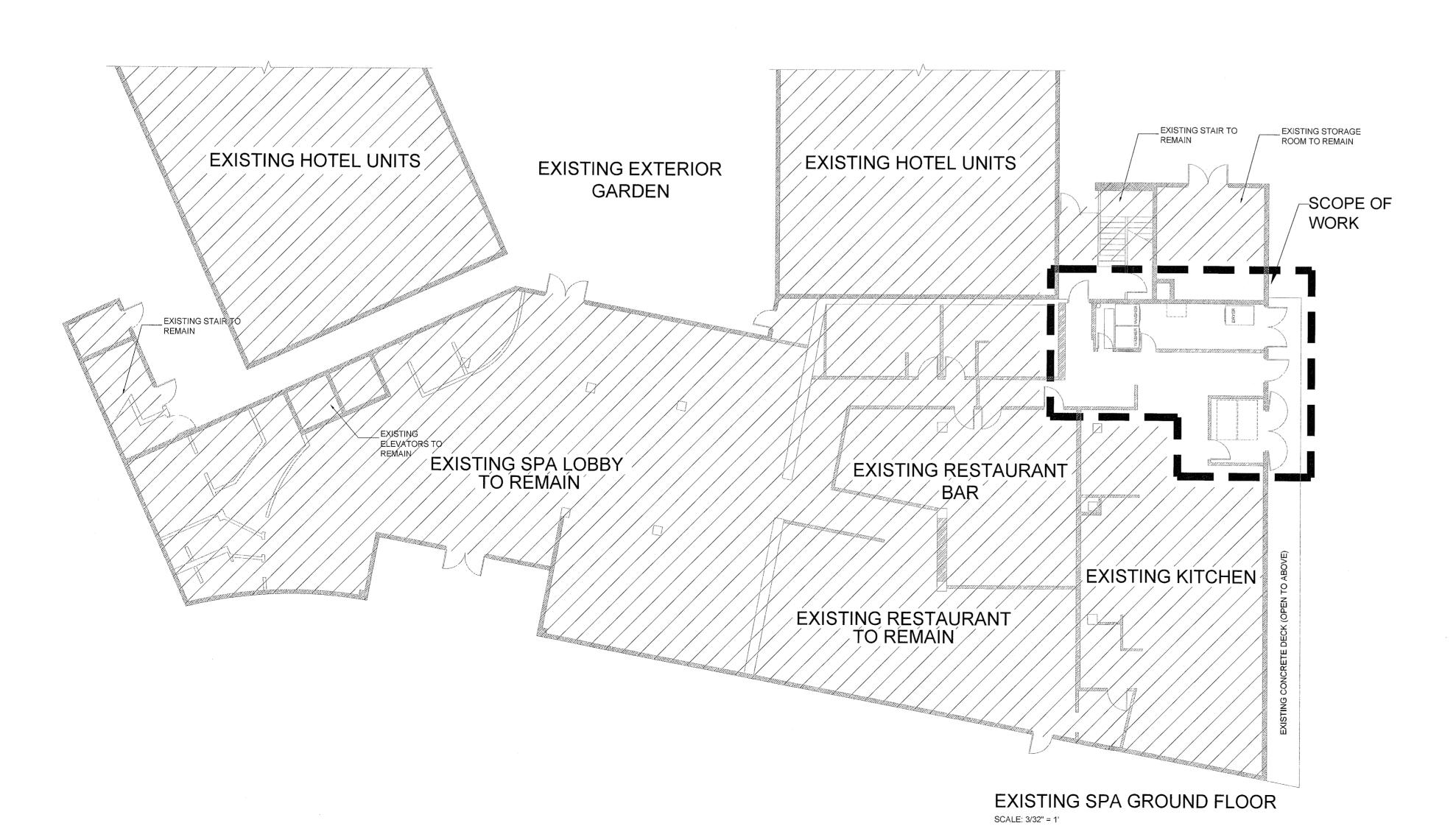


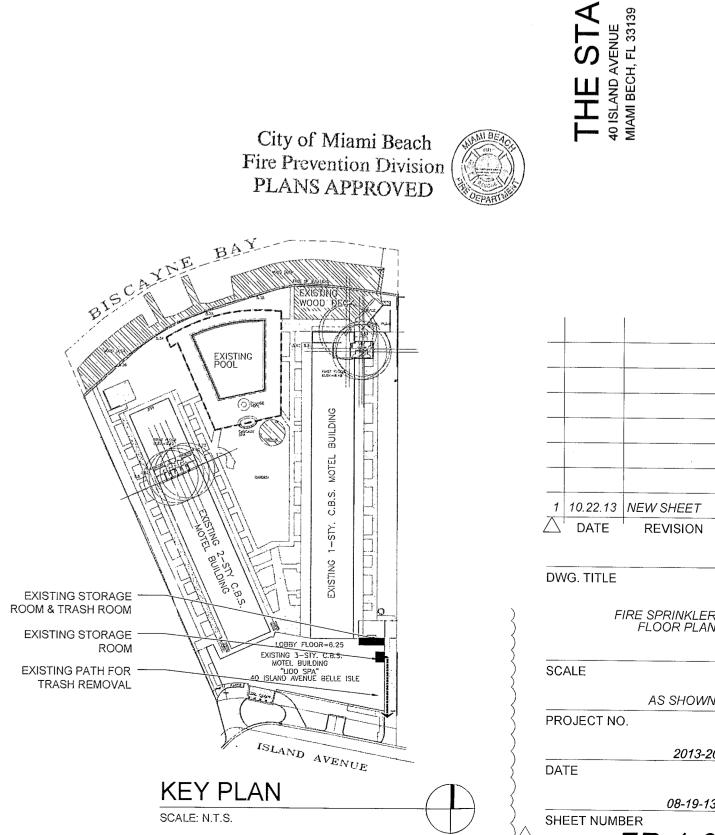


Fire Sprinkler Floor Plan
SCALE: 1/4"= 1'



	SPLINKE	ER HEAD LI	EGEND			PLUMBING KEY  1 EXISTING RECESS CEILING HEAD TO BE REPLACED WITH NEW UPRIGHT HEAD AT SAME LOCATION. FIELD COORDINATE. 2 EXISTING RECESS CEILING HEAD TO BE	
SYMBOL	TYPE OF SPRINKLER	MODEL	MANUF.	ORIF.	TEMP.	REMAIN/OR REUSED AS POSSIBLE. FIELD VERIFY EXACT LOCATION.	
0	UPRIGHT HEAD	TY-3151	TYCO	1/2"	155^		
•	CHROME RECESSED PENDENT*	TY-3551	TYCO	1/2"	155^	-	
						BUILDING PROVIDED WITH EXISTING FIRE SPRINKLER SYSTEM TO REMAIN AS IS. SCOPE OF WORK LIMITED TO CHANGE HEAD TYPE AT NEW TRASH ROOM.	





