Tree Fifty-Eight



Ligustrum (*Ligustrum japonicum*), facing south. Note poor structure, deadwood and shaping.

**Tree Fifty-Nine** 



Coconut Palm (*Cocos nucifera*), facing north.



Note nutrient deficiencies and large trunk wounds (red arrow).

Tree Sixty



Coconut Palm (*Cocos nucifera*), facing south.



Note minor trunk wound.

**Tree Sixty-One** 



Ligustrum (*Ligustrum japonicum*), facing east.



Note poor structure, deadwood and shaping.

Tree Sixty-Two A



Ligustrum (*Ligustrum japonicum*), facing west.



Note poor structure, deadwood and shaping.

**Tree Sixty-Four** 



Brazilian Beautyleaf (*Calophyllum brasiliense*), facing south.



Note poor structure, over lifting, flush and stub cuts (red arrows).

**Tree Sixty-Five** 



Brazilian Beautyleaf (*Calophyllum brasiliense*), facing west.



Note poor structure, over lifting and trunk lean (east).

Tree Sixty-Six



Brazilian Beautyleaf (*Calophyllum brasiliense*), facing south.



Note poor structure, over lifting and trunk girdling (bracing strap) (red arrow).

**Tree Sixty-Seven** 



Black Olive (*Bucida buceras*), facing south.



Note poor structure, large diameter deadwood (red arrow), vertical trunk cracks (blue arrow) and girdling roots.

**Tree Sixty-Nine** 



Black Olive (*Bucida buceras*), facing south.



Note poor structure, deadwood (red arrow), over lifting and flush cuts.

**Tree Seventy** 



Brazilian Beautyleaf (<u>Calophyllum brasiliense</u>), facing east. Note poor structure, trunk girdling (bracing tape) (red arrow) and canopy crowding.

Tree Seventy-One



Brazilian Beautyleaf (*Calophyllum brasiliense*), facing west.



Note poor structure and canopy crowding.

Tree Seventy-Two



Brazilian Pepper (<u>Schinus terebinthifolia</u>), facing west.



Category 1 Exotic Invasive.

Page 74 of 74

#### **End Report**

Mach C William

ASCA Registered Consulting Arborist #580 ASCA Tree Plant Appraisal Qualified ISA Certified Arborist Municipal Specialist FL 5221-AM ISA Tree Risk Assessment Qualified LIAF Certified Landscape Inspector #2007-0083

## SURVEYOR'S NOTES:

PURSUANT TO TABLE OF REQUIREMENTS FROM THE "MINIMUM STANDARD DETAIL REQUIREMENTS FOR ALTA/ACSM LAND TITLE SURVEYS' WERE FOLLOWED AND ARE INCLUDED AS A PART OF THIS SURVEY: 2, 3, 4, 6(a), 6(b), 7(a), 7(b)(1), 7(c), 8, 9, 11(a) (as to utilities, surface matters only), 13, 16, 17, and 18.

ITEM 2: THE ADDRESS OF THIS PROPERTY IS:

4360 COLLINS AVENUE MIAMI BEACH, FL 33140

4370 COLLINS AVENUE MIAMI BEACH, FL 33140

THE FEDERAL EMERGENCY MANAGEMENT ASSOCIATION, (FEMA), NATIONAL FLOOD INSURANCE PROGRAM, (NFIP), INFORMATION FOR THIS SITE IS:

FLOOD INSURANCE RATE MAP, (FIRM), INDEX NUMBER: 12086CIND1A

FLOOD INSURANCE RATE MAP NUMBER: 12086C0328L FLOOD INSURANCE RATE MAP REVISED DATE, (MAP INDEX): SEPTEMBER 11, 2009

FLOOD INSURANCE RATE MAP NUMBER: 12086C0328L MAP REVISED DATE: SEPTEMBER 11, 2009 FLOOD INSURANCE RATE MAP PANEL: 328 OF 1031 COMMUNITY NAME: CITY OF MIAMI BEACH SUFFIX: L ZONES: AE and X, (CLEAR)

BASE FLOOD ELEVATION: AE – ELEVATION 7

X – AREAS DETERMINED TO BE OUTSIDE THE 0.2% ANNUAL CHANCE FLOODPLAIN

THE FLOOD ZONE DELINEATION LINES AS DEPICTED ON SHEETS 5 THROUGH 7 ARE APPROXIMATE AND ARE SHOWN FOR INFORMATION PURPOSES ONLY.

ITEM 4: THE GROSS LAND AREA FOR THIS PROPERTY IS:

EAST OF COLLINS AVENUE:

1.026 ACRES, (44,712 SQUARE FEET), MORE OR LESS.

WEST OF COLLINS AVENUE:

0.133 ACRES, (5,796 SQUARE FEET), MORE OR LESS.

<u>ITEM 6:</u>

AS OF THE DATE OF THIS ALTA/ACSM LAND TITLE SURVEY: (a) THE ZONING CLASSIFICATION FOR THIS PROPERTY IS:

RM-2, (RESIDENTIAL MULTIFAMILY, HIGH DENSITY);

(b) THE SETBACK REQUIREMENTS FOR THIS PROPERTY ARE:

VARY BY THE TYPE OF STRUCTURE. PLEASE SEE CITY OF MIAMI BEACH MUNICIPAL CODE CHAPTER 142, SECTION 247 FOR A DETAILED DESCRIPTION OR CONTACT THE CITY OF MIAMI BEACH PLANNING & ZONING DEPARTMENT.

THIS INFORMATION WAS OBTAINED FROM THE CITY OF MIAMI BEACH PLANNING & ZONING DEPARTMENT ON MARCH 08, 2012 VIA TELEPHONE CONVERSATION WITH A PLANNING & ZONING SPECIALIST.

(a) SEE SURVEY GRAPHICS FOR EXTERIOR DIMENSIONS OF ALL BUILDINGS AT GROUND LEVEL; (b), (1) SEE SURVEY GRAPHICS FOR SQUARE FOOTAGE AND FOOTPRINT OF ALL BUILDINGS AT GROUND LEVEL.

(c) NOT-APPLICABLE

ITEM 8: SEE SURVEY GRAPHICS FOR SUBSTANTIAL FEATURES OBSERVED IN THE PROCESS OF CONDUCTING THIS SURVEY.

<u>ITEM\_9:</u> NOT-APPLICABLE

<u>ITEM 11:</u> (a) SEE SURVEY GRAPHICS FOR OBSERVED EVIDENCE OF UTILITIES.

ITEM 13: SEE SURVEY GRAPHICS FOR THE NAMES OF THE ADJOINING OWNERS.

<u>ITEM 16:</u>

AS OF THE DATE OF THIS ALTA/ACSM LAND TITLE SURVEY, THERE IS NO EVIDENCE OF CURRENT EARTH MOVING WORK, BUILDING CONSTRUCTION OR BUILDING ADDITIONS.

ITEM 17: THERE IS NO EVIDENCE OF PROPOSED CHANGES IN STREET RIGHT OF WAY LINES OR OBSERVED EVIDENCE OF RECENT STREET OR SIDEWALK CONSTRUCTION OR REPAIRS.

<u>ITEM 18:</u> AS OF THE DATE OF THIS ALTA/ACSM LAND TITLE SURVEY, THERE IS NO EVIDENCE OF SITE USE AS A SOLID WASTE DUMP, SUMP OR SANITARY LANDFILL.

THE FOLLOWING SURVEYOR'S NOTES ARE REQUIRED AS A PART OF THE "STANDARDS OF PRACTICE FOR SURVEYING AND MAPPING" IN THE STATE OF FLORIDA, (SEE SURVEYOR'S CERTIFICATION):

A) DATE OF LAST FIELD WORK: MARCH 01, 2012

B) THE LEGAL DESCRIPTIONS AS SHOWN HEREON ARE BASED ON EITHER LEGAL DESCRIPTIONS FROM PRIOR SURVEYS OF THESE PROPERTIES AS PERFORMED BY CONSUL TECH SURVEYING & MAPPING, INC. UNDER PROJECT NUMBERS 97-0716, 97-0716.A, 01-0104, 01-010410, 01-010420, 01-010420.1, 01-010420.2, 01-010420.3, 01-010420.4, 01-010420.5, 01-010420.6, 01-010420.7, 01-010420.8, 01-010420.9, 01-010420.10, 01-010420.11, 01030120.D, 01-030140.A, 03-091020, 04-091920 AND 05-070920; LEGAL DESCRIPTIONS AS CREATED BY THIS COMPANY IN CONNECTION WITH PROJECTS ON THESE PROPERTIES, OR; VARIOUS TITLE COMMITMENTS REVIEWED BY THIS COMPANY DURING THE COURSE OF PERFORMING SURVEYS ON THESE PROPERTIES.

C) BEARINGS A SHOWN HEREON ARE BASED ON A PORTION OF THE COASTAL CONSTRUCTION CONTROL LINE AS RECORDED IN PLAT BOOK 74 AT PAGE 25, OF THE PUBLIC RECORDS OF MIAMI-DADE COUNTY, FLORIDA AND BEARS NORTH 07°16'18" EAST AS SHOWN HEREON AND ALL OTHER BEARINGS BEING RELATIVE THERETO. A PORTION OF THE EASTERLY RIGHT-OF-WAY LINE OF COLLINS AVENUE, (STATE ROAD A1A), BEARS NORTH 09°39'38" EAST RELATIVE TO THE COASTAL CONSTRUCTION CONTROL LINE AND IS A WELL IDENTIFIED AND MONUMENTED LINE.

D) ALL IMPROVEMENTS AS SHOWN HEREON THAT WERE LOCATED USING CONVENTIONAL SURVEYING METHODS AND PROCEDURES ARE BASED ON A CLOSED AND ADJUSTED TRAVERSE.

E) ALL IMPROVEMENTS AS SHOWN HEREON THAT WERE LOCATED USING GPS METHODS AND PROCEDURES ARE BASED ON REDUNDANT MEASUREMENTS.

F) THE SCALE OF SOME IMPROVEMENTS MAY HAVE BEEN EXAGGERATED FOR CLARITY AND REPRESENTATION.

NO UNDERGROUND EASEMENTS, ENCROACHMENTS, FOUNDATIONS OR UTILITIES HAVE BEEN LOCATED AS THIS WAS NOT A PART OF THE SCOPE OF SERVICES.

IMPROVEMENTS WITHIN THE INTERIOR OF THE BUILDINGS WERE NOT LOCATED ARE ARE NOT SHOWN.

ADDITIONS OR DELETIONS TO THIS SURVEY BY OTHER THAN THE SIGNING PARTY OR PARTIES IS PROHIBITED WITHOUT WRITTEN CONSENT OF THE SIGNING PARTY OR PARTIES.



# BOUNDARY SURVEY

THE FONTAINEBLEAU RESORT

4360 & 4370 COLLINS AVENUE, MIAMI BEACH FL





## LOCATION MAP IN SEC. 23 - TWP 53 SOUTH -42 EAST CITY OF MIAMI BEACH, MIAMI-DADE COUNTY, FLORIDA (NOT TO SCALE)

#### SHEET INDEX

COVER SHEET / SURVEYOR'S NOTES	1
LEGAL DESCRIPTIONS	2
BOUNDARY INFORMATION	2
TOPOGRAPHY INFORMATION	3

<ul> <li>THE FOLLOWING TITLE COMMITMENTS PREVIOUSLY REVIEWED WERE BASED ON:</li> <li>COMMITMENT FOR TITLE INSURANCE AGENT FILE NUMBER: HOTEL N12-026 ISSUED BY: STEWART TITLE AND GUARANTY CO. (HOUSTON) COMMITMENT NUMBER: 1200995-2801 FILE NUMBER: 1200995-2801 EFFECTIVE DATE: MARCH 2, 2012 AT 8:00 A.M.; REVISED APRIL 4, 2012 AND</li> <li>COMMITMENT FOR TITLE INSURANCE AGENT FILE NUMBER: TOWER 3 &amp; GARAGE N12-026 ISSUED BY: STEWART TITLE AND GUARANTY CO. (HOUSTON) COMMITMENT NUMBER: 1200994-2801 FILE NUMBER: 1200994-2801</li> <li>FILE NUMBER: MARCH 2, 2012 AT 8:00 A.M.; REVISED MARCH 19, 2012 REVIEWED BY C.S.A. GROUP.</li> <li>C) PLAT NAMES AS SHOWN HEREON, (EITHER IN THE LEGAL DESCRIPTIONS AND / OR ON THE FACE OF THE DRAWINGS), MAY HAVE BEEN PARTIALLY ABBREVIATED. THERE ARE TWO PLATS THAT MAKE UP THE MAIN PARCELS AS SHOWN ON THE EAST SIDE OF INDIAN CREEK DRIVE AND COLLINS AVENUE. THE COMPLETE NAMES OF THE PLATS ARE AS FOLLOWS:</li> <li>AMENDED PLAT OF THE INDIAN BEACH CORPORATION'S SUBDIVISION OF LANDS IN GOV'T. LOTS 1-2-3-4-5-6 AND OF SEC.3-TWP.53S-RGE.42E, (PLAT BOOK 8 AT PAGE 61 OF THE PUBLIC RECORDS OF MIAMI-DADE COUNTY, FLORIDA)</li> <li>AND</li> <li>AMENDED MAP OF THE OCEAN FRONT PROPERTY OF THE MIAMI BEACH IMPROVEMENT COMPANY, (PLAT BOOK 5 AT PAGES 7-8 OF THE PUBLIC RECORDS OF MIAMI-DADE COUNTY, FLORIDA)</li> </ul>	ORDER #     DATE     F.B. #     COMMENTS       03-86658     3-11-20     N/A     REVISE SURVEY FILED TO SHOW ALL PARCEL LESS PARCEL "1,2,3,5,A,C,D AND F"       03-86658     3-11-20     N/A     REVISE SURVEY FILED TO SHOW ALL PARCEL LESS PARCEL "1,2,3,5,A,C,D AND F"       03-86658     3-11-20     N/A     REVISE SURVEY FILED TO SHOW ALL PARCEL LESS PARCEL "1,2,3,5,A,C,D AND F"       03-86658     3-11-20     N/A     REVISE SURVEY FILED TO SHOW ALL PARCEL LESS PARCEL "1,2,3,5,A,C,D AND F"
<ul> <li>PARCEL "E", AS SHOWN HEREON, CONSTITUTES THE PROPOSED FUTURE "SOUTH PARKING GARAGE", AS DESCRIBED ON SHEET 2 AND GRAPHICALLY DEPICTED ON SHEET(S) 2.</li> <li>1) THE PORTIONS OF PARCELS 1 THROUGH 5 LOCATED EAST OF COLLINS AVENUE AND NORTH OF 44th STREET, (NEW), ARE ALL CONTIGUOUS TO EACH OTHER, WITHOUT GAPS, GORES OR HIATUSES ALONG THEIR COMMON BOUNDARIES.</li> <li>PARCEL "E" ARE CONTIGUOUS TO COLLINS AVENUE AND 44th STREET, (NEW), WITHOUT GAPS, GORES OR HIATUSES ALONG THEIR COMMON BOUNDARIES.</li> <li>J) BEARINGS AND DISTANCES ARE CALCULATED UNLESS OTHERWISE NOTED.</li> <li>K) THERE MAY BE EASEMENT, RESTRICTIONS OR OTHER MATTERS OF RECORD NOT SHOWN HEREON THAT MAY BE FOUND IN THE PUBLIC RECORDS OF MIAMI-DADE COUNTY, FLORIDA.</li> <li>L) THE EROSION CONTROL LINE AS RECORDED IN PLAT BOOK 105, AT PAGE 62, AND OFFICIAL RECORDS BOOK 9517 AT PAGES 2028-2031, BOTH RECORDED IN THE PUBLIC RECORDS OF MIAMI-DADE COUNTY, FLORIDA.</li> <li>L) THE EROSION CONTROL LINE AS RECORDED IN PLAT BOOK 105, AT PAGE 62, AND OFFICIAL RECORDS BOOK 9517 AT PAGES 2028-2031, BOTH RECORDED IN THE PUBLIC RECORDS OF MIAMI-DADE COUNTY, FLORIDA, ARE ONE AND THE SAME AND A PORTION OF WHICH COMPRISES THE EASTERLY BOUNDARY OF PARCEL "A", ('HOTEL SITE').</li> <li>M) THE COASTAL CONSTRUCTION CONTROL LINE AS SHOWN HEREON IS BASED ON INFORMATION AS SHOWN IN PLAT BOOK 74 AT PAGE 25, RECORDED ON FEBRUARY 10, 1982 OF THE PUBLIC RECORDS OF MIAMI-DADE COUNTY, FURDIDA, AS WELL AS INFORMATION PROVEDED TO THIS SURVEYOR BY THE MIAMI-DADE COUNTY, PLUBLIC WORKS DEPARTMENT, SURVEY SECTION.</li> <li>N) BUILDING AND IMPROVEMENT TIES TO THE COASTAL CONSTRUCTION CONTROL LINE, (CCCL), AS SHOWN HEREON ARE PER THE REQUEST OF THE CLIENT.</li> <li>O) WE HEREBY CERTIFY THAT THE LEGAL DESCRIPTION IS THE SAME AS SET FORTH IN THE VESTING DEED AS REFERENCE IN THE THE COMMITMENT.</li> <li>P) BOUNDARY AND TOPOGRAPHIC INFORMATION SHOW HERE ON WAS FIELD VERIFIED BY BISCAYNE ENGINEERING COMPANY.(09/18/2019)</li> <li>(R) ORIGINAL SURVEY INFORMATION WAS PREPARED BY C.S.A. GRO</li></ul>	In the properting company, inc. In the properting company, inc. In the property inc. In the p
<ul> <li>i) B-313, ELEVATION = 4.33 FEET (NGVD-29) ,36 ST 81.7' SOUTH OF SOUTH CURB,HWY A-1-A (COLLINS AVE) 57.8' EAST OF EAST CURB,US C &amp; G BRASS DISC ON TOP OF CONC RAMP DIRECTLY OVER A CATCH BASIN.</li> <li>i) D-313, ELEVATION = 6.17 FEET (NGVD-29) ,46 ST 41.2' SOUTH OF SOUTH CURB LINE OF ENTRANCE TO PARKING LOT, INDIAN CREEK DRIVE 19' EAST OF EAST CURB. US C &amp; G BRASS DISC IN TOP OF NE CORNER OF A 4' SQUARE CONC WALL</li> </ul>	- SINCE 1898 - SL
SURVEYOR'S CERTIFICATION: I hereby certify that the attached "SURVEY" complies with the Standards of Professional Surveyors and Mapping set farth by the State of Florida Board of Professional Surveyors and Mappers in chapter SJ-17, Florida Administrative Code, pursuant to chapter 472.027, Florida Statutes. MICON VALID WITHOUT THE ORIGINAL SIGNATURE AND SEAL OF A FLORIDA LICENSED SURVEYOR AND MAPPER. Biscourse Engineering Company, inc. S26 West Flogier Street, Miami, FL. 33130 305–324-761 State of Florida Department of Agriculture LID DOR A FGT SURVEY DATE: 09–18–2019 SURVEY DATE: 09–18–2019 SELWIN BRUCE, PSM for the FIRM Professional Surveyor and Mapper No. 5290 State of Florida	Initial ordering is the property of biscorine engineering company, inc. and shun hou be used of reproduced, in whole of its used of the used of reproduced, in whole of its used of the used of reproduced, in whole of its used of the used of reproduced, in whole of its used of the used of reproduced, in whole of its used of the used of reproduced, in whole of its used of the used of reproduced, in whole of its used of the used of reproduced, in whole of its used of the used of reproduced, in whole of its used of the used of the used of reproduced, in whole of its used of the used of reproduced, its used of the used of reproduced, its used of the used of



## BOUNDARY SURVEY

## LEGAL DESCRIPTION

LOTS 1 AND 2, BLOCK 40, OF AMENDED PLAT OF OCEAN FRONT PROPERTY OF THE MIAMI BEACH IMPROVEMENT COMPANY, ACCORDING TO THE PLAT THEREOF, AS FILED FOR RECORD IN PLAT BOOK 5, AT PAGES 7 AND 8, OF THE PUBLIC RECORDS OF MIAMI-DADE COUNTY, FLORIDA;

TOGETHER WITH A PORTION OF THAT UNNUMBERED TRACT OF LAND DESIGNATED AS "J.H. SNOWDEN" LYING NORTH OF AND ADJACENT TO LOT 1, BLOCK 40, IN SAID AMENDED PLAT OF OCEAN FRONT PROPERTY OF THE MIAMI BEACH IMPROVEMENT COMPANY AND MORE PARTICULARLY

BEGINNING AT THE NORTHWEST CORNER OF SAID LOT 1, BLOCK 40; THENCE NORTH 64.55 FEET ALONG INDIAN CREEK DRIVE TO A POINT; THENCE EAST 228.23 FEET TO A POINT; THENCE SOUTH 64.55 FEET ALONG COLLINS AVENUE TO THE NORTHEAST CORNER OF SAID LOT 1, BLOCK 40; THENCE WEST ALONG THE NORTH LINE OF SAID LOT 1. BLOCK 40 TO THE POINT OR PLACE OF BEGINNING

LESS THAT CERTAIN PROPERTY DESCRIBED IN WARRANTY DEED MADE BY BOARDRLPPLE INDIAN CREEK, INC., A FLORIDA CORPORATION, TO CITY OF MIAMI BEACH, A MUNICIPAL CORPORATION, DATED AUGUST 13, 1953, FILED FOR RECORD JUNE 30, 1954 IN DEED BOOK 3940, PAGE 284 PUBLIC RECORDS, MIAMI-DADE COUNTY, FLORIDA

ALSO LESS THAT PORTION OF THE ABOVE DESCRIBED PROPERTY DEEDED TO THE CITY OF MIAMI BEACH FOR ROAD RIGHT-OF-WAY PURPOSES BY REASON OF SPECIAL WARRANTY DEED DATED NOVEMBER 16, 2001, AND FILED FOR RECORD NOVEMBER 19, 2001, IN OFFICIAL RECORDS BOOK 20025, PAGE 4698, PUBLIC RECORDS OF MIAMI-DADE COUNTY, FLORIDA, MORE PARTICULARLY DESCRIBED AS FOLLOWS:

A PORTION OF THAT CERTAIN TRACT OF LAND DESIGNATED AS "J.H. SNOWDEN" LYING NORTH OF AND ADJOINING LOT 1. BLOCK 40. OF AMENDED MAP OF THE OCEAN FRONT PROPERTY OF THE MIAMI BEACH IMPROVEMENT COMPANY ACCORDING TO THE PLAT THEREOF, AS RECORDED IN PLAT BOOK 5, AT PAGES 7 AND 8, OF THE PUBLIC RECORDS OF MIAMI-DADE

COUNTY, FLORIDA, AND A PORTION OF SAID LOT 1, BLOCK 40, BEING MORE PARTICULARLY DESCRIBED AS FOLLOWS:

COMMENCE AT THE NORTHWEST CORNER OF THAT CERTAIN TRACT OF LAND DESIGNATED AS "R.P. VAN CAMP" AS SHOWN ON SAID "AMENDED MAP OF THE OCEAN FRONT PROPERTY OF THE MIAMI BEACH IMPROVEMENT COMPANY" PLAT; THENCE SOUTH 07' 25' 11" WEST ALONG THE WEST LINE OF SAID 'R.P. VAN CAMP" TRACT, AND THE WEST LINE OF LOT 1, BLOCK 39, OF SAID "AMENDED MAP OF THE OCEAN FRONT PROPERTY OF THE MIAMI BEACH IMPROVEMENT COMPANY" PLAT, SAID LINE ALSO BEING THE EAST RIGHT-OF-WAY LINE OF COLLINS AVENUE, FOR A DISTANCE OF 220.45 FEET; THENCE NORTH 82'34'49" WEST, FOR A DISTANCE OF 60.00 FEET TO A POINT ON THE EAST LINE OF SAID LOT 1, BLOCK 40, SAID LINE ALSO BEING THE WEST RIGHT-OF-WAY LINE OF COLLINS AVENUE, AND SAID POINT ALSO BEING THE POINT OF BEGINNING; THENCE NORTH 37'35'00" WEST FOR A DISTANCE OF 35.36 FEET; THENCE NORTH 82' 34'49" WEST ALONG A LINE PARALLEL WITH AND 4.55 FEET NORTH OF AS MEASURED AT RIGHT ANGLES TO THE SOUTH LINE OF SAID "J.H. SNOWDEN" TRACT, FOR A DISTANCE

OF 200.22 FEET TO A POINT ON THE WEST LINE OF SAID "J.H. SNOWDEN" TRACT, SAID LINE ALSO BEING THE EAST RIGHT-OF-WAY LINE OF INDIAN

THENCE NORTH 04"33'25" EAST ALONG THE LAST DESCRIBED LINE, FOR A DISTANCE OF 83.06 FEET TO A POINT OF CURVATURE OF A CIRCULAR CURVE TO THE RIGHT; THENCE ALONG THE ARC OF SAID CURVE, HAVING A RADIUS OF 50.00 FEET, A CENTRAL ANGLE OF 27'21'20" FOR A DISTANCE OF 23.87 FEET TO A POINT ON THE ARC OF A CIRCULAR CURVE TO THE LEFT BEING NON-TANGENT WITH THE LAST DESCRIBED CURVE AND WHOSE RADIUS POINT BEARS NORTH 74'49'14" EAST; THENCE ALONG THE ARC OF SAID CURVE HAVING A RADIUS OF 75.00 FEET, A CENTRAL ANGLE OF 67'24'03" FOR A DISTANCE OF 88.23 FEET TO THE POINT OF TANGENCY; THENCE SOUTH 82'34'49" EAST, ALONG A LINE PARALLEL WITH AND 64.55 FEET NORTH OF AS MEASURED AT RIGHT ANGLES TO THE SOUTH LINE OF SAID "J.H. SNOWDEN" TRACT, FOR A DISTANCE OF 148.91 FEET; THENCE NORTH 47'19'52" EAST FOR A DISTANCE OF 10.57 FEET; THENCE SOUTH 07'25'11" WEST ALONG THE EAST LINE OF SAID "J.H. SNOWDEN" TRACT AND THE EAST LINE OF SAID LOT 1, BLOCK 40, SAID LINE ALSO BEING THE WEST RIGHT-OF-WAY LINE OF COLLINS AVENUE FOR A DISTANCE OF 93.11 FEET TO THE POINT OF BEGINNING

TOGETHER WITH THAT CERTAIN STRIP OF LAND LYING BETWEEN INDIAN CREEK DRIVE AND INDIAN CREEK WHICH IS BOUNDED ON THE SOUTH BY THE SOUTHERLY LINE OF LOT 1, BLOCK 40, AS EXTENDED WESTERLY TO SAID INDIAN CREEK; AND BOUNDED ON THE NORTH BY THE NORTHERLY LINE OF SAID "J.K. SNOWDEN" PARCEL, AS EXTENDED WESTERLY TO SAID INDIAN CREEK AND BEING PARALLEL TO AND APPROXIMATELY 240.30 FEET NORTHERLY OF THE SAID SOUTHERLY BOUNDARY LINE.

PA	RCEL	OWNERSH	IP									
PA	RCEL	OWNER										
1.	FONT	AINEBLEAU	FLORIDA	HOTEL,	LLC,	A	DELAW	ARE	LIMITED	LIABILITY	СОМ	PANY
2.	FONT	AINEBLEAU	FLORIDA	HOTEL,	LLC,	А	DELAW	ARE	LIMITED	LIABILITY	СОМ	PANY
3.	FONT	AINEBLEAU	FLORIDA	HOTEL,	LLC,	А	DELAW	ARE	LIMITED	LIABILITY	СОМ	PANY
4.	FONT	AINEBLEAU	FLORIDA	HOTEL,	LLC,	А	DELAW	ARE	LIMITED	LIABILITY	СОМ	PANY
5.	FONT	AINEBLEAU	FLORIDA	HOTEL,	LLC,	А	DELAW	ARE	LIMITED	LIABILITY	СОМ	PANY
C.	FONT	AINEBLEAU	FLORIDA	HOTEL,	LLC,	А	DELAW	ARE	LIMITED	LIABILITY	СОМ	PANY
D.	FONT	AINEBLEAU	FLORIDA	HOTEL,	LLC,	А	DELAW	ARE	LIMITED	LIABILITY	СОМ	PANY
E.	FONT	AINEBLEAU	FLORIDA	HOTEL,	LLC,	А	DELAW	ARE	LIMITED	LIABILITY	СОМ	PANY
F.	FONT	AINEBLEAU	FLORIDA	TOWER	2, LLC,	A	DELAW	ARE	LIMITED	LIABILITY	COM	IPANY
TO۱	NER ii	i FONTAINE	BLEAU FL	ORIDA	TOWER 3	3,	LLC, A	FLO	RIDA LIM	ITED LIABI	LITY	COMPANY

CURVE TABLE							
CURVE	DELTA	LENGTH	RADIUS				
Α	92°14'27"	120.74'	75.00'				
В	67°24'03" RADIAL BE S74°49'14"	75.00 <b>'</b>					
С	90°00'00"	78.54'	50.00'				
D	65°30'23"	57.17 <b>'</b>	50.00'				
E	24°50'24"	32.52'	75.00'				
F	27°21'21"	23.87'	50.00'				
G	92°14'27"	116.56'	72.40'				

TOWER III FONTAINEBLEAU TOWER 3 GARAGE GARAGE AND RESTAURANT, LLC, A FLORIDA LIMITED RESTAURANT LIABILITY COMPANY

PTION	(C)	- CALCULATED
	¢	- CENTERLINE
	Ĺ	<ul> <li>ARC LENGTH</li> </ul>
D LIGHT	R	- RADIUS
Y RECORDS	D	- CENTRAL ANGLE
BOOK	Sg.Ft.	– SQUARE FEET
	Ι.Ρ.	- IRON PIPE
3		
MENT		

- DENOTES FND. NAIL AND DISC - LB# 3527

- DENOTES FND. 5/8" IRON ROD AND CAP - LB# 3527 - DENOTES FOUND NAIL AND TIN TAB - LB# 166

STRUCTURE PARCELS AFFECTED	
FONTAINEBLEAU HOTEL	1
FONTAINEBLEAU 2	3, 4, 5, F
FONTAINEBLEAU III	1, 3
FONTAINEBLEAU IV (PROPOSED NORTH TOWER)	2, C
BALLROOM	2, C
COCONUT WILLIES	1
MARINA PARCEL	D
PROPOSED SOUTH PARKING GARAGE	E

PARCEL DESIGNATION

the property of Biscayne <b>4360 &amp; 4</b> FOR: FONTAINEBLE SCALE: 1":30' DESI DATE: 09/18/19 APPI	Engineering Company, Inc. and shall not be used or reproduced, in whole or in part without permission of Biscayne Engineering Company, Inc.	MIAMI-DADE ORDER # DATE F.B. # COMMENTS	4370 Collins Avenue. Miami Beach FL			TEL (561) 609-2329	SURVEYORS • ENGINEERS E-MAIL INFOMINISCAVNEENING COM	
+	the property of Biscayne Engineering Company, Inc. ar		4360 & 4370 Collins A		TUN: FUNIAINEBLEAU DEVELUTMENI			UAIE. U3/ 10/ 13 AFFRUVED DI. 3.5.



	SYMBOL LEGEND							
۲	BOLLARD / POST							
_	BACKFLOW PREVENTER							
BELL	TELEPHONE SERVICE BOX							
	CATCH BASIN							
÷	TREE							
×	PALM TREE							
0	CLEANOUT							
0	IRRIGATION VALVE COVER							
$\psi^{\rm C}_{\rm A}$	WATER VALVE COVER							
$\square$	ELECTRIC BOX							
GD	GREASE TRAP							
¢	LIGHT POLE							
$\square$	STORM MANHOLE							
E	ELECTRIC MANHOLE							
S	SANITARY SEWER MANHOLE							
P	PARKING METER							
	SINGLE SUPPORT SIGN							
(TRAF)	TRAFFIC CONTROL BOX							
Ô	TRAFFIC LIGHT POLE							
icv X	IRRIGATION VALVE							
sv ⊠	SEWER VALVE							
WM	WATER METER							
0	MONITORING WELL							
♦	FIRE HYDRANT							
⊜	DRAIN							
•	YARD DRAIN							
P	PROPERTY LINE							
€	GROUND LIGHT FIXTURE							

PH.	ASPHALT
3.S.	CONCRETE BLOCK STRUCTURE
	CHAIN-LINK
NC.	CONCRETE
.P.	DUCTILE IRON PIPE
/	IRRIGATION CONTROL VALVE
√.C.	POLYVINYL CHLORIDE
۶.	SPLIT-RAIL
P.	TYPICAL
K.	UNKNOWN PURPOSE
)	CALCULATED
5.5 = GRC (TYPIC	DUND SURFACE ELEVATION
s≂ HARD	SURFACE ELEVATION (TYPICAL)







#### BOUNDARY SURVEY THE FONTAINEBLEAU RESORT 4360 & 4370 COLLINS AVENUE, MIAMI BEACH FL TITLE POLICY DATA NOTE: SOME ITEMS SHOWN ON THIS TABLET MAY NOT AFFECT PROPERTY STEWART TITLE AND GUARANTY CO. (HOUSTON) Effective Date: Septembet 24, 2013 at 8:00 A.M.; Revised October 14,2013. Schedule B-II Affects / Does Plottable / Not mment Not Affect Plottable Affects Not Plottable is is not a survey related item, (Defects, liens, encumbrances, adverse claims or other matters, ...) Affects Not Plottable is is not a survey related item, (Standard Exceptions) Affects Not Plottable is is not a survey related item, (Taxes and assessments for the year 2013 and subsequent years, ...) 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FLAGLER ST, MIAMI, FL 33130 TEL (305) 324-7671, FAX (305) 324-0809 PALM BEACH 449 NW 35TH ST, BOCA RATON, FL 33431 TEL (561) 609-2329 Affects Plat of Property, (See Survey) Plottable Affects Coastal Construction Control Line, (See Survey) Plottable osion Control Line, (See Survey) Affects Plottable Affects rosion Control Line, (See Survey) Plottable Affects Not Plottable This is not a survey related item, (Riparian right, rights of accretion, reliction, submerged lands or ...) Affects Not Plottable This is not a survey related item, (Any adverse ownership claim by the State of Florida by right of ...) 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1750 PONCE DE LEON BOULEVARD | CORAL GABLES, FLORIDA 33134 305•447•0900 | DPA@DPLUMMER.COM

February 27, 2020

Firat Akcay, M.S.C.E. MBA Transportation Analyst Transportation and Mobility Department 1688 Meridian Avenue, Suite 801 Miami Beach, FL 33139 305-673-7000, ext 6839 FiratAkcay@miamibeachfl.gov

## RE: <u>The Fontainebleau Hotel Ballroom and Parking Garage Traffic Statement</u> - #19185

Dear Firat,

The proposed project is located at 4441 Collins Avenue in Miami Beach, Florida. The project is proposing to develop an existing Fontainebleau Hotel surface parking lot (at the southeast corner of the Collins Avenue / W 44<sup>th</sup> Street intersection) into a hotel ballroom and parking garage with approximately 278 parking spaces. The existing surface parking lot is currently used for employees. The proposed parking garage will also be restricted to employees. Additionally the proposed project will include a pedestrian bridge that connects the ballroom / garage building to the main campus, providing access to all guests. There is no guest drop-off/pick-up at the proposed building. Guests will use the existing arrival and departure valet areas at the main campus, keeping valet operations internal within the current operations. See Attachment A for the proposed site plan. Exhibit 1 shows the location of the project.