BEILLINSON , , GOMEZ

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FIRE SPRINKLER FLOOR PLAN

AS SHOWN

SHEET NUMBER

#### **SUMMARY OF WORK**

INSTALL A TEMPORARY DUST/ WEATHER BARRIER WALL INSIDE THE BUILDING AS DIRECTED BY ENGINEER.

REPAIR ALL CRACKED AND SPALLED CONCRETE AT THE TOP, BOTTOM AND EDGE SURFACES OF THE WINDOWS INCLUDED IN THE WORK AS DIRECTED BY THE ENGINEER

REPAIR ALL CRACKED AND SPALLED CONCRETE AT THE BUILDING COLUMNS AND WALLS INCLUDED IN THE WORK AS DIRECTED BY THE ENGINEER

INSTALL SHORING AS DIRECTED BY THE ENGINEER OR AS OTHERWISE NEEDED TO PERFORM THE WORK. PROVIDE SIGNED AND SEALED SHORING PLANS PREPARED BY A FLORIDA REGISTERED PROFESSIONAL ENGINEER.

## CONCRETE FORMWORK REFERENCES

ACI 301 - Structural Concrete for Buildings.

ACI 318 - Building Code Requirements for Reinforced Concrete.

ACI 347 - Recommended Practice For Concrete Formwork.

Florida Building Code.

#### DESIGN REQUIREMENTS

Design, engineer and construct formwork, shoring and bracing to conform to design and code requirements; resultant concrete to conform to required shape, line and dimension.

#### QUALITY ASSURANCE

Perform Work in accordance with ACI 347, 301 and 318, and Florida Building Code standards. Maintain one copy of each document on site.

Design formwork under direct supervision of a Professional Engineer experienced in design of this work and licensed in the State of Florida.

#### WOOD FORM MATERIALS

Form Materials: Site fabricated plywood with wood reinforcement.

#### **FORMWORK ACCESSORIES**

Form Release Agent: Colorless mineral oil which will not stain concrete, or absorb moisture, or impair natural bonding or color characteristics of coating intended for use on concrete.

Nails, Spikes, Lag Bolts, Through Bolts, Anchorages: Sized as required, of sufficient strength and character to maintain formwork in place while placing concrete.

Erect formwork, shoring and bracing to achieve design requirements, in accordance with

requirements of ACI 301.

Provide bracing to ensure stability of formwork. Shore or strengthen formwork subject to

Arrange and assemble formwork to permit dismantling and stripping. Do not damage concrete during stripping. Permit removal of remaining principal shores.

## CONCRETE REINFORCEMENT

over stressing by construction loads.

REFERENCES
ACI 301 - Structural Concrete for Buildings.
ACI 318 - Building Code Requirements For Reinforced Concrete.
ACI SP-66 - American Concrete Institute - Detailing Manual.
ASTM A615 - Deformed and Plain Billet Steel Bars for Concrete Reinforcement.
AWS D1.4 - Structural Welding Code for Reinforcing Steel.
CRSI - Concrete Reinforcing Steel Institute - Manual of Practice.
Florida Building Code.

## REINFORCEMENT

Reinforcing Steel: ASTM A615, 60 ksi yield grade; deformed billet steel bars, unfinished.

## ACCESSORIES

Columns

Tie Wire: Minimum 16 gage annealed type.

Chairs, Bolsters, Bar Supports, Spacers: Sized and shaped for strength and support of reinforcement during concrete placement conditions, plastic coated steel.

Rust-Inhibitive Coating: See Section 03732 2.3(B).

Maintain concrete cover around reinforcing as follows:
Item Coverage
Supported Slabs 1-1/2 inches
Walls 1-1/2 inches

Lap splice reinforcing bars 48 bar diameters unless indicated otherwise by Engineer. Apply brush coating of rust-inhibitive coating to all exposed reinforcing steel in concrete repair areas.

1-1/2 inches

## Align joints and make watertight. Keep form joints to a minimum.

If formwork is placed after reinforcement resulting in insufficient concrete cover over reinforcement, before proceeding, request instructions from Engineer.

#### APPLICATION - FORM RELEASE AGENT

#### INSERTS, EMBEDDED PARTS, AND OPENINGS

Provide formed openings where required for items passing through concrete work.

Locate and set in place items which will be cast directly into concrete.

Install accessories in accordance with manufacturer's instructions, straight, level, and plumb. Ensure items are not disturbed during concrete placement.

Provide temporary ports or openings in formwork where required to facilitate cleaning and inspection. Locate openings at bottom of forms to allow flushing water to drain.

Close temporary openings with tight fitting panels, flush with inside face of forms, and neatly fitted so joints will not be apparent in exposed concrete surfaces.

#### FORMWORK TOLERANCES

Construct formwork to maintain tolerances required by ACI 301

CAST-IN-PLACE CONCRETE

REFERENCES
ACI 211.1 - Selecting Proportions for Normal, Heavyweight, and Mass Concrete.

ACI 301 - Structural Concrete for Buildings.
ACI 302 - Guide for Concrete Floor and Slab Construction.

ACI 304 - Recommended Practice for Measuring, Mixing, Transporting and Placing

Concrete.
ACI 305R - Hot Weather Concreting.

ACI 308 - Standard Practice for Curing Concrete.
ACI 318 - Building Code Requirements for Reinforced Concrete.

ASTM C33 - Concrete Aggregates.

ASTM C94 - Ready-Mixed Concrete.

ASTM C150 - Portland Cement.

ASTM C260 - Air Entraining Admixtures for Concrete. ASTM C494 - Chemical Admixtures for Concrete.

Florida Building Code.

CONCRETE MATERIALS
Cement: ASTM C150, Type I - Normal.
Fine and Coarse Aggregates: ASTM C33.

Water: Clean and not detrimental to concrete.

ADMIXTURES

#### Air Entrainment: ASTM C260.

Chemical: ASTM C494 Type A - Water Reducing, Type B - Retarding, Type D - Water Reducing and Retarding, Type F - Water Reducing, High Range.

#### Calcinated Pozzolan: ASTM C618 Class MBSF, Microsilica.

Corrosion Inhibitor: Rheocrete 222+ manufactured by Master Builders, Inc. or DCI manufactured by W. R. Grace, Inc.

Mix concrete in accordance with ACI 304. Deliver concrete in accordance with ASTM C94.

## Provide concrete to the following mix design:

Unit	Mossymans
	Measurement
Compressive Strength (7 day)	3,000 psi
Compressive Strength (28 day)	5,000 psi
Water/Cement Ratio (maximum)	0.40 by weight
Aggregate Size (maximum)	3/8 inch
Air Entrained	4 percent
Admixture	ASTM C-260
Admixture	ASTM C-494,B/D
Admixture	ASTM C-494,A/F
Corrosion Inhibitor	As recommended

## PLACING CONCRETE

Place concrete in accordance with ACI 301, ACI 318, and ACI 304.

Notify Engineer minimum 48 hours prior to commencement of operations.

Ensure reinforcement, block-outs, inserts and embedded parts are not disturbed during concrete placement.

Maintain records of concrete placement. Record date, location, quantity, air temperature, and test samples taken.

Do not interrupt successive placement; do not permit cold joints to occur.

Screed floors or to match slopes, maintaining surface flatness of maximum 1/4 inch in 10 ft.

## CURING AND PROTECTION

Immediately after placement, protect concrete from premature drying, excessively hot temperatures, and mechanical injury.

Maintain concrete with minimal moisture loss at relatively constant temperature for period necessary for hydration of cement and hardening of concrete.

Cure concrete floor surfaces in accordance with ACI 308.

Spraying: Spray water over floor slab areas and maintain wet for 7 days.

Curing Compound: Apply curing compound in accordance with manufacturer's instruction as an alternate to spraying. Confirm that curing compound is compatible with any subsequent paint or coating.

## PATCHING

Allow Engineer to inspect concrete surfaces immediately upon removal of forms.

Shrinkage cracking, honeycomb or embedded debris in concrete shall be considered defective concrete.

Patch imperfections as directed. Repair shrinkage cracks with pressure-injected or gravity-feed epoxy adhesive as directed by the Engineer.

### DEFECTIVE CONCRETE

Defective Concrete: Concrete not conforming to required lines, details, dimensions, tolerances or specified requirements.

Repair or replacement of defective concrete will be determined by the Engineer.

Do not patch, fill, touch-up, repair, or replace exposed concrete except upon express direction of Engineer for each individual area.

#### CONCRETE REPAIR

REFERENCES

ASTM A615/A615M - Deformed and Plain Billet-Steel Bars for Concrete Reinforcement. ASTM C882 - Bond Strength of Epoxy Resin Systems Used with Concrete. Florida Building Code.

International Concrete Repair Institute.

PRODUCTS MANUFACTURERS
Degussa Building Systems (ThoRoc, Master Builders, Sonneborn)
Sika Corporation
Sto Construction Restoration Division

PATCHING MATERIALS

Epoxy Adhesive: Two-component, 100% solids, moisture insensitive, structural epoxy adhesive.

Bonding Agent: Multi-component, moisture tolerant, epoxy-modified, cementitious bonding agent.

Cementitious Mortar: One or two-component, polymer modified, cementitious mortar.

Curing Compound: As recommended by repair mortar manufacturer. Compatible with subsequent waterproof membranes, coatings and finishes.

Sealant: One-part, polyurethane sealant.

REINFORCEMENT MATERIALS

Reinforcing Steel: ASTM A615, 60 ksi yield grade billet-steel deformed bars, unfinished with rust-inhibitive coating.

Rust-Inhibitive Coating: Multi-component, moisture tolerant, epoxy-modified, cementitious rust-inhibitive coating.

#### MIXING EPOXY ADHESIVES

Mix epoxy adhesives in accordance with manufacturer's instructions for purpose intended.

Mix components in clean equipment or containers. Conform to pot life and workability limits.

MIXING CEMENTITIOUS MATERIALS

Mix cementitious mortar in accordance with manufacturer's instructions for purpose intended.

## PREPARATION - SPALL REPAIR

Clean concrete surfaces of dirt, laitance, corrosion, or other contamination; sandblast; rinse surface and allow to dry.

Remove deteriorated or unsound concrete by chipping hammer where directed by the Engineer. Removal of concrete shall extend 2" to 4" beyond the outer boundary mark of unsound concrete. Areas removed shall be rectangular shaped.

The edges of the patch area shall be perpendicular or slightly undercut between 3/8" and 1/2" deep. Feather edges will not be permitted.

Concrete shall be removed completely around exposed corroded reinforcing steel such that a 3/4" clearance from the existing concrete is obtained.

Removal of concrete shall be performed by using chipping hammers not in excess of 30-lb.

Remove loose concrete from the patch area and leave said area boom clean.

Sandblast clean the exposed reinforcement steel surfaces. Mechanically cut away damaged portions of bar.

Apply brush coating of rust-inhibitive coating to exposed reinforcement steel.

## APPLICATION - CEMENTITIOUS MORTAR

Apply scrub coat of neat mortar to SSD concrete surfaces. Provide full surface coverage.

Apply cementitious mortar by steel trowel to an average thickness of one inch. Tamp into place filling voids at spalled areas. Work mix into honeycomb. Apply additional lifts as necessary.

Alternately, install forms and place cementitious mortar by pouring. Vibrate as necessary to consolidate.

Damp cure cementitious mortar for four days or as per manufacturer's instructions. Alternatively, apply curing compound in accordance with manufacturer's instructions.

## NON-STRUCTURAL CRACK REPAIR

Rout cracks to a width and depth of ¼ inch.

Remove all dirt, dust and other foreign matter from the cracks using compressed air or water.

## Allow crack to dry.

Seal crack with a one-part urethane sealant.

Tool sealant flush with adjacent surfaces.