This traffic statement documents project location / background, trip generation analysis, intersection capacity analysis, valet operations / queuing, AutoTurn and circulation analysis.









## Traffic Analysis Methodology

The intersection analysis was conducted for the AM and PM peak hours of a regular weekday, and was based on the typical requirements for the City of Miami Beach. The methodology used in the analysis is outlined below:

- Traffic Counts Two-hour turning movement counts for the AM (7-9 AM) and PM (4-6 PM) peak hours were collected on January 22, 2020 at the Indian Creek Drive / 44<sup>th</sup> Street intersection, and are provided in Attachment B.
- Signal Location and Timing Existing signal phasing and timing for the signalized intersection were obtained from Miami-Dade County (see Attachment B).
- Background Traffic Available Florida Department of Transportation (FDOT) and Miami-Dade County (MDC) counts were consulted to determine a growth factor consistent with historical annual growth in the area. The growth factor was applied to the existing traffic volumes to establish background traffic.
- Future Transportation Projects The 2020 TIP and the 2045 LRTP were reviewed and considered in the analysis at project build-out.
- Analysis Intersection analysis was done using the Synchro software based on <u>Highway</u> <u>Capacity Manual</u> (HCM 6<sup>th</sup> Edition).

## **Traffic Data Collection**

Signal timing data was obtained from Miami-Dade County for the analyzed signalized intersection in this study. This information was used for the signal phasing and timing required for the intersection capacity analysis. A field survey was conducted to obtain the lane configurations used in the intersection analysis. Exhibit 2 shows the existing lane configurations. Signal timings are also provided in Attachment B.

Vehicle turning movement counts were collected on January 22, 2020 at the study intersection during the AM (7-9 AM) and PM (4-6 PM) peak periods. The counts were adjusted to reflect average annual daily traffic conditions using the latest weekly volume adjustment factors obtained from FDOT. A weekly volume adjustment factor of 1.04 (Miami-Dade County North) corresponding to the dates of the counts was used. Traffic counts are provided in Attachment B. Traffic volumes used in the analyses are shown in Exhibit 2.









## **Existing Conditions Intersection Capacity Analysis**

The Synchro software was used to perform intersection capacity analysis. Synchro is a macroscopic analysis and optimization software application that implements the Intersection Capacity Utilization method for determining intersection capacity. Synchro also supports the Highway Capacity Manual's methodology for signalized intersections. Exhibit 3 shows the resulting Level of Service (LOS) for AM and PM peak hour conditions. The analysis shows that the Indian creek Drive/ 44<sup>th</sup> Street intersection currently operates at LOS B and C during the AM and PM peak hours respectively. Capacity worksheets are included in Attachment C.

Weekday AM and PM Peak Hour Conditions									
<b>T</b> , , , , ,	Signalized/	D: (:	AM	Peak	PM Peak				
Intersection	Un-signalized	Direction	LOS	Delay	LOS	Delay			
Indian Creek Drive / 44th Street	S	NB SB WB <b>Overall</b>	А А Е <b>В</b>	5.4 3.1 57.3 11.9	B A D C	13.4 4.8 54.9 <b>23.1</b>			

Exhibit 3 Existing Conditions Intersection Capacity Analysis Weekday AM and PM Peak Hour Conditions

## **Future Conditions**

Average Daily Traffic counts published by the Miami-Dade Public Works Department and the FDOT were reviewed to determine historic growth in the area. This analysis indicated that the growth rate is 0.3% in the past years. However, a conservative 0.5% annual growth rate was used for the analysis. Historic growth rate documentation is included in Attachment B. In order to obtain future conditions for the year 2022, two years of background growth were applied to the existing traffic counts.



#### **Trip Generation and Distribution Analysis**

A trip generation analysis was conducted for the proposed ballroom facilities. Trip generation for the project was based on the number of attendees expected at each type of space (ballroom, Jr. ballroom, and meeting space. In order to quantify daily and peak hour vehicle trips, percentages and rates were applied based on data provided by the Fontainebleau Development and engineering judgement. (See Attachment D for trip generation documentation). Percentages and rates include ballroom square footage per attendee, percent of attendees that are internal (hotel guests), vehicle occupancy, and percent of trips arriving during the peak hour. Similarly, trips associated with event employees were also calculated. The calculations for the peak hours assumed that not all of the ballroom space will be in operation simultaneously. Exhibit 4 shows the calculations for the proposed ballroom spaces and Exhibit 5 show the trip generation summary.

Proposed Ballroom Trip Generation									
Calculations	Ballroom	Jr. Ballrom	Meeting	Space	Percentages / Rates Applied				
Area	16,247 SF	9,038 SF	6,249 SF	-					
Number of Attendees	464	258	178	35	SF/person <sup>1</sup>				
Attendees - Internal	450	250	173	97%	internal <sup>1</sup>				
Attendees - External	14	8	5	3%					
External Vehicles Trips	7	4	2	2	persons/auto <sup>2</sup>				
Peak Hour Trips	5	3	2	75%	arrive/depart during the peak hour				
Number of Employees	32	18	11	7%	of attendees <sup>3</sup>				
Employees arriving by car	25	14	9	78%	(Other modes of transportation at 22%) $^4$				
Employees Vehicles Trips	23	13	8	1.1	persons/auto <sup>5</sup>				
Employees Peak Hour Trips	8	4	3	35%	arrive/depart during the peak hour				
Total Daily Vehicle Trips	30	17	10						
Total Peak Hour Vehicle Trips	13	7	4						

## EXHIBIT 4

(1) Based on data provided by Fontainebleau Development

(2) Based on data provided by Miami Beach

(3) Based on information provided by Fontainebleau Development

(4) Based on survey data provided by Fontainebleau Development

(5) Calculated based on survey data provided by Fontainebleau Development



### **EXHIBIT 5**

	-	-		
Peak Hour	AN	1 Peak H	our	
Ballroom Trips	13	IN	80%	
		OUT	20%	
Jr. Ballroom Trips	7			
		PN	1 Peak Ho	our
Meeting Space Trips	5	IN	30%	
		OUT	70%	
Subtotal Trips (All Venues)	25			
Average % of Rented Events Space	60%			
Total Vehicle Trips	15			

<b>Proposed Trip Generation S</b>	ummary
-----------------------------------	--------

12 3

5

10

Daily	
Ballroom Trips	30
Jr. Ballroom Trips	17
Meeting Space Trips	10
Total Vehicle Trips	57

Ballroom event guest will be using the existing valet arrival and departure area at the Fontainebleau Hotel. Valet trips will remain internal to the main property. Employees will be accessing the proposed parking garage via the inbound driveway on Indian Creek Drive and the two-way driveway on Collins Avenue. For estimating trip distribution for the project traffic, consideration was given to conditions such as the roadway network accessed by the project traffic, roadways available to travel in the desired direction, and attractiveness of traveling on a specific roadway. Project trip distribution for both guest and employees of the proposed project are shown on Exhibits 6 and 7. Furthermore existing employees currently using the north parking lot located east of Collins Avenue at the 4600 block, will now be using the proposed parking garage. These trips were redistributed on the roadway network to access the proposed parking garage.

The project trip assignments and background growth were combined to obtain future with project traffic volumes at the analyzed intersection. Future with project volumes for the AM and PM peak hour are shown in Exhibit 8.



Page 7



In
 Out
 Project Location
 Exhibit 6
 Project Trip Distribution (Guest)





Inbound %
 Outbound %
 Project Location
 Exhibit 7
 Project Trip Distribution (Employees)





OO AM (OO) PM **Exhibit 8** Future With Project AM & PM Peak Hour Traffic Volumes



DAVID PLUMMER & ASSOCIATES | Project No. 19185

## **Future with Project Conditions Intersection Capacity Analysis**

The intersection of Indian Creek Drive / 44<sup>th</sup> Street was analyzed for future with project conditions. Exhibit 9 shows the resulting LOS for the AM and PM peak hours. The minor change in approach delays and overall delay is considered not significant. This intersection continues to and is projected to operate at LOS B and C during the AM and PM peak hours respectively. Capacity worksheets are included in Attachment C.

Weekday AM and PM Peak Hour Conditions									
Future with Project Conditions Intersection Capacity Analysis									
Intersection	Signalized/ Un-signalized	Direction	AM Peak		PM Peak				
			LOS	Delay	LOS	Delay			
		NB	А	5.5	В	14.8			
Indian Creek Drive / 44th Street	S	SB	А	3.2	А	5.0			
		WB	Е	57.2	D	53.3			
		Overall	В	11.9	С	23.5			

# Exhibit 9

## **Circulation Plan**

The proposed project is located at 4441 Collins Avenue in Miami Beach, Florida. The project is proposing to develop an existing Fontainebleau Hotel surface parking lot (at the southeast corner of the Collins Avenue / W 44th Street intersection) into a hotel ballroom and parking garage with approximately 278 parking spaces. The existing surface parking lot is currently used for employees and provides 148 parking spaces. The proposed parking garage will also be restricted to employees. Additionally the proposed project will include a pedestrian bridge that connects the ballroom / garage building to the main campus, providing the access for all guests. This keeps pedestrian traffic overhead reducing pedestrian conflicts with vehicles at grade crossings. There is no guest drop-off/pick-up at the proposed building. Guests will use the existing arrival and departure valet areas at the main campus, keeping valet operations internal. A mobility and circulation plan was prepared for the project. The plan discussed driveways, delivery areas, crosswalks, sidewalks, bike facilities, on-street parking, and the location of available transit in the vicinity of the project.





There are six (6) on-street parking spaces adjacent to the property along Collins Avenue currently designated as a taxi loading zone. Along Indian Creek Drive there are two (2) on-street parking spaces. The project will be removing the on-street parking adjacent to the property along both Collins Avenue and Indian Creek Drive (see Exhibit 10).

Loading and trash pick-up will be available on the southwest side of the parking garage. Loading / trash vehicles will enter the garage via a one-way driveway located on Indian Creek Drive and exit the garage via a driveway on Collins Avenue. An AutoTurn analysis was completed to evaluate the maneuverability of loading vehicles through the garage driveway. The design vehicle used was WB-50. The AutoTurn analysis is included in Attachment E.

The project is located in an urban area that is conducive for pedestrian and bicycle activities. The development is located approximately 0.3 miles from Indian Beach Park and directly adjacent to the Miami Beach Boardwalk. Indian Beach Park is a public park that provides public parking, Citi Bike Station 221, public beach access, and marks the start of the Miami Beach Boardwalk. All of the surrounding streets provide sidewalks on both sides of the road. All intersections adjacent to the site, have clearly marked crosswalks and most signalized intersections provide pedestrian signals. The project is providing bicycle racks on the first floor. Indian Creek Drive is a shared roadway with an exclusive bike lane south of 41<sup>st</sup> Street. There are three Citi Bike stations north and south of the project. The northern Citi Bike station is located within Indian Beach Park. The closest station is located across from the project on the west side of the Collins Avenue / 44<sup>th</sup> Street intersection. The most southern station is located on the southwest corner of the Collins Avenue / 40<sup>th</sup> Street intersection. A mobility plan was prepared for the site (see Exhibit 11). The plan shows the project location, bike lanes, shared bike lanes, sidewalk connections, and pedestrian crosswalks.





# Project Location Exhibit 10 Circulation Plan - Pedestrians

Citi Bike Station

Crosswalk
 Sidewalk
 Shared Road
 Bike Lane
 Miami Beach Boardwalk



DAVID PLUMMER & ASSOCIATES | Project No. 19185



The area surrounding the project is served by transit. Two trolleys, the Middle Beach Loop and the Collins Express, are provided by the City of Miami Beach with stops close to the project site. There are also six MDT bus routes that traverse this area of Miami Beach (Routes: 103, 112, 110, 113, 119, and 150). Descriptions for each of the Miami-Dade Transit Routes providing service to the project area are provided below:

## Route C (103)

Route C (103) operates on Collins Avenue / SR A1A and Indian Creek Drive within the vicinity of the project. This route serves the Adrienne Arsht Center Metromover Station / Bus Terminal, Jungle Island, Lincoln Road Mall area, and Mt. Sinai Hospital. This route operates with 20-minute headways throughout the day and provides connecting service to 23 additional Miami-Dade Transit bus routes, as well as the Metrorail via the Metromover.

## Route J (110)

Route J (110) operates on Collins Avenue / SR A1A, Indian Creek Drive, and the Julia Tuttle Causeway (41<sup>st</sup> Street) within the vicinity of the project. This route serves the Allapattah Metrorail Station, Miami International Airport (MIA), MIA Metrorail Station, Tri-Rail Metrorail Station, and the MIA Metromover Station.

## <u>Route L (112)</u>

Route L (112) operates on Collins Avenue / SR A1A and Indian Creek Drive within the vicinity of the project. This route serves the Miami Beach Convention Center, Normandy Drive, Northside Metrorail Station, Tri-Rail Metrorail Station, Hialeah Metrorail Station, and Amtrak Passenger Terminal. This route operates with 15-minute headways and provides connecting service to 24 additional Miami-Dade Transit bus routes, as well as the Metrorail and Tri-Rail.

### Route M (113)

Route M (113) operates on Collins Avenue / SR A1A, Indian Creek Drive, and the Julia Tuttle Causeway (41<sup>st</sup> Street) within the vicinity of the project. This route serves the Adrienne Arsht Center Metromover Station / Bus Terminal, Civic Center Metrorail Station, and Mt. Sinai Hospital. This route operates with 40-minute headways and provides connecting service to 20 additional Miami-Dade Transit bus routes, as well as the Metrorail via the Metromover.



#### Route S (119)

Route S (119) operates on Collins Avenue / SR A1A and Indian Creek Drive / SR A1A within the vicinity of the project. This route serves the Adrienne Arsht Center Metromover Station / Bus Terminal, Downtown Bus Terminal, Alton Road, and Aventura Mall. This route operates with 12-minute headways.

### Route 150

Route 150 (Airport Express) operates on Collins Avenue / SR A1A, Indian Creek Drive, and the Julia Tuttle Causeway (41<sup>st</sup> Street) within the vicinity of the project. This route operates with 20-minute headways through the day and provides connection to Lincoln Road, Earlington Heights Metrorail Station, and Miami International Airport.

The closest bus and trolley stop to the project site is located on Collins Avenue at the Collins Avenue / 4441 Exit driveway intersection directly in front of The Fontainebleau Hotel. Exhibit 11 shows the available bus routes and bus stops in the area. Transit information is available in Attachment F.



#### **Queuing Analysis**

There is no guest drop-off/pick-up areas at the proposed site. All guest access to the proposed ballroom will be through the pedestrian bridge from the existing main campus. Ballroom event guests will be using the existing valet arrival and departure area at the Fontainebleau Hotel. Valet trips will remain internal to the main property. The proposed garage will be for employees only and will provide a total of 278 parking spaces. The ground level will provide 17 self-park temporary short term spaces. Parking level one (B1) will be self-park and valet assisted parking and will provide 83 parking spaces consisting of 13 standard spaces and 70 tandem spaces. Parking level two (B2) will be valet assisted parking and will provide 178 parking spaces consisting of 12 single vertical stackers and 76 tandem spaces with vertical stackers. Both parking level one (B1) and parking level two (B2) will have valet attendants to assist employees with parking vehicles in tandem / mechanical stackers. Access to the employee parking garage levels will be provided via a two-way ramp with mechanical arm gates. It's should be noted that access to this garage is limited to pre-authorized employees only with gate access.

Queuing analyses based on the methodology outlined in the *Institute of Transportation Engineers (ITE) Transportation and Land Development* were performed for the follow:

- Employee self-park with valet assist parking garage level one (B1)
- Employee valet assist parking garage level two (B2)
- Employee parking entrance gate
- Guest valet (Operations at the existing Fontainebleau Hotel)

### Employee Valet Assist Queuing Analysis

The potential demand was calculated based on employee shift information provided by Fontainebleau Hotel. Based on the employee shift breakdown, the peak valet demand will be 85 vehicles for arrival and departure of the 8:00 am - 4:30 pm shift. The peak demand was used for the purpose of calculating the number of valet attendants required to service each level and to ensure the expected queues at the entrance to the employee parking level does not spill into the public right-of-way or interfere with internal circulation of the parking garage.



The number of vehicles trips distributed to each parking level was done proportionate to the number of parking spaces per level. Therefore, 32% trips were assigned to level one (B1) and 68% to level two (B2). Since parking level one (B1) will mostly be self- park, not all of the demand will be processed by the valet attendants. During the arrival of a shift, employees will self-park their vehicles in tandem spaces. Employees that park on the second tandem space will leave their keys with the valet attendant. During the departure of a shift, valet attendants will assist by maneuvering vehicles parked on the second tandem space as needed. Based on the proposed operations on this level, it was assumed that 25% of the demand on level one will be processed by the valet attendants. On level two (B2) the upper stacked spaces will be partially used for long term guest vehicles and partially for employee vehicles on demand. Based on the parking spaces distribution (45 upper spaces / 133 valet spaces), it was assumed that 75% of the demand on level two (B2) will be processed by the valet attendants. When employees arrive or depart work at set times, their vehicle trips do not spread evenly throughout an hour. Employee's vehicle trips tend to peak in the last 30 to 15 minutes of their start time and first 15 to 30 minutes of their departure time. To account for this condition, a factor of 1.4 was applied to the calculated vehicle volume. Based on these assumptions, the expected volume at each queuing area was calculated as followed:

- Entrance Gate: 85 veh/hr x 1.4 = 119 veh/hr
- Level one (B1): 85 veh/hr x 1.4 x 32% (assigned to B1) x 25% (valet volume) = 10 veh/hr
- Level two (B2): 85 veh/hr x  $1.4 \times 68\%$  (assigned to B2) x 75% (valet volume) = 61 veh/hr

The queuing analyses for the valet areas were performed based on the methodology outlined in the *Institute of Transportation Engineers (ITE) Transportation and Land Development*. A queuing analysis was performed at each parking level to determine the number of valet parking attendants required for each station during the peak period so that the expected queue fits within the provided storage area (95% confidence level analysis).