FLUID APPLIED WATERPROOFING

#### REFERENCES

ASTM D412 - Rubber Properties in Tension.
ASTM 1653 - Vapor Permeability.
ASTM C297 - Adhesion to Concrete.
ASTM D570 - Water Absorption.

SYSTEM DESCRIPTION

Waterproofing System: Single application of fluid applied material to prevent moisture migration.

#### MANUFACTURERS

Sonneborn/Chemrex, Inc. Product Flextight.
Sto Construction Restoration Division Product Watertight Coat.

MEMBRANE COMPOUND MATERIAL

Waterproofing Membrane: Modified acrylic dispersion with special cements and fillers.

### Cured Membrane Characteristics:

Properties	Test	Results
Tensile Strength:	ASTM D412	250 psi
Elongation:	ĄSTM D412	15%
Water Absorption:	ĄSTM D570	7.1%
Moisture Vapor:	ÁSTM 1653	1.20 dry perms
Concrete Adhesion	ASTM C297	89 psi

#### **EXAMINATION**

Verify substrate surfaces are durable; free of dampness, loose particles, cracks, pits, projections, or foreign matter detrimental to adhesion or application of waterproofing system.

Verify that substrate surfaces are smooth, free of honeycomb or pitting, and not detrimental to full contact bond of waterproofing materials.

Verify items which penetrate surfaces to receive waterproofing are securely installed.

#### PORTLAND CEMENT PLASTER

REFERENCES
ASTM C150 - Portland Cement.
ASTM C926 - Application of Portland Cement Based Plaster.

PRODUCTS
MANUFACTURERS

Larsen Products Corp. Weld-Crete bonding agent.

Rinker Stucco Mix.

Florida Building Code.

PREPARATION

Roughen smooth concrete surfaces using mechanical scabbler or similar method.

Remove all loose material, dust, dirt, laitance, etc. from surfaces to receive stucco to

Apply bonding agent uniformly, using brush or roller, to form continuous blue film over entire

## Allow to dry one hour.

Apply plaster within 10 days.

provide clean, dry surface.

## PLASTERING

Apply plaster in accordance with ASTM C926 and manufacturer's instructions.

Apply scratch coat to a nominal thickness of 3/8 inch, brown coat to a nominal thickness of 3/8 inch and a finish coat to a nominal thickness of 1/8 inch over metal-lathed surfaces.

Apply brown coat to a nominal thickness of 3/8 inch and a finish coat to nominal thickness of 1/8 inch over masonry and concrete surfaces.

Avoid excessive working of surface. Delay troweling as long as possible to avoid drawing

## Moist cure scratch and brown coats

excess fines to surface.

After curing, dampen base coat prior to applying finish coat.

Apply finish coat and trowel to a consistent finish to match existing.

Moist cure finish coat for minimum period of 48 hours.

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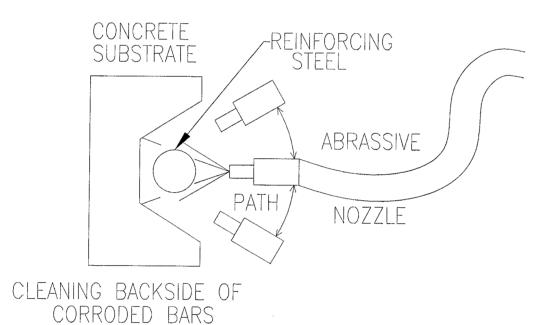
SHEET NUMBER **S-1.** 

S-1.0

BEAM OVER OPENING PATCH DETAIL
SCALE: 3/4" =1'-0"

## **CLEANING OF REINFORCING STEEL**

- 6 ALL HEAVY CORROSION AND SCALE SHOULD BE REMOVED FROM BAR AS NECESSARY TO PROMOTE MAXIMUM BOND OF REPLACEMENT MATERIAL.
- OIL FREE ABRASIVE BLAST IS THE PREFERRED METHOD. A TIGHTLY BONDED LIGHT RUST BUILD—UP ON THE SURFACE IS USUALLY NOT DETRIMENTAL TO BOND, UNLESS A PROTECTIVE COATING IS BEING APPLIED TO THE BAR SURFACE, IN WHICH CASE THE COATING MANUFACTURER'S RECOMMENDATION FOR SURFACE PREPARATION SHOULD BE FOLLOWED.

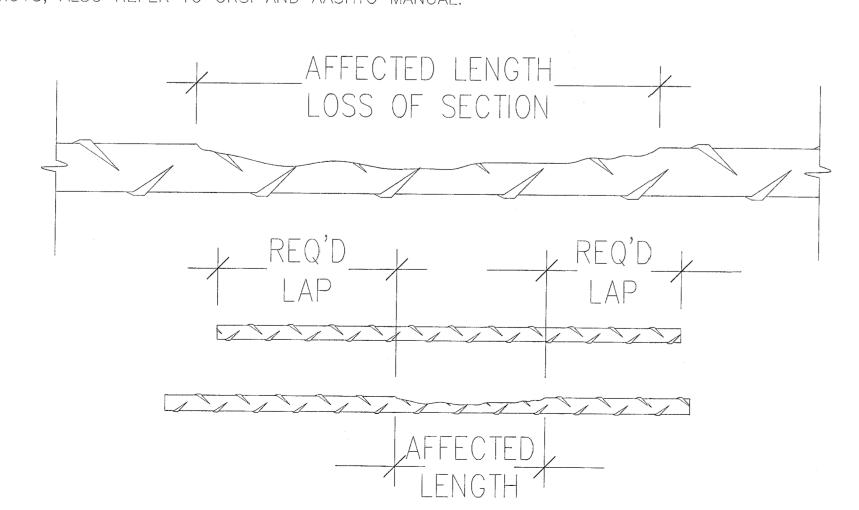


## REPAIR OF REINFORCING STEEL DUE TO LOSS SECTION

IF REINFORCING STEEL HAS LOST MORE THAN 5% OF ITS CROSS SECTION, A STRUCTURAL ENGINEER SHOULD BE CONSULTED. IF REPAIRS ARE REQUIRED TO THE REINFORCING STEEL, ONE OF THE FOLLOWING REPAIR METHODS SHOULD BE USED.

- COMPLETE BAR REPLACEMENT, OR
- ADDITIONAL OF SUPPLEMENT BAR OVER AFFECTED SECTION.

NEW BARS MAY BE MECHANICALLY SPLICED TO OLD BARS OR PLACED PARALLEL TO AND APPROXIMATELY 1/4" FROM EXISTING BARS.LAP LENGTH SHALL BE DETERMINED IN ACCORDANCE WITH ACI318; ALSO REFER TO CRSI AND AASHTO MANUAL.



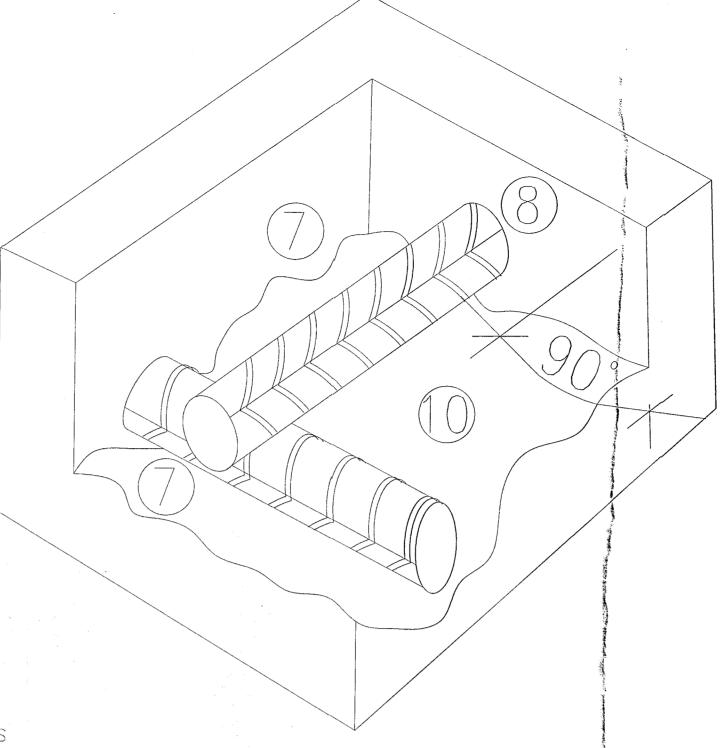
## EDGE AND SURFACE CONDITIONING OF CONCRETE

THESE DETAILS ARE APPLICABLE TO HORIZONTAL, VERTICAL, AND OVERHEAD LOCATIONS. THEY ARE ALSO APPLICABLE TO REMOVE BY HYDRO—DEMOLITION, HYDROMILLING, AND ELECTRIC, PNEUMATIC OR HYDRAULIC IMPACT BREAKERS.

DO NOT USE THESE DETAILS FOR SHOTCRETE APPLICATIONS, FOR SHOTCRETE REPAIRS REFER TO AC1506 EDGE PREPARATION GUIDELINES.

- 7 REMOVE DELAMINATED CONCRETE, UNDERCUT REINFORCING

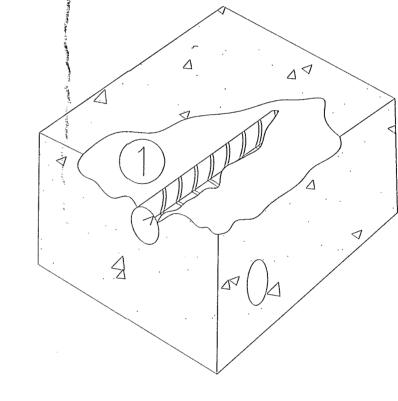
  ( ) STEEL (REFER TO "EXPOSING AND UNDERCUTTING OF REINFORCING
- STEEL (REFER TO "EXPOSING AND UNDERCUTTING OF REINFORCING STEEL" ON THIS SHEET), REMOVE ADDITIONAL CONCRETE AS REQUIRED TO TO PROVIDE MINIMUM REQUIRED THICKNESS OF REPAIR MANUAL.
- 8 AT EDGE LOCATIONS, PROVIDE RIGHT ANGLE CUTS TO THE CONCRETE SURFACE WITH EITHER OF THE FOLLOWING METHOD:
  - SAWCUT 1/2" (16mm) OR LESS AS REQUIRED TO AVOID CUTTING REINFORCING STEEL.
  - USE POWER EQUIPMENT SUCH AS HYDRODEMOLITION OR IMPACT BREAKERS. AVOID FEATHER EDGES.
- 9 REPAIR CONFIGURATIONS SHOULD BE KEPT AS SIMPLE AS POSSIBLE, PREFERABLY WITH SQUARED CORNERS.
- AFTER REMOVALS AND EDGE CONDITIONING ARE COMPLETE,
  REMOVE BOND INHIBITING MATERIALS (DIRT, CONCRETE SLURRY,
  LOOSELY BONDED AGGREGATES) BY ABRASIVE BLASTING OR
  HIGH PRESSURE WATER BLASTING WITH OR WITHOUT ABRASIVE.
  CHECK THE CONCRETE SURFACES AFTER CLEANING TO INSURE THAT
  SURFACE IS FREE FROM ADDITIONAL LOOSE AGGREGATE, OR THAT
  ADDITIONAL DELAMINATIONS ARE NOT PRESENT.
- (1) IF HYDRODEMOLITION IS USED, CEMENT AND PARTICULATE SLURRY
  MUST BE REMOVED FROM THE PREPARED SURFACES BEFORE SLURRY HARDENS