The queuing analysis used the single-channel waiting line model with Poisson arrivals and exponential service times. The analysis is based on the coefficient of utilization ( $\rho$ ) which is the ratio of the average arrival rate of vehicles to the average service rate.

 $\rho = \frac{Average \; Demand \; Rate}{Average \; Sevice \; Rate}$ 

Re: The Fontainebleau Hotel Ballroom and Parking Garage Traffic Statement - # 19185



The average service rate corresponds to the time it will take a valet parking attendant to park or retrieve a vehicle. If the coefficient of utilization is greater than 1, then the calculation will yield an infinite queue length.

The required queue storage (M) is determined using the following equation:

$$M = \left[\frac{\ln P(x > M) - \ln Q_M}{\ln \rho}\right] - 1$$

In this equation, P(x > M) is set at 5% to yield a 95% confidence that the queue will not back-up onto the adjacent street.

The processing rates were calculated by adding the time it will take a valet attendant to process the vehicles (**processing time**), the time it will take the valet attendant to circulate to the parking space (**driving time**), the time it will take him to park or retrieve a vehicle (**mechanical lift processing time** and **tandem space processing time**), and the time it will take the valet attendant to walk to/from the parking area (**walking time**). A processing time of 51 seconds per vehicle was used in the analysis. This information is based on data collected from a hotel on Miami Beach (see Attachment G). The driving time for the valet attendant was calculated on a conservative speed of 15 mph, and the walking time for the valet attendant was calculated on a jogging speed of 8 ft / sec. The valet processing rate for parking level one (B1) can be seen in Exhibit 12.


### Exhibit 12 Parking Level One (B1) Valet Processing Rate

### Valet Time (Inbound/Outbound)

Processing time:	51 sec / 60 sec / 1 min = <b>0.85 min</b>
Driving time:	250 ft * 1 mile / 5280 ft * 1hr / 15 miles * 60 min / hr = <b>0.19 min</b>
Tandem Park Processing Time:	0.15 min / movement * 2 movements = <b>0.30 min</b>
Walking time:	250 ft / 8 ft / sec / 60 sec / min = $0.52$ min
Total	= <u>1.86 min</u>

An iterative approach was used to determine the minimum number of valet attendants required during the peak hour to serve both the entering and/or exiting vehicles that will ensure that the average queue at parking level one (B1) will not interfere with internal circulation. Exhibit 13 shows the calculations for the valet during both the am peak hour (inbound) and pm peak hour (outbound).

### Exhibit 13 Parking Level One (B1) Valet Queuing Calculations

 $Q = \text{Processing Rate} = \frac{60 \text{ min/hr}}{1.86 \text{ min/process}} = 32.25 \text{ process/hr}$   $q = \text{Demand Rate} = 85 \frac{\text{veh}}{\text{hr}} \text{ x } 1.4 \text{ x } 32\% \text{ x } 25\% = 10 \frac{\text{veh}}{\text{hr}}$  N = Service Positions = 1 Attendant  $\rho = \text{Utilization factor} = \frac{q}{(NQ)} = \frac{10 \text{ veh/hr}}{1 \times 32 \text{ process/hr}} = 0.3100$   $Q_{\text{m}} = \text{Table Value} = 0.3100$  M = queue length which is exceeded 5% of the time [P(x>M)]  $M = \frac{\ln P(x>M) - \ln(Q_m)}{\ln(\rho)} - 1 = \frac{\ln(0.05) - \ln(0.3100)}{\ln(0.3100)} - 1 = 0.59, \text{ say 1 Vehicle on queue}$ 

The results of the analysis show that 1 valet attendant would be able to handle the demand during peak shift at parking level one with an average queue of approximately one vehicle or less.



### Parking Level Two (B2) Valet:

As with parking level one, a processing time of 51 seconds per vehicle was used in the analysis. The driving time for the valet attendant was calculated based on a speed of 15 mph, and the walking time for the valet attendant was calculated on a jogging speed of 8 ft / sec. In addition, parking level two (B2) will have vertical stackers. The *mechanical lift time* has a process time of 30 seconds per platform lift. The valet processing rate for parking level two (B2) can be seen in Exhibit 14.

### Exhibit 14 Parking Level Two (B2) Valet Processing Rate

### Valet Time (Inbound/Outbound)

Processing time:	51 sec / 60 sec / 1 min = <b>0.85</b> min
Driving time:	250 ft * 1 mile / 5280 ft * 1hr / 15 miles * 60 min / hr = <b>0.19 min</b>
Mechanical Lift Processing Time:	30 sec / lift * 2 lift * 1 min / 60 sec = <b>1.50 min</b>
Tandem Park Processing Time:	0.15 min / movement * 2 movements = $0.30$ min
Walking time:	250 ft / 8 ft / sec / 60 sec / min = $0.52$ min
Total	= <u>2.86 min</u>

An iterative approach was used to determine the minimum number of valet attendants required during the peak hour to serve both the entering and/or exiting vehicles that will ensure that the average queue at parking level two (B2) will not interfere with internal circulation. Exhibit 15 shows the calculations for the valet during both the am peak hour (inbound) and pm peak hour (outbound).



### Exhibit 15

### Parking Level Two (B2) Valet Queuing Calculations

 $Q = \text{Processing Rate} = \frac{60 \text{ min/hr}}{2.86 \text{ min/process}} = 20.97 \text{ process/hr}$   $q = \text{Demand Rate} = 85 \frac{\text{veh}}{\text{hr}} \times 1.4 \times 68\% \times 75\% = 61 \frac{\text{veh}}{\text{hr}}$  N = Service Positions = 4 Attendants  $\rho = \text{Utilization factor} = \frac{q}{(NQ)} = \frac{61 \text{ veh/hr}}{4 \times 21 \text{ process/hr}} = 0.7269$   $Q_{\text{m}} = \text{Table Value} = 0.4739$  M = queue length which is exceeded 5% of the time [P(x>M)]  $M = \frac{\ln P(x>M) - \ln(Q_m)}{\ln(\rho)} - 1 = \frac{\ln(0.05) - \ln(0.4739)}{\ln(0.7269)} - 1 = 6.05, \text{ say 7 vehicles on queue}$ 

The results of the analysis show that a total of 4 valet attendants would be able to handle the demand during peak shift at parking level two with an average queue of approximately seven vehicles or less.

### **Employee Parking Entrance Gate Queuing Analysis**

The project is proposing a ramp that will provided employees direct access to the employee parking level of the parking garage. Access to the employee parking will be restricted via a mechanical arm gate. A queuing analysis was performed to determine the anticipated queue at the mechanical arm gate for the employee parking during the peak inbound demand. Based on the employee shift breakdown, the peak inbound valet demand will be 85 vehicles (shift beginning at 8:00 am).

The queuing analysis used the single-channel waiting line model with Poisson arrivals and exponential service times. The analysis is based on the coefficient of utilization ( $\rho$ ) which is the ratio of the average arrival rate of vehicles to the average service rate.

### $\rho = \frac{Average \ Demand \ Rate}{Average \ Sevice \ Rate}$

The average service rate corresponds to the time it will take an employee to conservatively pass through the mechanical arm gate. If the coefficient of utilization is greater than 1, then the calculation will yield an infinite queue length.

Page 22

The required queue storage (M) is determined using the following equation:

$$M = \left[\frac{\ln P(x > M) - \ln Q_M}{\ln \rho}\right] - 1$$

In this equation, P(x > M) is set at 5% to yield a 95% confidence that the queue will not back-up onto the adjacent street.

The time for an employee to conservatively pass through the mechanical arm gate with a card reader is 4.25 seconds per vehicle (0.07 minutes per vehicle). This data was collected at a similar parking garage with a mechanical arm gate and card reader (see Attachment G). Exhibit 16 shows the calculations for the gate entrance.

### Exhibit 16 Employee Parking Entrance Queue Calculations

 $Q = \text{Processing Rate} = \frac{60 \text{ min/hr}}{0.07 \text{ min/process}} = 847.06 \text{ process/hr}$   $q = \text{Demand Rate} = 85 \frac{\text{veh}}{\text{hr}} \times 1.4 = 119 \frac{\text{veh}}{\text{hr}}$  N = Service Positions = 1 lane  $\rho = \text{Utilization factor} = \frac{q}{(NQ)} = \frac{119 \text{ veh/hr}}{1 \times 847.06 \text{ process/hr}} = 0.1405$   $Q_{\text{m}} = \text{Table Value} = 0.1405$  M = queue length which is exceeded 5% of the time [P(x>M)]  $M = \frac{\ln P(x>M) - \ln(Q_m)}{\ln(\rho)} - 1 = \frac{\ln(0.05) - \ln(0.1405)}{\ln(0.1405)} - 1 = -0.47 \text{ say no vehicles on queue}$ 

The result of the analysis shows that during peak arrival hour (inbound) there will be no vehicle queue expected at the employee gate entrance.

The results of the queuing analysis shows that one valet attendant at parking level one (B1) and four valet attendants at parking level two (B2) is sufficient to handle the expected demand. The



results of the queuing analysis also shows no vehicles queue at employee parking mechanical gate entrances. It should be noted that the queuing analysis considers the worst case scenario during the peak hours to make sure that the queue never spills onto the public right-of-way or interferes with site operations. Once operational, the development can assess the actual need for valet attendants at different times of day and make adjustments as needed.

### Guest Valet Queuing (Operations at the Existing Fontainebleau Hotel)

The existing valet service at the Fontainebleau Hotel provides two separate valet areas, one for arrivals and one for departures. Since ballroom event guests will be using the existing valet arrival and departure areas at the Fontainebleau Hotel a comparison of existing and with project conditions was completed. It should be noted that as with existing operations, valet trips will remain internal to the main property. Data showing peak hourly valet demand (average of the three peak months) at arrivals and departures was provided by the Fontainebleau Development. Peak hour vehicle trips (see Exhibit 3 and 4) associated with the proposed ballrooms were added to the AM and PM peak hour of the valet demand.

The queuing analysis for the existing valet areas were performed based on the methodology outlined in the *Institute of Transportation Engineers (ITE) Transportation and Land Development*. In order to calculate the valet processing time, several assumptions were taken. A processing time of 51 seconds per vehicle was used in the analysis. This information is based on data collected from a hotel on Miami Beach (see Attachment G). The driving time for the valet attendant was calculated on a conservative speed of 15 mph, and the walking time for the valet attendant was calculated on a jogging speed of 8 ft / sec. An average distance of 1,000 feet from the arrival area to the existing parking garage and an average distance of 750 feet from the existing parking garage to the departure area was assumed. The valet processing rate and queuing calculations for the arrival and departure area were included in Attachment G. Exhibit 17 provided a comparison of existing and with project condition based on the assumption made for purpose of this analysis. The comparison shows that the additional demand associated with the proposed ballroom space represent approximately one new vehicle or less to the queues at the arrival and departure areas. Therefore, the impact of the addition of the ballroom space to the existing valet operations at the Fontainebleau Hotel can be considered *de minimis*.



### Exhibit 17

		Arrival			Departure	
AM Peak Hour	Valet	Number of Valet	Expected	Valet	Number of Valet	Expected
	Demand	Attendants	Queue (veh)	Demand	Attendants	Queue (veh)
Existing	8	2	-0.51	18	2	1.13
With Project	13	2	0.65	19	2	1.4
Difference	5	0	1.16	1	0	0.27
		Arrival			Departure	
PM Peak Hour	Valet Demand	Arrival Number of Valet Attendants	Expected Queue (veh)	Valet Demand	Departure Number of Valet Attendants	Expected Queue (veh)
<b>PM Peak Hour</b> Existing	Valet Demand 33	Arrival Number of Valet Attendants 4	Expected Queue (veh) 0.91	Valet Demand	Departure Number of Valet Attendants 4	Expected Queue (veh) 0.04
PM Peak Hour Existing With Project	Valet Demand 33 35	Arrival Number of Valet Attendants 4 4	Expected Queue (veh) 0.91 1.37	Valet Demand 35 39	Departure Number of Valet Attendants 4 4 4	Expected Queue (veh) 0.04 0.61

### Guest Valet at the Fontainebleau Hotel Queuing Comparison

### **Conclusions**

A trip generation analysis was completed for the proposed project. The results of the trip generation analysis indicate that the proposed development represents 15 vehicle trips during both the AM and PM peak hours. An intersection capacity analysis was completed for the Indian Creek Drive / 44<sup>th</sup> Street intersection. The results of the analysis for existing and future with project conditions shows that this intersection operates at LOS B and C during the AM and PM peak hours respectively. Therefore, the impact of the addition of the ballroom space and parking garage on the adjacent roadway network can be considered *de minimis*.

A mobility and circulation plan was also completed. The plan shows that the project area is currently served by six Miami-Dade Transit bus routes and two Miami Beach Trolley routes. The project is located in an urban area that is conducive for pedestrian and bicycle activities providing shared bike lanes, bike rental stations, ample sidewalks, and crosswalks. These conditions encourage the use other modes of transportation and reduce the vehicular impact on the roadway network.

Queuing analyses for the proposed valet assist parking garage levels and the employee entrance gate were performed. The results of the queuing analysis shows that one valet attendant at parking level one (B1) and four valet attendants at parking level two (B2) is sufficient to handle the





expected demand. The results of the queuing analysis also show no vehicles queue at employee parking mechanical gate entrances. As previously noted the queuing analysis considers the worst case scenario during the peak hours to make sure that the queue never spills onto the public right-of-way or interferes with site operations. Once operational, the development can assess the actual need for valet attendants at different times of day and adjustments as needed.

The queuing analysis for the guest valet at the existing valet areas and a comparison of existing and with project condition were performed. The comparison shows that the additional demand associated with the proposed ballroom space represent approximately one new vehicle or less to the queues at the arrival and departure areas. Therefore, the impact of the addition of the ballroom space to the existing valet operations at the Fontainebleau Hotel can be considered *de minimis*.

We stand ready to provide any support needed for this project. Should you have any questions or comments, please call me at (305) 447-0900.

Sincerely,

Juan Espinosa, PE Vice President – Transportation cc: File Attachments

W:\19\19185\Traffic Statement FEB 2020\The Fontainebleau Hotel Traffic Statement\_Feb 2020.docx



# ATTACHMENT A Site Plan

# UN NICHOLS BROSCH WURST WOLFE & ASSOCIATES, INC.





COLLINS AVE. (1)(1.1)(1.2)(2) (5.1) **5** (5.2) (6) (7) 3 (8) 4 LANDSCAPE AREA PROPERTY LINE -2' - 0". \_ \_ \_ \_ \_ \_ \_ \_ \_\_\_ \_ E AREA LANDSCAPE AREA LANDSCAPE AREA •<u>-2' - 0"</u> Π Ŋ UP-DN ASSEMBLY -SPACE-ADA RAMP AREA +8'-0" N.G.V.D. DN LOBBY +8'-0" N.G.V.D.  $\Diamond$ YIHH UP P.E. 1 - P.E. 2 - $\langle ----$ RAMP DOWN AT 15.0% SLOPE • • • • 10.0% 10.0% \_\_\_\_ DOMESTIC FIRE PUMP PUMP UP STAIR 1 PEDESTAL SETBACK  $\sum$ Gr CHILLER \_ \_ \_ ROOM MAIN ELECT.  $\overline{\mathbf{v}}$ 18'-7" ð 27'-0"  $\langle \square$ **17 PARKING SPACES** PARKING TOTAL ELECT. VAULT. • 0' - 0" (7 HC SPACES)  $\square$ + 4' - 0" A.F.F.  $\rightarrow$ LOADING DOCK STAIR 3 STAIR 4 ASSEMBLY SPACE ELEV. ADA RAMP UP-----• 0' - 0" •-2' - 0" • DN +8'-0" N.G.V.D. LANDSCAPE AREA DN LANDSCAPE AREA LANDSCAPE AREA ENTRANCE RAMP ADA RAMP •<u>-2' - 0"</u> 20 SIDEWALK LANDSCAPE AREA <del>3 113/40\* 15' - 9 1/4" 19' - 8 3/4"</del> 27' - 7 5/16" 32' - 2 9/16" 15' - 4 1/4" 14' - 10 7/8" 10' - 0" 18' - 4 3/4" 15' - 1" 7 8 5.2 6 (5.1) 5

INDIAN CREEK DR











# ATTACHMENT B

Traffic Counts Signal Timings FDOT Adjustment Factors Historical Growth LRTP / TIP

### **Traffic Counts**

### Location: Indian Creek Dr/A1A/Collins Av Intersection Turning Movement Count

City: Miami Beach Control:

NL

0

0

0.000

0.00%

TOTAL VOLUMES

APPROACH %'s

**PEAK HR FACTOR :** 

**PEAK HR VOL :** 

PEAK HR :