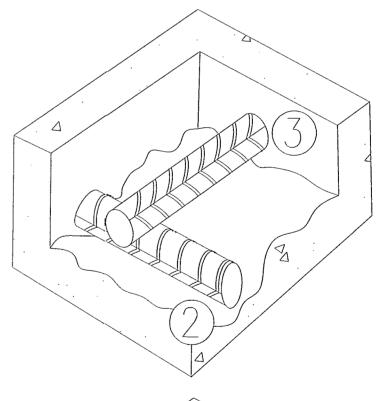


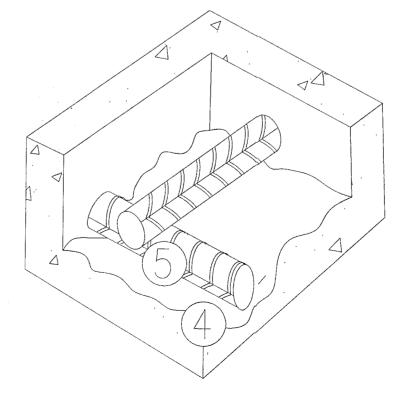
## **EXPOSING AND UNDERCUTTING OF REINFORCING STEEL**

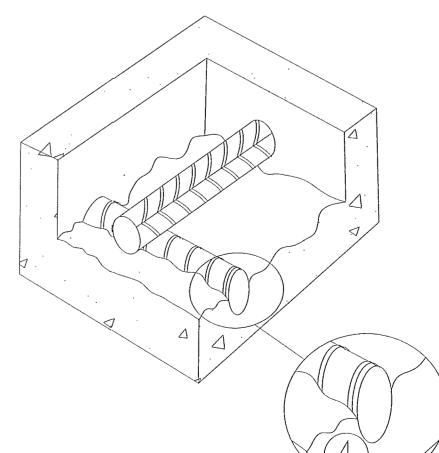
THESE DETAILS ARE APPLICABLE TO HORIZONTAL, VERTICAL, AND OVERHEAD LOCATIONS. THEY ARE ALSO APPLICABLE TO REMOVE BY HYDRO-DEMOLITION, HYDROMILLING, AND ELECTRIC, PNEUMATIC OR HYDRAULIC IMPACT BREAKERS.

- 1 REMOVE LOOSE OR DELAMINATED CONCRETE ABOVE CORRODED REINFORCING STEEL.
- ONCE INITIAL REMOVALS ARE MADE, PROCEED WITH THE UNDERCUTTING OF ALL EXPOSED CORRODED BARS. UNDERCUTTING WILL PROVIDE CLEARANCE FOR UNDER BAR CLEANING AND FULL BAR CIRCUMFERENCE BONDING TO SURROUNDING CONCRETE, AND WILL SECURE THE REPAIR STRUCTURALLY, PROVIDE MINIMUM 3/4" inch. (19mm) CLEARANCE BETWEEN EXPOSED REBARS AND SURROUNDING CONCRETE OR 1/4" (6mm) LARGER THAN LARGEST AGGREGATE IN REPAIR MATERIAL, WHICHEVER IS GREATER.
- 3 CONCRETE REMOVALS SHALL EXTEND ALONG THE BARS TO LOCATIONS ALONG THE BAR FREE OF BOND INHIBITING CORROSION, AND WHERE THE BAR IS WELL BONDED TO SURROUNDING CONCRETE.
- IF NON-CORRODED REINFORCING STEEL IS EXPOSED DURING THE UNDERCUTTING PROCESS CARE SHALL BE TAKEN NOT TO DAMAGE THE BAR'S BOND TO SURROUNDING CONCRETE IS BROKEN, UNDERCUTTING OF THE BAR SHALL BE REQUIRED.
- ANY REINFORCEMENT WHICH IS LOOSE SHALL BE SECURED IN PLACE BY TYING TO OTHER SECURED BARS OR BY WHEN APPROVAL METHODS.









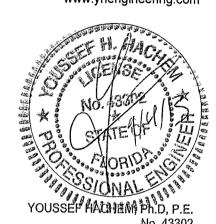


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SHEET NUMBER **S-2.** 

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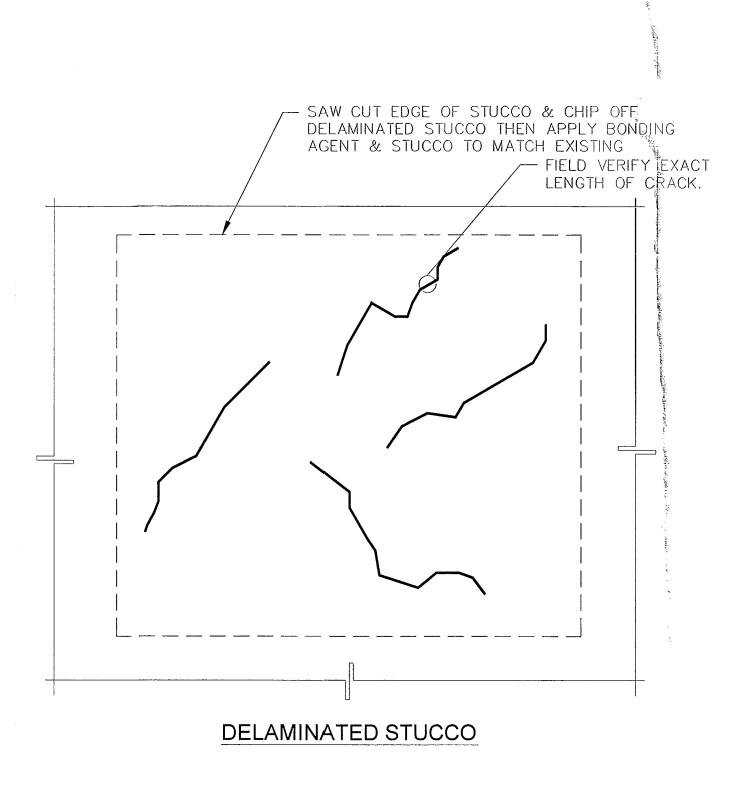
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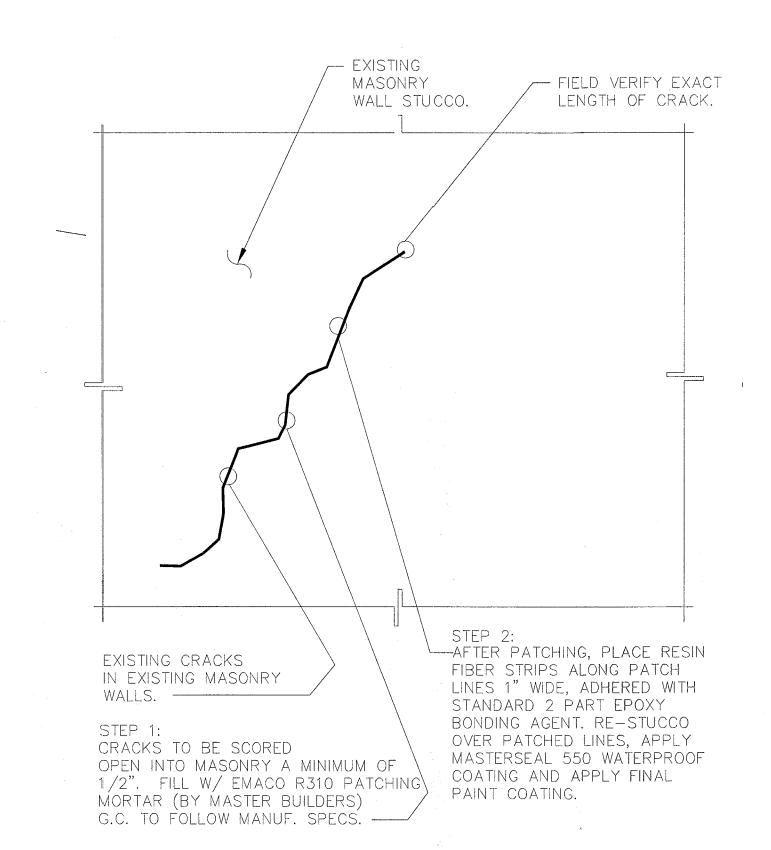
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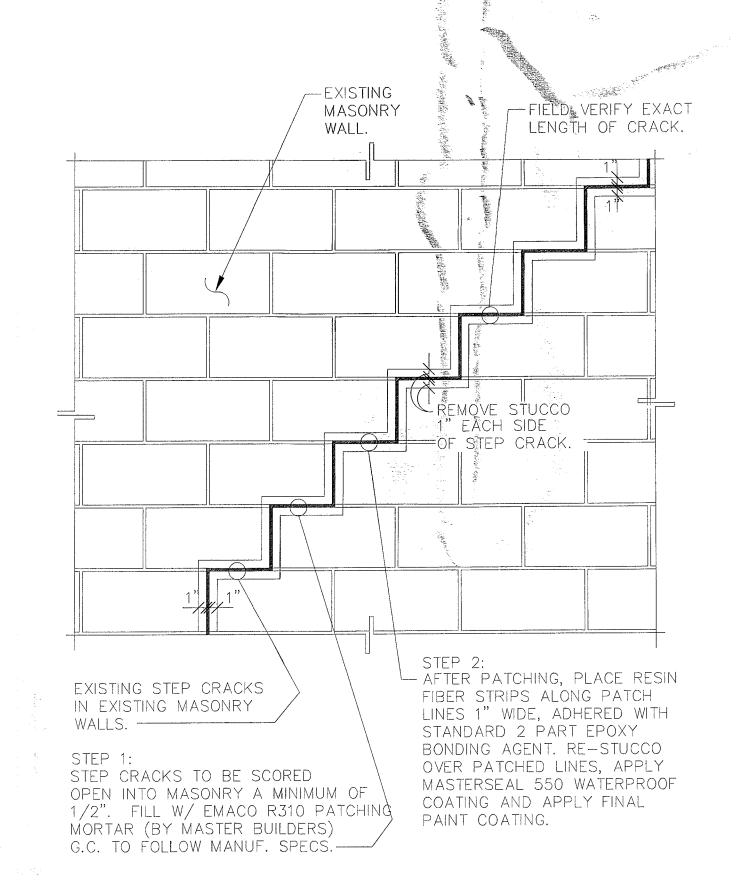
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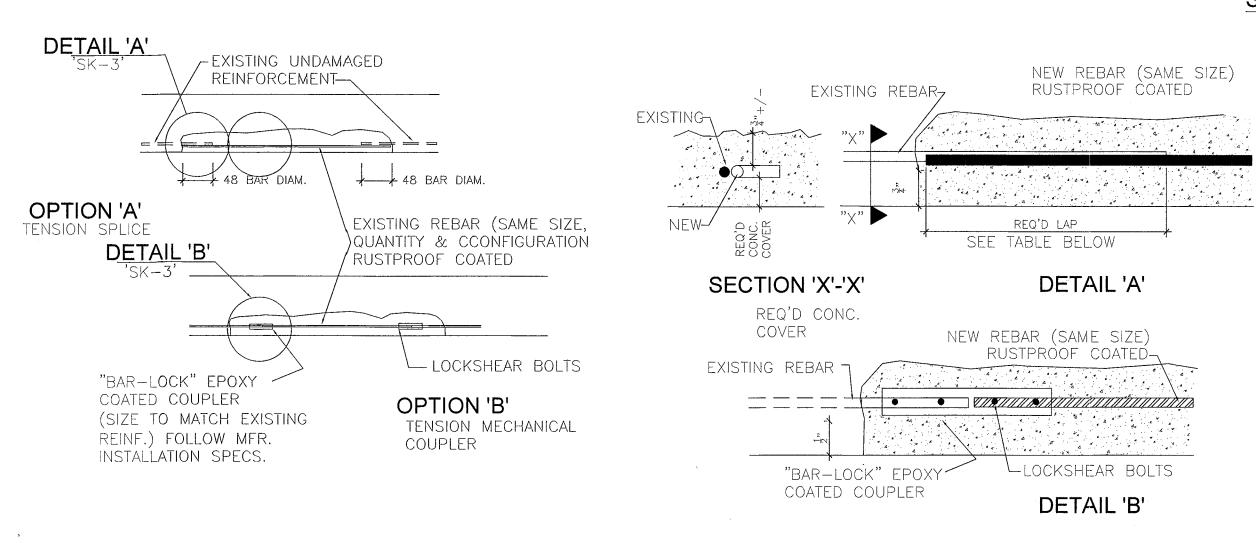
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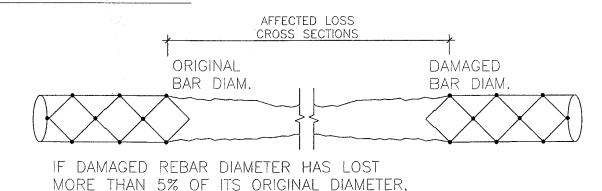






TOP REINF. REPAIR

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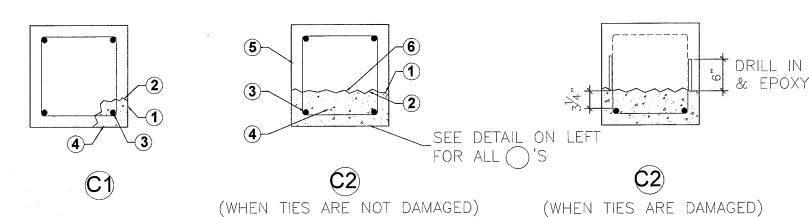
## DAMAGED REINFORCING