NT

2059

1116

0.955

99.95%

05:00 PM - 06:00 PM

0.955

NR

0

0

0.000

0.00%

NU

1

0

0.000

0.05%

SL

0

0

0.000

0.00%

ST

2391

1153

0.873

0.874

99.96%

SR

0

0

0.000

0.00%

SU

1

1

0.250

0.04%

EL

0

0

0.000

ΕT

0

0

0.000

ER

0

0

0.000

EU

0

0

0.000

WL

420

202

0.828

21.99%

WT

0

0

0.000

0.00%

WR

1490

781

0.892

0.881

78.01%

Project ID: 20-03028-001 Date: 1/22/2020

TOTAL

6362

TOTAL

3253

0.909

WU

0

0

0.000

0.00%

_								To	tal								
NS/EW Streets:	India	an Creek Dr/	A1A/Collins	Ave	India	n Creek Dr//	A1A/Collins	Ave		44th St/C	ollins Ave			44th St/Co	ollins Ave		
		NORTH	IBOUND			SOUTH	BOUND			EAST	BOUND			WESTE	BOUND	-	
AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
7:00 AM	0	114	0	0	0	404	0	0	0	0	0	0	32	0	53	0	603
7:15 AM	0	172	0	0	0	332	0	0	0	0	0	0	32	0	52	0	588
7:30 AM	0	132	0	0	0	399	0	0	0	0	0	0	30	0	53	0	614
7:45 AM	0	158	0	0	0	423	0	0	0	0	0	0	31	0	79	0	691
8:00 AM	0	138	0	0	0	458	0	0	0	0	0	0	36	0	66	0	698
8:15 AM	0	154	0	0	0	495	0	0	0	0	0	0	35	0	76	0	760
8:30 AM	0	148	0	0	0	407	0	0	0	0	0	0	39	0	64	0	658
8:45 AM	0	178	0	0	0	440	0	0	0	0	0	0	39	0	74	0	731
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES :	0	1194	0	0	0	3358	0	0	0	0	0	0	274	0	517	0	5343
APPROACH %'s :	0.00%	100.00%	0.00%	0.00%	0.00%	100.00%	0.00%	0.00%					34.64%	0.00%	65.36%	0.00%	
PEAK HR :		08:00 AM -	09:00 AM		1												TOTAL
PEAK HR VOL :	0	618	0	0	0	1800	0	0	0	0	0	0	149	0	280	0	2847
PEAK HR FACTOR :	0.000	0.868	0.000	0.000	0.000	0.909	0.000	0.000	0.000	0.000	0.000	0.000	0.955	0.000	0.921	0.000	0.027
		0.8	68		1	0.90	)9							0.9	49		0.937
		NORTH	IBOUND			SOUTH	BOUND			EAST	BOUND			WESTE	30UND		
PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
4:00 PM	0	219	0	0	0	332	0	0	0	0	0	0	53	0	188	0	792
4:15 PM	0	247	0	0	0	273	0	0	0	0	0	0	48	0	167	0	735
4:30 PM	0	219	0	1	0	345	0	0	0	0	0	0	65	0	188	0	818
4:45 PM	0	258	0	0	0	288	0	0	0	0	0	0	52	0	166	0	764
5:00 PM	0	258	0	0	0	289	0	0	0	0	0	0	60	0	219	0	826
5:15 PM	0	278	0	0	0	263	0	1	0	0	0	0	40	0	158	0	740
5:30 PM	0	292	0	0	0	330	0	0	0	0	0	0	61	0	212	0	895
5:45 PM	0	288	0	0	0	271	0	0	0	0	0	0	41	0	192	0	792

# Location: Indian Creek Dr/A1A/Collins Ave & 44th St/Collins Ave

City: Miami Beach Control: 0

Project ID: 20-03028-001 Date: 1/22/2020

-								Ca	rs								
NS/EW Streets:	India	an Creek Dr//	A1A/Collins	Ave	India	n Creek Dr//	A1A/Collins	Ave		44th St/0	Collins Ave			44th St/Co	llins Ave		
		NORTH	BOUND			SOUTH	BOUND			EAST	BOUND			WESTE	OUND		
AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
,	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
7:00 AM	0	111	0	0	0	392	0	0	0	0	0	0	28	0	47	0	578
7:15 AM	0	169	0	0	0	326	0	0	0	0	0	0	29	0	48	0	572
7:30 AM	0	125	0	0	0	388	0	0	0	0	0	0	26	0	49	0	588
7:45 AM	0	155	0	0	0	417	0	0	0	0	0	0	29	0	69	0	670
8:00 AM	0	134	0	0	0	444	0	0	0	0	0	0	29	0	58	0	665
8:15 AM	0	149	0	0	0	489	0	0	0	0	0	0	33	0	68	0	739
8:30 AM	0	146	0	0	0	398	0	0	0	0	0	0	35	0	59	0	638
8:45 AM	0	169	0	0	0	426	0	0	0	0	0	0	33	0	70	0	698
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES :	0	1158	0	0	0	3280	0	0	0	0	0	0	242	0	468	0	5148
APPROACH %'s :	0.00%	100.00%	0.00%	0.00%	0.00%	100.00%	0.00%	0.00%					34.08%	0.00%	65.92%	0.00%	
PEAK HR :		08:00 AM -	09:00 AM														TOTAL
PEAK HR VOL :	0	598	0	0	0	1757	0	0	0	0	0	0	130	0	255	0	2740
PEAK HR FACTOR :	0.00	0.885	0.000	0.000	0.000	0.898	0.000	0.000	0.000	0.000	0.000	0.000	0.929	0.000	0.911	0.000	0.027
		0.88	35			0.89	98							0.93	34		0.927

		NORTH	BOUND			SOUTH	BOUND			EAST	BOUND			WESTE	OUND		
PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
4:00 PM	0	214	0	0	0	325	0	0	0	0	0	0	49	0	178	0	766
4:15 PM	0	244	0	0	0	262	0	0	0	0	0	0	42	0	161	0	709
4:30 PM	0	218	0	0	0	340	0	0	0	0	0	0	61	0	179	0	798
4:45 PM	0	257	0	0	0	281	0	0	0	0	0	0	47	0	161	0	746
5:00 PM	0	257	0	0	0	279	0	0	0	0	0	0	58	0	212	0	806
5:15 PM	0	277	0	0	0	253	0	1	0	0	0	0	36	0	155	0	722
5:30 PM	0	292	0	0	0	323	0	0	0	0	0	0	56	0	202	0	873
5:45 PM	0	285	0	0	0	265	0	0	0	0	0	0	39	0	186	0	775
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES :	0	2044	0	0	0	2328	0	1	0	0	0	0	388	0	1434	0	6195
APPROACH %'s :	0.00%	100.00%	0.00%	0.00%	0.00%	99.96%	0.00%	0.04%					21.30%	0.00%	78.70%	0.00%	
PEAK HR :		05:00 PM -	06:00 PM														TOTAL
PEAK HR VOL :	0	1111	0	0	0	1120	0	1	0	0	0	0	189	0	755	0	3176
PEAK HR FACTOR :	0.00	0.951	0.000	0.000	0.000	0.867	0.000	0.250	0.000	0.000	0.000	0.000	0.815	0.000	0.890	0.000	0.010
		0.9	51			0.8	68							0.87	74		0.910

# Intersection Turning Movement Count Location: Indian Creek Dr/A1A/Collins Ave & 44th St/Collins Ave

City: Miami Beach Control: 0

Project ID: 20-03028-001 Date: 1/22/2020

NS/EW Streets         Indian Creek Dr/A1A/Collins Ave         Indian Creek Dr/A1A/Collins Ave         Indian Creek Dr/A1A/Collins Ave         Indian Creek Dr/A1A/Collins Ave         Vert Httts:         Vert Htttts:	-									-								
AM         0	NS/EW Streets:	India	n Creek Dr/A	A1A/Collins	Ave	India	n Creek Dr//	A1A/Collins	Ave		44th St/C	ollins Ave			44th St/Co	llins Ave		
AM         0 <			NORTH	BOUND			SOUTH	BOUND			EAST	BOUND			WESTB	OUND		
NL         NT         NR         NU         SL         ST         SR         SU         EL         ET         ER         EU         WL         WT         WR         WU         TOTAL           7:00 AM         0         3         0         0         0         12         0         0         0         0         0         4         0         6         0         25           7:15 AM         0         3         0         0         0         6         0         0         0         0         3         0         4         0         6         0         25           7:15 AM         0         3         0         0         0         6         0         0         0         0         4         0         25           7:30 AM         0         7         0         0         0         6         0         0         0         0         2         0         10         21           8:00 AM         0         4         0         0         6         0         0         0         0         2         0         8         0         21           8:00 AM <td< th=""><th>ΔΜ</th><th>0</th><th>0</th><th>0</th><th>0</th><th>0</th><th>0</th><th>0</th><th>0</th><th>0</th><th>0</th><th>0</th><th>0</th><th>0</th><th>0</th><th>0</th><th>0</th><th></th></td<>	ΔΜ	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
7:00 AM       0       3       0       0       12       0       0       0       0       4       0       6       0       25         7:15 AM       0       3       0       0       0       6       0       0       0       0       0       3       0       4       0       16         7:30 AM       0       7       0       0       0       0       0       0       0       4       0       4       0       26         7:45 AM       0       3       0       0       0       0       0       0       0       4       0       4       0       26         7:45 AM       0       3       0       0       0       0       0       0       0       0       2       0       10       21         8:00 AM       0       4       0       0       0       0       0       0       0       0       2       0       8       0       33         8:00 AM       0       2       0       0       0       0       0       0       0       0       0       0       0       0       0 <t< th=""><th>/</th><th>NL</th><th>NT</th><th>NR</th><th>NU</th><th>SL</th><th>ST</th><th>SR</th><th>SU</th><th>EL</th><th>ET</th><th>ER</th><th>EU</th><th>WL</th><th>WT</th><th>WR</th><th>WU</th><th>TOTAL</th></t<>	/	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
7:15 AM       0       3       0       0       0       6       0       0       0       0       3       0       4       0       16         7:30 AM       0       7       0       0       0       11       0       0       0       0       0       4       0       4       0       26         7:45 AM       0       3       0       0       6       0       0       0       0       0       2       0       10       0       21         8:00 AM       0       4       0       0       6       0       0       0       0       0       7       0       8       0       33         8:15 AM       0       5       0       0       0       4       0       0       0       0       0       2       0       8       0       33         8:15 AM       0       2       0       0       0       9       0       0       0       0       0       0       0       0       0       2       0       8       0       20         8:30 AM       0       2       0       0       14       <	7:00 AM	0	3	0	0	0	12	0	0	0	0	0	0	4	0	6	0	25
7:30 AM       0       7       0       0       11       0       0       0       0       0       4       0       4       0       26         7:45 AM       0       3       0       0       6       0       0       0       0       0       2       0       10       0       21         8:00 AM       0       4       0       0       0       0       0       0       7       0       8       0       33         8:10 AM       0       4       0       0       0       0       0       0       7       0       8       0       33         8:15 AM       0       5       0       0       0       6       0       0       0       0       2       0       8       0       20         8:30 AM       0       2       0       0       0       0       0       0       0       0       0       2       0       8       0       20       20       33         8:30 AM       0       9       0       0       0       0       0       0       0       0       0       0       0	7:15 AM	0	3	0	0	0	6	0	0	0	0	0	0	3	0	4	0	16
7:45 AM       0       3       0       0       6       0       0       0       0       0       0       0       2       0       10       0       21         8:00 AM       0       4       0       0       14       0       0       0       0       0       0       0       7       0       8       0       33         8:15 AM       0       5       0       0       0       6       0       0       0       0       0       2       0       8       0       21         8:30 AM       0       2       0       0       0       9       0       0       0       0       0       0       2       0       8       0       21         8:30 AM       0       2       0 <td< th=""><th>7:30 AM</th><th>0</th><th>7</th><th>0</th><th>0</th><th>0</th><th>11</th><th>0</th><th>0</th><th>0</th><th>0</th><th>0</th><th>0</th><th>4</th><th>0</th><th>4</th><th>0</th><th>26</th></td<>	7:30 AM	0	7	0	0	0	11	0	0	0	0	0	0	4	0	4	0	26
8:00 AM       0       4       0       0       14       0       0       0       0       0       7       0       8       0       33         8:15 AM       0       5       0       0       0       6       0       0       0       0       0       2       0       8       0       21         8:30 AM       0       2       0       0       0       9       0       0       0       0       0       4       0       5       0       20         8:45 AM       0       9       0       0       14       0       0       0       0       0       0       0       4       0       5       0       20         8:45 AM       0       9       0       0       14       0 <t< th=""><th>7:45 AM</th><th>0</th><th>3</th><th>0</th><th>0</th><th>0</th><th>6</th><th>0</th><th>0</th><th>0</th><th>0</th><th>0</th><th>0</th><th>2</th><th>0</th><th>10</th><th>0</th><th>21</th></t<>	7:45 AM	0	3	0	0	0	6	0	0	0	0	0	0	2	0	10	0	21
8:15 AM       0       5       0       0       6       0       0       0       0       0       2       0       8       0       21         8:30 AM       0       2       0       0       0       9       0       0       0       0       0       0       4       0       5       0       20       20         8:30 AM       0       9       0       0       9       0       0       0       0       0       0       4       0       5       0       20       33         0       9       0       0       14       0       0       0       0       0       0       4       0       33         TOTAL VOLUMES :       0       36       0       0       0       0       0       0       0       0       0       10 <t< th=""><th>8:00 AM</th><th>0</th><th>4</th><th>0</th><th>0</th><th>0</th><th>14</th><th>0</th><th>0</th><th>0</th><th>0</th><th>0</th><th>0</th><th>7</th><th>0</th><th>8</th><th>0</th><th>33</th></t<>	8:00 AM	0	4	0	0	0	14	0	0	0	0	0	0	7	0	8	0	33
8:30 AM 8:45 AM       0       2       0       0       9       0       9       0       0       0       0       0       0       4       0       5       0       20         8:45 AM       0       9       0       0       14       0       0       0       0       0       0       4       0       5       0       20       33         ML       NL       NR       NU       SL       ST       SR       SU       EL       ET       ER       EU       WL       WT       WR       WU       TOTAL         APPROACH %:       0.00%       36       0       0       0.00%       10.00%       0.00%	8:15 AM	0	5	0	0	0	6	0	0	0	0	0	0	2	0	8	0	21
8:45 AM       0       9       0       0       14       0       0       0       0       0       6       0       4       0       33         TOTAL VOLUMES: APPROACH %'s:       NL       NT       NR       NU       SL       ST       SR       SU       EL       ET       ER       EU       WL       WT       WR       WU       TOTAL         0       36       0       0       78       0       0       0       0       0       32       0       49       0       <	8:30 AM	0	2	0	0	0	9	0	0	0	0	0	0	4	0	5	0	20
Image: Constraint of the system of	8:45 AM	0	9	0	0	0	14	0	0	0	0	0	0	6	0	4	0	33
NL       NT       NR       NU       SL       ST       SR       SU       EL       ET       ER       EU       WL       WT       WR       WU       TOTAL         TOTAL VOLUMES:       0       36       0       0       78       0       0       0       0       0       0       32       0       49       0       195         APPROACH %'s:       0.00%       100.00%       0.00%       100.00%       0.00																		
TOTAL VOLUMES:       0       36       0       0       78       0       0       0       0       0       32       0       49       0       195         APPROACH %'s:       0.00%       100.00%       0.00%       100.00%       0.00%       100.00%       0.00%		NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
APPROACH %'s:         0.00%         100.00%         0.00%         100.00%         0.00%	TOTAL VOLUMES :	0	36	0	0	0	78	0	0	0	0	0	0	32	0	49	0	195
PEAK HR:         08:00 AM - 09:00 AM         09:00 AM         09:00 AM         00         0	APPROACH %'s :	0.00%	100.00%	0.00%	0.00%	0.00%	100.00%	0.00%	0.00%					39.51%	0.00%	60.49%	0.00%	
PEAK HR VOL:         0         20         0         0         43         0         0         0         0         0         19         0         25         0         107           PEAK HR FACTOR:         0.000         0.556         0.000         0.000         0.768         0.000         0.000         0.000         0.000         0.000         0.679         0.000         0.781         0.000         0.811	PEAK HR :		08:00 AM -	09:00 AM														TOTAL
PEAK HR FACTOR:         0.000         0.556         0.000         0.000         0.000         0.000         0.000         0.000         0.679         0.000         0.781         0.000           0.811	PEAK HR VOL :	0	20	0	0	0	43	0	0	0	0	0	0	19	0	25	0	107
0.811	PEAK HR FACTOR :	0.000	0.556	0.000	0.000	0.000	0.768	0.000	0.000	0.000	0.000	0.000	0.000	0.679	0.000	0.781	0.000	0.011
0.556 0.768 0.733 0.733			0.55	56			0.76	58							0.73	33		0.811

		NORTH	BOUND			SOUTH	BOUND			EAST	BOUND			WESTE	BOUND		
PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
4:00 PM	0	5	0	0	0	7	0	0	0	0	0	0	4	0	10	0	26
4:15 PM	0	3	0	0	0	11	0	0	0	0	0	0	6	0	6	0	26
4:30 PM	0	1	0	0	0	5	0	0	0	0	0	0	4	0	9	0	19
4:45 PM	0	1	0	0	0	7	0	0	0	0	0	0	5	0	5	0	18
5:00 PM	0	1	0	0	0	10	0	0	0	0	0	0	2	0	7	0	20
5:15 PM	0	1	0	0	0	10	0	0	0	0	0	0	4	0	3	0	18
5:30 PM	0	0	0	0	0	7	0	0	0	0	0	0	5	0	10	0	22
5:45 PM	0	3	0	0	0	6	0	0	0	0	0	0	2	0	6	0	17
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES :	0	15	0	0	0	63	0	0	0	0	0	0	32	0	56	0	166
APPROACH %'s :	0.00%	100.00%	0.00%	0.00%	0.00%	100.00%	0.00%	0.00%					36.36%	0.00%	63.64%	0.00%	
PEAK HR :		05:00 PM -	06:00 PM														TOTAL
PEAK HR VOL :	0	5	0	0	0	33	0	0	0	0	0	0	13	0	26	0	77
PEAK HR FACTOR :	0.00	0.417	0.000	0.000	0.000	0.825	0.000	0.000	0.000	0.000	0.000	0.000	0.650	0.000	0.650	0.000	0.975
		0.4	17			0.8	25							0.65	50		0.675

ш	T.	