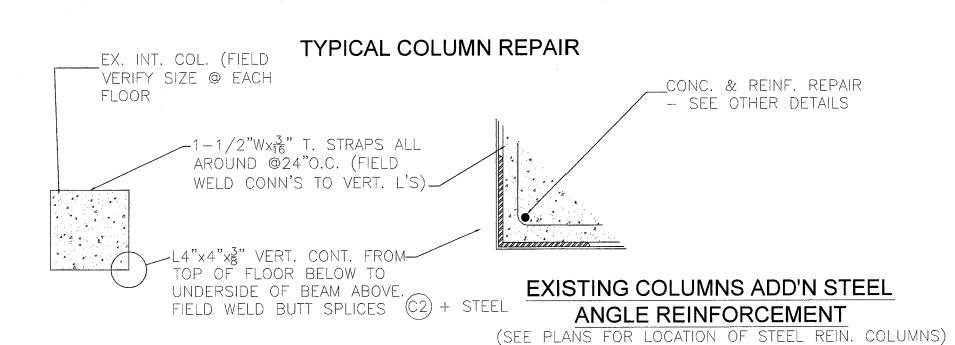
SEE OPTIONS 'A' OR 'B' FOR SPLICING NEW

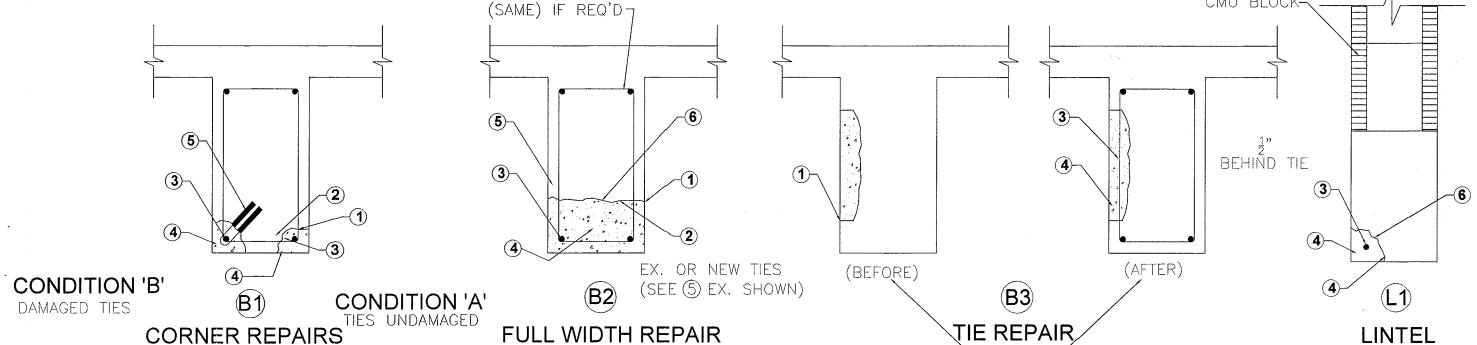
BAR SIZE	TENSION @ SLAB, BEAMS & RIBS F'C= 3000 PSI MIN	COMPRESSION COLUMNS
#3	21"	12"
#4	28"	12"
#5	36" *	14"
#6	43"	16"
#7	62"	19"
#8	71"	22"
#9	80"	25"

LAP LENGTH TABLE

STEP CRACK DETAIL









## CONCRETE REPAIR LEGEND

ALL REPAIR MATERIALS NAMED HERE ARE AS MANUFACTURED BY 'MASTER

1. SAW CUT 1/2" DEEP (90° TO THE SURFACE OF SLABS COLUMNS RIBS &

2. CHIP AND REMOVE CRACKED AND DAMAGED CONCRETE TO A MINIMUM DISTANCE OF 34" BEHIND REBARS, EXTEND CHIPPING TO FOLLOW THE REBARS LENGTH UNTIL SOUND CONCRETE IS ENCOUNTERED AND THE REBAR BEING EXPOSED IS NOT RUSTED. IF HAIRLINE CRACKS CONTINUE INTO OTHERWISE SOUND CONCRETE, CONTRACTOR TO EPOXY INJECT THE INNER

3. EXPOSE RUSTED REBARS. SAND BLAST CLEAN AND OBSERVE CROSS SECTION (SEE CROSS SECTION REDUCTION DETAIL FOR MORE INFORMATION). COAT REBAR WITH RUSTPROOF PAINT ('EMACO P-24'). NEW ADDED REBARS

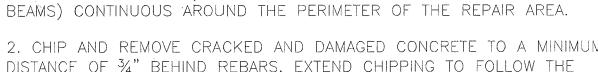
('EMACO S88 CI' OR 'MASTERPATCH 240 CR') ALTERNATIVELY CONCRETE APPLIED BY GUNITE MAY BE CONSIDERED. IF REQUIRED APPLY 'EMACO P-24' EPOXY BONDING AGENT TO EXISTING CONCRETE. ALL CONCRETE F'c = 5000 PSI MINIMUM.

5. ADD #3 HAIRPINS (DRILLED IN AND EPOXY BONDED) AT SAME SPACING AS ORIGINAL DAMAGED TIES.

6. EXISTING HAIRLINE TO MEDIUM SIZED CRACKS TO BE CLEANED AND INJECTED WITH 'SCB CONCRESIVE 1380' EPOXY INJECTION ADHESIVE. THE MOST SUITABLE INJECTION MATERIAL WILL BE DETERMINED AFTER EXPOSING AND CLEANING SOME OF THE EXISTING CRACKS.

7. LIGHTLY RUSTED REBAR (NOT ALL AROUND) TO BE CLEANED OBSERVED





CRACKS (WITH 'SCB CONCRESIVE 1380', BEFORE APPLYING PATCHING).

# SHALL BE PAINTED WITH SAME EPOXY REBAR COATING.

4. PATCH CONCRETE (TO ORIGINAL DIMENSIONS) WITH REPAIR MORTAR

AND COATED AS PER ITEM #3.

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