# Location: Indian Creek Dr/A1A/Collins Ave & 44th St/Collins Ave

City: Miami Beach Control: 0

Project ID: 20-03028-001 Date: 1/22/2020

_								Bik	es								_
NS/EW Streets:	India	n Creek Dr//	A1A/Collins	Ave	Indiar	Creek Dr/	A1A/Collins	Ave		44th St/C	ollins Ave			44th St/Co	ollins Ave		
		NORTH	BOUND			SOUTH	BOUND			EAST	BOUND			WEST	BOUND		
AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
7:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:15 AM	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1
7:30 AM	0	2	0	0	0	1	0	0	0	0	0	0	0	0	1	0	4
7:45 AM	0	0	0	0	0	1	0	0	0	0	0	0	0	0	0	0	1
8:00 AM	0	1	0	0	0	1	0	0	0	0	0	0	0	0	1	0	3
8:15 AM	0	0	0	0	0	1	0	0	0	0	0	0	0	0	0	0	1
8:30 AM	0	2	0	0	0	1	0	0	0	0	0	0	0	0	1	0	4
8:45 AM	0	0	0	0	1	1	0	0	0	0	0	0	0	0	1	0	3
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES :	0	6	0	0	1	6	0	0	0	0	0	0	0	0	4	0	17
APPROACH %'s :	0.00%	100.00%	0.00%	0.00%	14.29%	85.71%	0.00%	0.00%					0.00%	0.00%	100.00%	0.00%	
PEAK HR :		08:00 AM -	09:00 AM														TOTAL
PEAK HR VOL :	0	3	0	0	1	4	0	0	0	0	0	0	0	0	3	0	11
PEAK HR FACTOR :	0.000	0.375	0.000	0.000	0.250	1.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.750	0.000	0.688
		0.37	75			0.62	25							0.7	50		0.000

		NORTH	BOUND			SOUTH	BOUND			EAST	BOUND			WESTE	BOUND		
PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
4:00 PM	0	2	0	0	0	0	0	0	0	0	0	0	0	0	2	0	4
4:15 PM	0	2	1	0	0	2	0	0	0	0	0	0	0	0	0	0	5
4:30 PM	0	1	0	0	0	0	0	0	0	0	0	0	1	0	1	0	3
4:45 PM	0	1	0	0	0	2	0	0	0	0	0	0	0	0	1	0	4
5:00 PM	0	0	0	0	0	3	0	0	0	0	0	0	0	0	0	0	3
5:15 PM	0	4	0	0	0	2	0	0	0	0	0	0	0	0	6	0	12
5:30 PM	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	1
5:45 PM	0	0	0	0	0	1	0	0	0	0	0	0	0	0	4	0	5
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES :	0	10	2	0	0	10	0	0	0	0	0	0	1	0	14	0	37
APPROACH %'s :	0.00%	83.33%	16.67%	0.00%	0.00%	100.00%	0.00%	0.00%					6.67%	0.00%	93.33%	0.00%	1
PEAK HR :		05:00 PM -	06:00 PM		105:00 PR												TOTAL
PEAK HR VOL :	0	4	1	0	0	6	0	0	0	0	0	0	0	0	10	0	21
PEAK HR FACTOR :	0.00	0.250	0.250	0.000	0.000	0.500	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.417	0.000	0.420
		0.3	13			0.5	00							0.4	17		0.438

### National Data & Surveying Services Location: Indian Creek Dr/A1A/Collins Ave & 44th St/Collins Age Movement Count City: Miami Beach Date: 1/22/2020

			Pede	strians	(Crossw	alks)			
NS/EW Streets:	Indian Dr/A1A/Co	Creek ollins Ave	Indian Dr/A1A/C	Creek Collins Ave	44th St/C	collins Ave	44th St/C	ollins Ave	
A N A	NORTI	H LEG	SOUT	h leg	EAST	T LEG	WES	Г LEG	
AIVI	EB	WB	EB	WB	NB	SB	NB	SB	TOTAL
7:00 AM	1	0	0	0	1	0	0	0	2
7:15 AM	0	0	2	1	0	1	0	0	4
7:30 AM	1	0	5	1	7	1	0	0	15
7:45 AM	7	0	1	1	7	0	0	0	16
8:00 AM	1	0	1	0	2	0	0	0	4
8:15 AM	0	0	1	3	5	5	0	0	14
8:30 AM	1	0	4	0	6	1	0	0	12
8:45 AM	6	0	4	1	21	4	0	0	36
	EB	WB	EB	WB	NB	SB	NB	SB	TOTAL
TOTAL VOLUMES :	17	0	18	7	49	12	0	0	103
APPROACH %'s :	100.00%	0.00%	72.00%	28.00%	80.33%	19.67%			
PEAK HR :	- MA 00:80	09:00 AM							TOTAL
PEAK HR VOL :	8	0	10	4	34	10	0	0	66
<b>PEAK HR FACTOR :</b>	0.333		0.625	0.333	0.405	0.500			0 450
	0.3	33	0.7	700	0.4	140			0.458

	NORT	h leg	SOUT	h leg	EAST	Г LEG	WES		
PIVI	EB	WB	EB	WB	NB	SB	NB	SB	TOTAL
4:00 PM	0	0	6	1	10	10	0	0	27
4:15 PM	1	1	0	0	2	19	0	0	23
4:30 PM	1	0	2	2	14	9	0	0	28
4:45 PM	0	0	3	11	16	18	0	0	48
5:00 PM	0	0	0	0	12	9	0	0	21
5:15 PM	0	0	0	0	19	18	0	0	37
5:30 PM	0	1	0	0	13	24	0	0	38
5:45 PM	0	0	0	0	12	12 17		0	29
	EB	WB	EB	WB	NB	SB	NB	SB	TOTAL
TOTAL VOLUMES :	2	2	11	14	98	124	0	0	251
APPROACH %'s :	50.00%	50.00%	44.00%	56.00%	44.14%	55.86%			
PEAK HR :	05:00 PM - 06:00 PM								TOTAL
PEAK HR VOL :	0	1	0	0	56	68	0	0	125
PEAK HR FACTOR :		0.250			0.737	0.708			0 0 2 2
	0.2	250			0.838				0.822

### Indian Creek Dr/A1A/Collins Ave & 44th St/Collins Ave

Peak Hour Turning Movement Count









Site Code:	20-3028-001
Date:	01/22/2020
Weather:	Sunny
City:	Miami Beach
County:	Miami - Dade
Count Times:	07:00 - 09:00
	16:00 - 18:00
Control:	Signalized

#### SIGNAL TIMING

PHASES	1	2	3
ST	01:25	01:25	01:25
NT	00:25	00:25	00:25
WL	00:30	00:31	00:29



E/W Street: 44th St/Collins Ave



### **Signal Timings**

### TOD Schedule Report

### for 2679: Collins Av&Indian Creek Dr&44 St

Print Time:



<u>9/24/2019</u>												4:55 PM
Asset		Intersection	L	5	<u>TOD</u> Schedule	<u>Op Mode</u>	<u> Plan #</u>	<u>Cycle</u>	<u>Offset</u>	<u>TOD</u> <u>Setting</u>	<u>Active</u> <u>PhaseBank</u>	<u>Active</u> <u>Maximum</u>
2679	Collins Av	&Indian Cre	ek Dr&44 St	D	OW-3		[19] WKND-MORN	140	87	N/A	1	Max 2
			<u>S</u>	<u>plits</u>								
<u>PH 1</u>	<u>PH 2</u>	<u>PH 3</u>	<u>PH 4</u>	<u>PH 5</u>	<u>PH 6</u>	<u>PH 7</u>	<u>PH 8</u>					
-	SBT	-	-	WBR	NBT	WBL	PED					
0	83	0	0	9	68	20	19					
	<b>↓</b>			Ł	↑		N/A					

#### Active Phase Bank: Phase Bank 1

<u>Phase</u>	<u>Walk</u>	Don't Walk	<u>Min Initial</u>	<u>Veh Ext</u>	<u>Max Limit</u>	<u>Max 2</u>	<u>Yellow</u>	<u>Red</u>	Last In Service Date:	unknown
	Phase Bank								Last III Service Date.	UTKIOWI
	1 2 3	1 2 3	1 2 3	1 2 3	1 2 3	1 2 3			Permitted Phases	
1 -	0 - 0 - 0	0 - 0 - 0	0 - 0 - 0	0 - 0 - 0	0 - 0 - 0	0 - 0 - 0	0	0	T ennitied T hases	
2 SBT	5 - 5 - 5	23 - 23 - 23	5 - 5 - 5	1 - 1 - 1	50 - 50 - 50	0 - 50 - 50	) 4	2		<u>12345678</u>
3 -	0 - 0 - 0	0 - 0 - 0	0 - 0 - 0	0 - 0 - 0	0 - 0 - 0	0 - 0 - 0	0	0	Default	-25678
4 -	0 - 0 - 0	0 - 0 - 0	0 - 0 - 0	0 - 0 - 0	0 - 0 - 0	0 - 0 - 0	0	0	External Permit 0	-25678
5 WBR	0 - 0 - 0	0 - 0 - 0	7 - 7 - 7	2.5 - 2.5 - 2.5	8 - 8 - 8	20 - 20 - 20	) 4	2	External Permit 1	-25678
6 NBT	5 - 5 - 5	23 - 23 - 23	5 - 5 - 5	1 - 1 - 1	50 - 50 - 50	0 - 50 - 50	) 4	2	External Permit 2	-25678
7 WBL	0 - 0 - 0	0 - 0 - 0	7 - 7 - 7	2.5 - 2.5 - 2.5	15 - 15 - 15	25 - 25 - 25	6 4	2		
8 PED	5 - 5 - 5	13 - 13 - 13	0 - 0 - 0	0 - 0 - 0	0 - 0 - 0	0 - 0 - 0	4	2		

### TOD Schedule Report

#### for 2679: Collins Av&Indian Creek Dr&44 St

Print Date: 9/24/2019

Print Time: 4:55 PM

						Green	<u> Time</u>					
Current			1	2	3	4	5	6	7	8		
TOD Schedule	<u>Plan</u>	<u>Cycle</u>	-	SBT	-	-	WBR	NBT	WBL	PED	Ring Offset	<u>Offset</u>
	1	90	0	41	0	0	7	28	12	19	0	66
	2	100	0	47	0	0	13	28	16	19	0	15
	3	100	0	47	0	0	13	28	16	19	0	53
	4	140	0	87	0	0	11	70	16	19	0	108
	5	100	0	47	0	0	13	28	16	19	0	53
	6	100	0	47	0	0	13	28	16	19	0	53
	8	105	0	52	0	0	7	39	16	19	0	75
	9	105	0	48	0	0	14	28	20	19	0	75
	10	120	0	63	0	0	9	48	20	19	0	22
	11	140	0	83	0	0	12	65	20	19	0	45
	12	120	0	63	0	0	22	35	20	19	0	70
	13	100	0	48	0	0	13	29	15	19	0	53
	14	105	0	53	0	0	18	29	15	19	0	75
	15	120	0	68	0	0	18	44	15	19	0	70
	16	100	0	48	0	0	14	28	15	19	0	30
	17	100	0	48	0	0	14	28	15	19	0	61
	18	140	0	83	0	0	9	68	20	19	0	131
	19	140	0	83	0	0	9	68	20	19	0	87
	20	120	0	68	0	0	14	48	15	19	0	22
	21	120	0	68	0	0	14	48	15	19	0	22
	22	90	0	41	0	0	7	28	12	19	0	66
	23	90	0	41	0	0	7	28	12	19	0	66

Local TOD Schedule												
<u>Time</u>	<u>Plan</u>	DOW										
0000	1	Su	S									
0000	2	M T W Th F										
0700	18	M T W Th F										
0930	2	M T W Th F										
1000	2	Su	S									
1400	19	M T W Th F										
2000	1	Su	S									
2200	2	M T W Th F	-									

<u>Time</u>	Function	<u>Settings *</u>	<u>Day of Week</u>
0000	TOD OUTPUTS		SuM T W ThF S
0000	TOD LOCAL MULTIFU	4	SuM T W ThF S
0500	TOD LOCAL MULTIFU		SuM T W ThF S

### Local Time of Day Function

<u>Time</u>	Function	<u>Settings *</u>	Day of Week
0000	TOD OUTPUTS		SuM T W ThF S
0000	TOD LOCAL MULTIFU	NCT4	SuM T W ThF S
0500	TOD LOCAL MULTIFU	NCT	SuM T W ThF S

### \* Settings

Blank - FREE - Phase Bank 1, Max 1 Blank - Plan - Phase Bank 1, Max 2 1 - Phase Bank 2, Max 1 2 - Phase Bank 2, Max 2 3 - Phase Bank 3, Max 1 4 - Phase Bank 3, Max 2 5 - EXTERNAL PERMIT 1 6 - EXTERNAL PERMIT 2 7 - X-PED OMIT 8 - TBA



6/27/2016	3.00
3/2//2015	

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	D	irection	SB	NB	NB WB				F	Ped H	leads	[] N		
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Flashing Ope	era	tion	I FY	FY	Fere	FR					<u> </u>	#		Page 1 of 1
Miami-Dade County Public Works Department														
Drawn H. FRA	N	cillon	Date <i>41/4</i>	102	Coli	ins i	4v /:	INDIA	N CR	EE K	DR	Ę	44	+ ST
Checked	. 1		Date	100		PI	aced ii	n Servie	ce		F	hasi	ng No.	Asset Number
H. HERNANDEL		4/4/	0 L	Date	4/5	02	By M	ASTE	C		9		2679	

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### **FDOT Adjustment Factors**

WEEK	DATES	SF	MOCF: 0.98 PSCF		
====== 1 2 3 4 5 6 7 8 9 0 1 1 2 3 4 5 6 7 8 9 0 1 1 2 3 4 5 6 7 8 9 0 1 1 2 3 4 5 6 7 8 9 0 1 1 2 3 4 5 6 7 8 9 0 1 1 2 3 4 5 6 7 8 9 0 1 1 2 3 4 5 6 7 8 9 0 1 1 2 3 4 5 6 7 8 9 0 1 1 2 3 4 5 6 7 8 9 0 1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	$\begin{array}{l} 01/01/2018 & - 01/06/2018\\ 01/07/2018 & - 01/13/2018\\ 01/14/2018 & - 01/20/2018\\ 01/21/2018 & - 02/03/2018\\ 02/04/2018 & - 02/10/2018\\ 02/11/2018 & - 02/17/2018\\ 02/18/2018 & - 02/24/2018\\ 02/25/2018 & - 03/03/2018\\ 03/04/2018 & - 03/03/2018\\ 03/04/2018 & - 03/10/2018\\ 03/11/2018 & - 03/24/2018\\ 03/25/2018 & - 03/24/2018\\ 04/01/2018 & - 04/07/2018\\ 04/01/2018 & - 04/21/2018\\ 04/01/2018 & - 04/21/2018\\ 04/01/2018 & - 04/21/2018\\ 04/22/2018 & - 05/12/2018\\ 04/29/2018 & - 05/12/2018\\ 05/13/2018 & - 05/12/2018\\ 05/20/2018 & - 05/19/2018\\ 05/20/2018 & - 05/26/2018\\ 05/27/2018 & - 05/26/2018\\ 06/03/2018 & - 05/26/2018\\ 06/10/2018 & - 06/09/2018\\ 06/10/2018 & - 06/09/2018\\ 06/10/2018 & - 06/23/2018\\ 06/10/2018 & - 07/07/2018\\ 07/01/2018 & - 07/21/2018\\ 07/08/2018 & - 07/21/2018\\ 07/08/2018 & - 07/21/2018\\ 07/29/2018 & - 07/221/2018\\ 07/29/2018 & - 07/221/2018\\ 07/22/2018 & - 07/221/2018\\ 07/22/2018 & - 07/221/2018\\ 07/29/2018 & - 07/221/2018\\ 07/29/2018 & - 09/01/2018\\ 07/029/2018 & - 09/01/2018\\ 08/12/2018 & - 08/11/2018\\ 08/05/2018 & - 08/11/2018\\ 09/09/2018 & - 09/01/2018\\ 09/09/2018 & - 09/22/2018\\ 09/09/2018 & - 09/22/2018\\ 09/09/2018 & - 09/22/2018\\ 09/09/2018 & - 09/22/2018\\ 09/09/2018 & - 09/22/2018\\ 09/09/2018 & - 09/22/2018\\ 09/09/2018 & - 09/22/2018\\ 09/02/2018 & - 09/22/2018\\ 09/02/2018 & - 10/13/2018\\ 10/14/2018 & - 10/20/2018\\ 10/21/2018 & - 10/20/2018\\ 10/21/2018 & - 10/20/2018\\ 10/21/2018 & - 10/20/2018\\ 10/21/2018 & - 10/20/2018\\ 10/21/2018 & - 10/20/2018\\ 10/21/2018 & - 10/20/2018\\ 10/21/2018 & - 10/20/2018\\ 10/21/2018 & - 10/20/2018\\ 10/21/2018 & - 11/02018\\ 11/04/2018 & - 11/2008\\ 11/04/2018 & - 11/2008\\ 11/04/2018 & - 11/2008\\ 11/04/2018 & - 11/2008\\ 11/04/2018 & - 11/2008\\ 11/04/2018 & - 11/2008\\ 11/04/2018 & - 11/2008\\ 11/04/2018 & - 11/2008\\ 11/04/2018 & - 11/2008\\ 11/2008 & - 11/2008\\ 12/09/2018 & - 12/08/2018\\ 12/09/2018 & - 12/08/2018\\ 12/09/2018 & - 12/08/2018\\ 12/09/2018 & - 12/08/2018\\ 12/09/2018 & - 12/08/2018\\ 12/09/2018 & - 12/08/2018\\ 12/09/2018 & - 12/08/2018\\ 12/09/2018 & - 1$	$\begin{array}{c} 1.03\\ 1.03\\ 1.03\\ 1.04\\ 1.02\\ 1.01\\ 0.99\\ 0.98\\ 0.98\\ 0.98\\ 0.98\\ 0.97\\ 0.97\\ 0.97\\ 0.97\\ 0.97\\ 0.97\\ 0.97\\ 0.97\\ 0.97\\ 0.97\\ 0.97\\ 0.97\\ 0.97\\ 1.00\\ 1.01\\ 1.01\\ 1.01\\ 1.01\\ 1.01\\ 1.01\\ 1.01\\ 1.01\\ 1.02\\ 1.02\\ 1.02\\ 1.02\\ 1.02\\ 1.02\\ 1.02\\ 1.02\\ 1.02\\ 1.02\\ 1.02\\ 1.00\\ 1.00\\ 1.00\\ 1.00\\ 1.00\\ 1.00\\ 1.00\\ 1.00\\ 1.00\\ 1.00\\ 1.00\\ 1.00\\ 1.00\\ 1.00\\ 1.02\\ 1.02\\ 1.02\\ 1.02\\ 1.02\\ 1.02\\ 1.02\\ 1.02\\ 1.02\\ 1.03\\$	$\begin{array}{c} 1.05\\ 1.05\\ 1.06\\ 1.04\\ 1.03\\ 1.01\\ 1.00\\ 1.00\\ 1.00\\ 1.00\\ 0.99\\ 0.99\\ 0.99\\ 0.99\\ 0.99\\ 0.99\\ 0.99\\ 0.99\\ 0.99\\ 0.99\\ 1.00\\ 1.01\\ 1.02\\ 1.03\\ 1.02\\ 1.03\\ 1.03\\ 1.04\\ 1.04\\ 1.04\\ 1.04\\ 1.04\\ 1.04\\ 1.05\\$		
53	12/30/2018 - 12/31/2018	1.04	1.06		

\* PEAK SEASON

28-FEB-2019 15:24:23

830UPD

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**Historical Growth** 

### Fontainebleau Hotel Ballroom & Parking Garage

						19185
Station	Location	2014	2015	2016	2017	2018
0011	SR A1A/ Collins Ave, 200' S of 4700 Blk	36,500	44,000	40,500	40,000	39,000
2646	Indian Creek Dr. 200' South of 38 Street	19,000	16,000	16,000	14,000	15,000
5171	200' N 35 St (Miami Beach)	12,500	15,000	13,000	12,000	14,000
5388	SR 112/Arthur Godfrey Rd, 200' W Indian Creek Dr	34,000	39,000	36,000	41,000	34,000
	Total	102,000	114,000	105,500	107,000	102,000
	Yearly Growth		11.8%	-7.5%	1.4%	-4.7%
	Growth Trend					0.3%

Background Growth Rate

COUNTY: 87 - MIAMI-DADE

SITE: 0011 - SR A1A/COLLINS AVE, 200' S OF 4700 BLK

YEAR	AADT	DI	RECTION 1	DI	RECTION 2	*K FACTOR	D FACTOR	T FACTOR
2018	39000 C	N N	19500	 S	19500	9.00	54.30	5.50
2017	40000 C	Ν	20000	S	20000	9.00	55.00	5.30
2016	40500 C	Ν	21500	S	19000	9.00	54.50	2.80
2015	44000 C	Ν	20500	S	23500	9.00	54.70	5.20
2014	36500 C	Ν	15500	S	21000	9.00	54.50	6.10
2013	35500 C	Ν	16000	S	19500	9.00	52.40	8.30
2012	45000 C	N	23000	S	22000	9.00	55.70	3.70
2011	38500 C	Ν	19000	S	19500	9.00	55.10	3.30
2010	36500 C	N	18000	S	18500	8.98	54.08	3.30
2009	32500 C	Ν	16000	S	16500	8.99	53.24	3.30
2008	34000 C	Ν	17000	S	17000	9.09	55.75	3.60
2007	35000 C	Ν	17500	S	17500	8.01	54.34	3.00
2006	34500 C	Ν	17500	S	17000	7.97	54.22	1.70
2005	44000 C	Ν	22000	S	22000	8.80	53.80	5.90
2004	45000 C	Ν	24000	S	21000	9.00	53.30	5.90
2003	37500 C	Ν	18500	S	19000	8.80	53.40	4.70

COUNTY: 87 - MIAMI-DADE

SITE: 2646 - INDIAN CREEK DR. 200' SOUTH OF 38 STREET

YEAR	AADT	DIRECTION 1	DIRECTION 2	*K FACTOR	D FACTOR	T FACTOR
2018	15000 C	s 15000	0	9.00	99.90	5.60
2017	14000 C	S 14000	0	9.00	99.90	5.30
2016	16000 C	S 16000	0	9.00	99.90	7.80
2015	16000 C	S 16000	0	9.00	99.90	4.60
2014	19000 C	S 19000		9.00	99.90	5.10
2013	16000 C	S 16000	0	9.00	99.90	6.10
2012	15000 C	S 15000	0	9.00	99.90	8.40
2011	10500 C	S 10500	0	9.00	99.90	7.50
2010	12000 C	S 12000	0	8.98	99.99	8.80
2009	14000 C	S 14000	0	8.99	99.99	8.40
2008	13500 C	S 13500	0	9.09	99.99	5.30
2007	16500 C	S 16500	0	8.01	99.99	4.90
2006	12500 C	S 12500	в 0	7.97	99.99	2.20
2005	25500 F	S		8.80	99.90	5.50
2004	25500 C	S 25500	0	9.00	99.90	8.20
2003	18500 C	S 18500	0	8.80	99.90	4.90

COUNTY: 87 - MIAMI-DADE

SITE: 5171 - 200' N OF 35 ST. (MIAMI BEACH)

YEAR	AADT	DI	RECTION 1	DIRECTION 2	*K FACTOR	D FACTOR	T FACTOR
2018	14000 C	Ν	14000	0	9.00	99.90	5.60
2017	12000 C	Ν	12000	0	9.00	99.90	5.30
2016	13000 C	Ν	13000	0	9.00	99.90	7.80
2015	15000 C	N	15000	0	9.00	99.90	4.60
2014	12500 C	Ν	12500		9.00	99.90	5.10
2013	14000 C	N	14000	0	9.00	99.90	6.10
2012	13000 C	N	13000	0	9.00	99.90	8.40
2011	12500 C	Ν	12500	0	9.00	99.90	7.50
2010	10500 C	N	10500	0	8.98	99.99	8.80

COUNTY: 87 - MIAMI-DADE

SITE: 5388 - SR 112/ARTHUR GODFREY RD, 200' W INDIAN CREEK DR

YEAR	AADT	DIH	RECTION 1	DI	RECTION 2	*K FAG	CTOR	D FACTOR	T FACTOR
2018	34000 C	 E	16500	 W	17500		9.00	54.30	4.50
2017	41000 C	Е	18000	W	23000	(	9.00	55.00	4.00
2016	36000 C	Е	18500	W	17500	0	9.00	54.50	3.30
2015	39000 C	Е	19000	W	20000	0	9.00	54.70	4.40
2014	34000 C	Е	17000	W	17000	0	9.00	54.50	4.40
2013	41000 C	Ε	20500	W	20500	(	9.00	52.40	5.20
2012	42500 C	E	23000	W	19500	0	9.00	55.70	4.90
2011	44000 C	Ε	23000	W	21000	(	9.00	55.10	5.00
2010	38500 C	E	20500	W	18000	8	3.98	54.08	6.20
2009	37500 C	E	19000	W	18500	8	3.99	53.24	6.00
2008	36500 C	E	19000	W	17500	0	9.09	55.75	5.90
2007	39000 C	E	22000	W	17000	8	3.36	54.73	5.70
2006	36500 C	Е	21000	W	15500	8	3.70	56.15	13.70
2005	32000 C	E	17000	W	15000	8	3.50	53.00	5.50
2004	34500 C	E	18000	W	16500	8	3.70	54.00	7.00
2003	38500 C	E	20500	W	18000	8	3.50	53.40	4.20

### LRTP / TIP



### SR A1A/COLLINS AVE SIGNALIZED INTERSECTION LIGHTING

2020 Transportation Improvement Program

Project Type:	Arterial/Collector Road
MPO Project No.:	DT4401701
Type of Work:	LIGHTING
TIP Year:	2020
<b>Construction Year:</b>	2020
From:	FROM 18 ST
То:	TO 65TH ST
Agency:	FL Dept. of Transportation
Management Agency:	FDOT
Agency Project No:	4401701
Status:	
Contact Person:	
Contact Email:	
Contact Phone:	
Description:	

### Funding Information \$(thousands)

Project Phase	Funding	2019 - 2020	2020 - 2021	2021 - 2022	2022 - 2023	2023 - 2024
PRELIMINARY ENGINEERING	DIH	\$10	\$0	\$0	\$0	\$0
PRELIMINARY ENGINEERING	DS	\$0	\$0	\$0	\$0	\$0
CONSTRUCTION	ACSS	\$10	\$0	\$0	\$0	\$0
CONSTRUCTION	SA	\$5	\$0	\$0	\$0	\$0
CONSTRUCTION	DIH	\$16	\$0	\$0	\$0	\$0
PRELIMINARY ENGINEERING	HSP	\$0	\$0	\$0	\$0	\$0
CONSTRUCTION	ACSA	\$27	\$0	\$0	\$0	\$0
CONSTRUCTION	ACSS	\$304	\$0	\$0	\$0	\$0



### SR A1A/COLLINS AVE SIGNALIZED INTERSECTION LIGHTING

2020 Transportation Improvement Program

### Funding Chart \$(thousands)


# **ATTACHMENT C**

# **Capacity Analysis Worksheets**

# Existing

Number     WBL     WBR     NBT     NBR     SBL     SBT       ane Configurations     YT     YT <t< th=""><th></th><th>-</th><th>•</th><th><b>†</b></th><th>1</th><th>1</th><th>ŧ</th><th></th><th></th><th></th></t<>		-	•	<b>†</b>	1	1	ŧ			
ane Configurations     Y <thy< th="">     Y     Y</thy<>	Movement	WBL	WBR	NBT	NBR	SBL	SBT			
raffic Volume (vph) 155 291 643 0 0 1872 uture Volume (vph) 155 291 643 0 0 1872 jab Row (vphpi) 1900 1900 1900 1900 1900 total Lost time (s) 4.0 6.0 6.0 6.0 are Util. Factor 0.97 0.88 0.95 0.91 rpb, ped/bikes 1.00 1.00 1.00 1.00 rt 1.00 0.85 1.00 1.00 1.00 til Protected 0.95 1.00 1.00 1.00 total. Flow (ph) 165 41 643 0 0 1991 tron Type Prot custom NA NA NA NA totated Green, G (s) 11.6 18.6 105.4 118.4 tiffective Green, g (s) 0.10 0 1.00 toremental Delay, d1 61.9 53.4 5.2 2.7 togression Factor 1.00 1.00 toremental Delay, d2 2.5 0.1 0.2 0.4 till protective Draw till protective B KOM 2000 Volume to Capacity ratio 0.52 tutated Cycle Length (	Lane Configurations	ካካ	11	**			<b>**</b>			
uture Volume (vph) 155 291 643 0 0 1872 Jeal Row (vphpi) 1900 1900 1900 1900 1900 1900 1900 190	raffic Volume (vph)	155	291	643	0	0	1872			
iaeal Flow (vph)   1900   1900   1900   1900   1900     otal Lost time (s)   4.0   6.0   6.0   6.0     neb Util. Factor   0.97   0.88   0.95   0.91     rpb, ped/bikes   1.00   1.00   1.00   1.00     irpb, ped/bikes   1.00   1.00   1.00   1.00     irt   1.00   0.85   1.00   1.00   1.00     irt   1.00   0.85   1.00   1.00   1.00     irt Protected   0.95   1.00   1.00   1.00   1.00     irt Protected   0.95   1.00   1.00   1.00   1.00     irt Portected   0.95   1.00   1.00   1.00   1.00     irt Portected   0.95   1.00   1.00   1.00   1.00     irt Portected   0.94   0.94   0.94   0.94   0.94   0.94     ipi Flow (vph)   165   310   643   0   0   1991   0     iorn Flow (vph)   165   41   643   0   0   1991	uture Volume (vph)	155	291	643	0	0	1872			
total Lost time (s)     4.0     6.0     6.0     6.0       ane Util. Factor     0.97     0.88     0.95     0.91       pop. ped/bikes     1.00     1.00     1.00     1.00       pto, ped/bikes     1.00     1.00     1.00     1.00       th Protected     0.95     1.00     1.00     1.00       th Protected     0.95     1.00     1.00     1.00       th Cow (port)     3433     2787     3539     5085       eak-hour factor, PHF     0.94     1.00     0.94     0.94     0.94       dj. Flow (vph)     165     310     643     0     0     1991       TOR Reduction (vph)     0     269     0     0     0     1991       onfif. Peds. (#/hr)     14       1643     0     1991       um Type     Prot     custom     NA     NA     NA       rotected Phases     7     57     6     2     2       ctuated Grean, G (s)     11.6     16.	leal Flow (vphpl)	1900	1900	1900	1900	1900	1900			
ane Util. Factor 0.97 0.88 0.95 0.91 ptp. ped/bikes 1.00 1.00 1.00 1.00 1.00 pb, ped/bikes 1.00 1.00 1.00 1.00 tt 1.00 0.85 1.00 1.00 1.00 atd. Flow (prot) 3433 2787 3539 5085 tPermitted 0.95 1.00 1.00 1.00 atd. Flow (prot) 3433 2787 3539 5085 eak-hour factor, PHF 0.94 0.94 0.94 0.94 0.94 dj. Flow (vph) 165 310 643 0 0 1991 TOR Reduction (vph) 0 269 0 0 0 0 ane Group Flow (vph) 165 41 643 0 0 1991 onfl. Peds. (#/hr) 14 um Type Prot custom NA NA rotected Phases 7 57 6 2 ermitted Phases 7 57 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	otal Lost time (s)	4.0	6.0	6.0			6.0			
rpb, ped/bikes     1.00     1.00     1.00     1.00       lpb, ped/bikes     1.00     1.00     1.00     1.00       t     1.00     1.00     1.00     1.00       the protected     0.95     1.00     1.00     1.00       atd. Flow (port)     3433     2787     3539     5085       eak-hour factor, PHF     0.94     0.94     1.00     1.00       atd. Flow (perm)     3433     2787     3539     5085       eak-hour factor, PHF     0.94     0.94     0.94     0.94     0.94       di, Flow (vph)     165     310     643     0     0     1991       TOR Reduction (vph)     0     269     0     0     0     0       ane Group Flow (vph)     165     41     643     0     1991     1       offile     2.6     105.4     118.4     1     1     1       rotected Phases     7     5.7     6     2     2     1     1.0     1     1	ane Util. Factor	0.97	0.88	0.95			0.91			
hpb, ped/bikes     1.00     1.00     1.00     1.00       rt     1.00     0.85     1.00     1.00     1.00       atd. Flow (port)     3433     2787     3539     5085     5085       It Permitted     0.95     1.00     1.00     1.00     1.00       atd. Flow (port)     3433     2787     3539     5085     5085       eak-hour factor, PHF     0.94     0.94     0.94     0.94     0.94       dj. Flow (vph)     165     310     643     0     0     1991       rOmfl. Peds.(#/hr)     14     100     0.94     0.94     0.94     0.94       um Type     Prot     custom     NA     NA     NA       rotected Phases     7     57     6     2     2       remitted Phases     7     57     6     2     2       remitted Phases     7     57     0.85     3     3       retarited Phases     7     57     0.40     6.0     6.0	rpb, ped/bikes	1.00	1.00	1.00			1.00			
rt   1.00   0.85   1.00   1.00     It Protected   0.95   1.00   1.00   1.00     tad. Flow (prot)   3433   2787   3539   5085     the Permitted   0.95   1.00   1.00   1.00     tad. Flow (perm)   3433   2787   3539   5085     teak-hour factor, PHF   0.94   1.00   0.94   0.94   0.94     dj. Flow (perm)   3433   2787   3539   5085   5085     teak-hour factor, PHF   0.94   1.00   0.94   0.94   0.94   0.94     dj. Flow (vph)   165   310   643   0   0   100   1.00     ane Group Flow (vph)   165   41   643   0   0   1991   110     torottected Phases   7   57   6   2   2   116   18.6   118.4   118.4   118.4   118.4   118.4   116   18.6   10.75   0.85   116   12.6   10.5   1.0   1.0   1.0   1.0   1.0   1.0   1.0	lpb, ped/bikes	1.00	1.00	1.00			1.00			
It Protected   0.95   1.00   1.00   1.00     atd. Flow (prot)   3433   2787   3539   5085     atd. Flow (perm)   3433   2787   3539   5085     eak-hour factor, PHF   0.94   0.94   0.94   0.94   0.94     dj. Flow (vph)   165   310   643   0   0   1991     TOR Reduction (vph)   0   269   0   0   0   0     ane Group Flow (vph)   165   41   643   0   0   1991     onfl. Peds. (#/hr)   14            um Type   Prot   custom   NA   NA   NA <t< td=""><td>rt</td><td>1.00</td><td>0.85</td><td>1.00</td><td></td><td></td><td>1.00</td><td></td><td></td><td></td></t<>	rt	1.00	0.85	1.00			1.00			
Satd. Flow (prot)   3433   2787   3539   5085     It Permitted   0.95   1.00   1.00   1.00     satd. Flow (perm)   3433   2787   3539   5085     satd. Flow (perm)   3433   2787   3539   5085     seak-hour factor, PHF   0.94   1.00   0.94   0.94   0.94     dj. Flow (vph)   165   310   643   0   0   1991     Chon (vph)   165   41   643   0   0   1991     Conf. Peds. (#/hr)   14	It Protected	0.95	1.00	1.00			1.00			
iit Permitted   0.95   1.00   1.00   1.00     batd. Flow (perm)   3433   2787   3539   5085     break-hour factor, PHF   0.94   0.94   0.94   0.94   0.94     dj. Flow (vph)   165   310   643   0   0   1991     TCOR Reduction (vph)   0   269   0   0   0   0     ane Group Flow (vph)   165   41   643   0   0   1991     York   14	Satd. Flow (prot)	3433	2787	3539			5085			
Satd. Flow (perm)     3433     2787     3539     5085       Peak-hour factor, PHF     0.94     0.94     0.94     0.94     0.94     0.94       ddj. Flow (vph)     165     310     643     0     0     1991       XTOR Reduction (vph)     0     269     0     0     0     0       and Group Flow (vph)     165     41     643     0     0     1991       Confl. Peds. (#/hr)     14        Value     Value       Um Type     Prot     custom     NA     NA     NA       Protected Phases     7     5     6     2        vermited Phases     7     5     0.85         cutated Green, G (s)     11.6     18.6     105.4     118.4        cutated g/C Ratio     0.08     0.13     0.75     0.85         cutated g/C Ratio     0.05     0.01     0.18     c0.39      ///>/>/>/>/>/>/     //>/>/>/>/>/>/>/>/>/>/>/>	It Permitted	0.95	1.00	1.00			1.00			
beak-hour factor, PHF     0.94     0.94     0.94     0.94     0.94     0.94       kdj. Flow (vph)     165     310     643     0     0     1991       KTOR Reduction (vph)     0     269     0     0     0     0       ane Group Flow (vph)     165     41     643     0     0     1991       Joinfl. Peds. (#/hr)     14	Satd. Flow (perm)	3433	2787	3539			5085			
dj. Flow (vph)   165   310   643   0   0   1991     RTOR Reduction (vph)   0   269   0   0   0   0     ane Group Flow (vph)   165   41   643   0   0   1991     confl. Peds. (#/hr)   14	Peak-hour factor, PHF	0.94	0.94	1.00	0.94	0.94	0.94			
RTOR Reduction (vph)     0     269     0     0     0     0       ane Group Flow (vph)     165     41     643     0     0     1991       Confl. Peds. (#/hr)     14     14     1     1     1     1       Furn Type     Prot     custom     NA     NA     NA       Protected Phases     7     5     7     6     2       vermitted Phases	Adj. Flow (vph)	165	310	643	0	0	1991			
ane Group Flow (vph)   165   41   643   0   0   1991     confl. Peds. (#/hr)   14	RTOR Reduction (vph)	0	269	0	0	0	0			
Sonfi. Peds. (#/hr)     14       Turn Type     Prot     custom     NA     NA       Protected Phases     7     5.7     6     2       Permitted Phases      118.4     118.4       Iffective Green, g (s)     11.6     12.6     105.4     118.4       Iffective Green, g (s)     11.6     18.6     105.4     118.4       Incluated g/C Ratio     0.08     0.13     0.75     0.85       Clearance Time (s)     4.0     6.0     6.0       /ehicle Extension (s)     2.5     1.0     1.0       are Grp Cap (vph)     284     370     2664     4300       /s Ratio Prot     c0.05     0.01     0.18     c0.39       /s Ratio Prot     c0.05     0.01     0.18     c0.39       /s Ratio Prot     c0.05     0.11     0.24     0.46       /inform Delay, d1     61.9     53.4     5.2     2.7       Progression Factor     1.00     1.00     1.00     1.00       Incoremental Delay, d2     2.5<	ane Group Flow (vph)	165	41	643	0	0	1991			
Type     Prot     custom     NA     NA       Introtected Phases     7     57     6     2       termitted Phases	Confl. Peds. (#/hr)	14								
rotected Phases     7     5 7     6     2       ermitted Phases	urn Type	Prot	custom	NA			NA			
Permitted Phases     Actuated Green, G (s)   11.6   22.6   105.4   118.4     Iffective Green, g (s)   11.6   18.6   105.4   118.4     Actuated g/C Ratio   0.08   0.13   0.75   0.85     Clearance Time (s)   4.0   6.0   6.0     Vehicle Extension (s)   2.5   1.0   1.0     ane Grp Cap (vph)   284   370   2664   4300     /s Ratio Prot   c0.05   0.01   0.18   c0.39     /s Ratio Prot   c0.05   0.01   0.18   c0.39     /s Ratio Perm   /c   70   2.5   2.7     Progression Factor   1.00   1.00   1.00   1.00     Inform Delay, d1   61.9   53.4   5.2   2.7     Progression Factor   1.00   1.00   1.00   1.00     Incernental Delay, d2   2.5   0.1   0.2   0.4     belay (s)   64.4   53.5   5.4   3.1     opproach LOS   E   A   A   A     Meresection Summary   0.52	Protected Phases	7	57	6			2			
Actuated Green, G (s)   11.6   22.6   105.4   118.4     Effective Green, g (s)   11.6   18.6   105.4   118.4     Actuated g/C Ratio   0.08   0.13   0.75   0.85     Clearance Time (s)   4.0   6.0   6.0     Vehicle Extension (s)   2.5   1.0   1.0     ane Grp Cap (vph)   284   370   2664   4300     /s Ratio Prot   c0.05   0.01   0.18   c0.39     /s Ratio Perm   //s   6.0   1.00   1.00     /c Ratio   0.58   0.11   0.24   0.46     Inform Delay, d1   61.9   53.4   5.2   2.7     rogression Factor   1.00   1.00   1.00   1.00     ncemental Delay, d2   2.5   0.1   0.2   0.4     belay (s)   64.4   53.5   5.4   3.1     evel of Service   E   D   A   A     opproach LOS   E   A   A   A     McM 2000 Control Delay   11.9   HCM 2000 Level of Service   B	Permitted Phases									
Effective Green, g (s)   11.6   18.6   105.4   118.4     Actuated g/C Ratio   0.08   0.13   0.75   0.85     Clearance Time (s)   4.0   6.0   6.0     /ehicle Extension (s)   2.5   1.0   1.0     ane Grp Cap (vph)   284   370   2664   4300     /s Ratio Prot   c0.05   0.01   0.18   c0.39     /s Ratio Perm   //s Ratio   0.58   0.11   0.24   0.46     /normental Delay, d1   61.9   53.4   5.2   2.7     Progression Factor   1.00   1.00   1.00   1.00     ncremental Delay, d2   2.5   0.1   0.2   0.4     Delay (s)   64.4   53.5   5.4   3.1     evel of Service   E   D   A   A     opproach LOS   E   A   A   A     Metersection Summary   11.9   HCM 2000 Level of Service   B     ICM 2000 Volume to Capacity ratio   0.52   0.52   22.0     ICM 2000 Volume to Capacity ratio   0.52   22.0   140.0	Actuated Green, G (s)	11.6	22.6	105.4			118.4			
Instruction     0.08     0.13     0.75     0.85       Clearance Time (s)     4.0     6.0     6.0       Vehicle Extension (s)     2.5     1.0     1.0       ane Grp Cap (vph)     284     370     2664     4300       /s Ratio Prot     c0.05     0.01     0.18     c0.39       /s Ratio Perm     //     Ratio     0.58     0.11     0.24     0.46       Iniform Delay, d1     61.9     53.4     5.2     2.7     2.7       Progression Factor     1.00     1.00     1.00     1.00     1.00       ncremental Delay, d2     2.5     0.1     0.2     0.4     0.46       belay (s)     64.4     53.5     5.4     3.1     0.10     0.10       poproach Delay (s)     57.3     5.4     3.1     0.10	ffective Green, g (s)	11.6	18.6	105.4			118.4			
Clearance Time (s)     4.0     6.0     6.0       Yehicle Extension (s)     2.5     1.0     1.0       ane Grp Cap (vph)     284     370     2664     4300       /s Ratio Prot     c0.05     0.01     0.18     c0.39       /s Ratio Perm     //s Ratio Perm     //s Ratio Perm     //s Ratio Perm       /c Ratio     0.58     0.11     0.24     0.46       Iniform Delay, d1     61.9     53.4     5.2     2.7       trogression Factor     1.00     1.00     1.00     1.00       incremental Delay, d2     2.5     0.1     0.2     0.4       veleay (s)     64.4     53.5     5.4     3.1       evel of Service     E     D     A     A       pproach LOS     E     A     A     A       ICM 2000 Control Delay     11.9     HCM 2000 Level of Service     B       ICM 2000 Volume to Capacity ratio     0.52     22.0     140.0     Sum of lost time (s)     22.0       ttersection Capacity Utilization     50.3%     IC	ctuated g/C Ratio	0.08	0.13	0.75			0.85			
/ehicle Extension (s)     2.5     1.0     1.0       ane Grp Cap (vph)     284     370     2664     4300       /s Ratio Prot     c0.05     0.01     0.18     c0.39       /s Ratio Perm     //c Ratio     0.58     0.11     0.24     0.46       Jniform Delay, d1     61.9     53.4     5.2     2.7     2.7       Progression Factor     1.00     1.00     1.00     1.00     1.00       Inceremental Delay, d2     2.5     0.1     0.2     0.4     0.46       Delay (s)     64.4     53.5     5.4     3.1     2.5     0.1     0.2     0.4	Clearance Time (s)	4.0		6.0			6.0			
ane Grp Cap (vph)     284     370     2664     4300       /s Ratio Prot     c0.05     0.01     0.18     c0.39       /s Ratio Perm	ehicle Extension (s)	2.5		1.0			1.0			
/s Ratio Prot   c0.05   0.01   0.18   c0.39     /s Ratio Perm	ane Grp Cap (vph)	284	370	2664			4300			
/s Ratio Perm     /c Ratio   0.58   0.11   0.24   0.46     Iniform Delay, d1   61.9   53.4   5.2   2.7     Progression Factor   1.00   1.00   1.00   1.00     Incremental Delay, d2   2.5   0.1   0.2   0.4     Delay (s)   64.4   53.5   5.4   3.1     evel of Service   E   D   A   A     opproach Delay (s)   57.3   5.4   3.1     opproach LOS   E   A   A     Mtersection Summary   11.9   HCM 2000 Level of Service   B     ICM 2000 Control Delay   11.9   HCM 2000 Level of Service   B     ICM 2000 Volume to Capacity ratio   0.52    22.0     Actuated Cycle Length (s)   140.0   Sum of lost time (s)   22.0     ntersection Capacity Utilization   50.3%   ICU Level of Service   A	/s Ratio Prot	c0.05	0.01	0.18			c0.39			
/c Ratio     0.58     0.11     0.24     0.46       Uniform Delay, d1     61.9     53.4     5.2     2.7       Progression Factor     1.00     1.00     1.00     1.00       Incremental Delay, d2     2.5     0.1     0.2     0.4       Delay (s)     64.4     53.5     5.4     3.1       evel of Service     E     D     A     A       opproach Delay (s)     57.3     5.4     3.1       opproach LOS     E     A     A       opproach LOS     E     A     A       ICM 2000 Control Delay     11.9     HCM 2000 Level of Service     B       ICM 2000 Volume to Capacity ratio     0.52     0.52     0.52     0.53     140.0     Sum of lost time (s)     22.0       netersection Capacity Utilization     50.3%     ICU Level of Service     A     A	/s Ratio Perm									
Iniform Delay, d1     61.9     53.4     5.2     2.7       Progression Factor     1.00     1.00     1.00     1.00       Incremental Delay, d2     2.5     0.1     0.2     0.4       Delay (s)     64.4     53.5     5.4     3.1       evel of Service     E     D     A     A       opproach Delay (s)     57.3     5.4     3.1       opproach LOS     E     A     A       opproach LOS     E     A     A       Antersection Summary     11.9     HCM 2000 Level of Service     B       4CM 2000 Volume to Capacity ratio     0.52     0.52     0.52     0.52       Actuated Cycle Length (s)     140.0     Sum of lost time (s)     22.0       netersection Capacity Utilization     50.3%     ICU Level of Service     A	/c Ratio	0.58	0.11	0.24			0.46			
Progression Factor     1.00     1.00     1.00     1.00       Incremental Delay, d2     2.5     0.1     0.2     0.4       Delay (s)     64.4     53.5     5.4     3.1       evel of Service     E     D     A     A       opproach Delay (s)     57.3     5.4     3.1       opproach Delay (s)     57.3     5.4     3.1       opproach LOS     E     A     A       ntersection Summary     11.9     HCM 2000 Level of Service     B       ICM 2000 Control Delay     11.9     HCM 2000 Level of Service     B       ICM 2000 Volume to Capacity ratio     0.52     0.52     0.52       octuated Cycle Length (s)     140.0     Sum of lost time (s)     22.0       ntersection Capacity Utilization     50.3%     ICU Level of Service     A       analysis Period (min)     15     15     15     15	Jniform Delay, d1	61.9	53.4	5.2			2.7			
Incremental Delay, d2   2.5   0.1   0.2   0.4     Delay (s)   64.4   53.5   5.4   3.1     evel of Service   E   D   A   A     opproach Delay (s)   57.3   5.4   3.1     opproach Delay (s)   57.3   5.4   3.1     opproach LOS   E   A   A     Intersection Summary   11.9   HCM 2000 Level of Service   B     ICM 2000 Control Delay   11.9   HCM 2000 Level of Service   B     ICM 2000 Volume to Capacity ratio   0.52   0.52   0.52     octuated Cycle Length (s)   140.0   Sum of lost time (s)   22.0     ntersection Capacity Utilization   50.3%   ICU Level of Service   A     analysis Period (min)   15   15   0.52   0.52	Progression Factor	1.00	1.00	1.00			1.00			
Delay (s)64.453.55.43.1evel of ServiceEDAAApproach Delay (s)57.35.43.1Approach LOSEAAAntersection SummaryAAHCM 2000 Control Delay11.9HCM 2000 Level of ServiceBICM 2000 Volume to Capacity ratio0.52CActuated Cycle Length (s)140.0Sum of lost time (s)22.0Analysis Period (min)1515	ncremental Delay, d2	2.5	0.1	0.2			0.4			
evel of ServiceEDAAApproach Delay (s)57.35.43.1Approach LOSEAAAntersection SummaryAAICM 2000 Control Delay11.9HCM 2000 Level of ServiceBICM 2000 Volume to Capacity ratio0.52CActuated Cycle Length (s)140.0Sum of lost time (s)22.0Antersection Capacity Utilization50.3%ICU Level of ServiceAAnalysis Period (min)1515A	Delay (s)	64.4	53.5	5.4			3.1			
Approach Delay (s)   57.3   5.4   3.1     Approach LOS   E   A   A     Antersection Summary   Intersection Summary   Intersection Summary     ICM 2000 Control Delay   11.9   HCM 2000 Level of Service   B     ICM 2000 Volume to Capacity ratio   0.52   0.52     Actuated Cycle Length (s)   140.0   Sum of lost time (s)   22.0     Analysis Period (min)   15	evel of Service	E	D	A			A			
Approach LOS   E   A   A     Intersection Summary   Intersection Summary   Intersection Summary     ICM 2000 Control Delay   11.9   HCM 2000 Level of Service   B     ICM 2000 Volume to Capacity ratio   0.52   Intersection Capacity Utilization   Sum of lost time (s)   22.0     Intersection Capacity Utilization   50.3%   ICU Level of Service   A     Intersection Capacity Utilization   15   ICU Level of Service   A	Approach Delay (s)	57.3		5.4			3.1			
Itersection Summary     ICM 2000 Control Delay   11.9   HCM 2000 Level of Service   B     ICM 2000 Volume to Capacity ratio   0.52	pproach LUS	E		A			A			
ICM 2000 Control Delay11.9HCM 2000 Level of ServiceBICM 2000 Volume to Capacity ratio0.52Actuated Cycle Length (s)140.0Sum of lost time (s)22.0Intersection Capacity Utilization50.3%ICU Level of ServiceAICU Level of Service1515ICU Level of Service	ntersection Summary									
ICM 2000 Volume to Capacity ratio0.52Actuated Cycle Length (s)140.0Sum of lost time (s)22.0Intersection Capacity Utilization50.3%ICU Level of ServiceAAnalysis Period (min)1515A	ICM 2000 Control Delay			11.9	Н	CM 2000	Level of Service	)	В	
Actuated Cycle Length (s)140.0Sum of lost time (s)22.0Intersection Capacity Utilization50.3%ICU Level of ServiceAInalysis Period (min)1515ICU Level of Service	HCM 2000 Volume to Capacit	ty ratio		0.52						
Icu Level of Service A   Inalysis Period (min) 15	Actuated Cycle Length (s)			140.0	S	um of lost	t time (s)		22.0	
nalysis Period (min) 15	Intersection Capacity Utilization	on		50.3%	IC	CU Level o	of Service		A	
	Analysis Period (min)			15						

	4	•	1	1	1	ţ			
Lane Group	WBL	WBR	NBT	NBR	SBL	SBT	Ø5	Ø8	
Lane Configurations	ሻሻ	11	<u></u>			<b>^</b>			
Traffic Volume (vph)	155	291	643	0	0	1872			
Future Volume (vph)	155	291	643	0	0	1872			
Confl. Peds. (#/hr)	14								
Confl. Bikes (#/hr)									
Peak Hour Factor	0.94	0.94	1.00	0.94	0.94	0.94			
Growth Factor	100%	100%	100%	100%	100%	100%			
Heavy Vehicles (%)	2%	2%	2%	2%	2%	2%			
Bus Blockages (#/hr)	0	0	0	0	0	0			
Parking (#/hr)									
Mid-Block Traffic (%)	0%		0%			0%			
Shared Lane Traffic (%)									
Turn Type	Prot	custom	NA			NA			
Protected Phases	7	57	6			2	5	8	
Permitted Phases									
Detector Phase	7	57	6			2			
Switch Phase									
Minimum Initial (s)	7.0		5.0			5.0	7.0	1.0	
Minimum Split (s)	24.0		34.0			34.0	13.0	25.0	
Total Split (s)	26.0		74.0			89.0	15.0	25.0	
Total Split (%)	18.6%		52.9%			63.6%	11%	18%	
Yellow Time (s)	2.0		4.0			4.0	4.0	4.0	
All-Red Time (s)	2.0		2.0			2.0	2.0	2.0	
Lost Time Adjust (s)	0.0		0.0			0.0			
Total Lost Time (s)	4.0		6.0			6.0			
Lead/Lag	Lead		Lag				Lead	Lag	
Lead-Lag Optimize?	Yes		Yes				Yes	Yes	
Recall Mode	None		C-Max			C-Max	None	None	
Intersection Summary									
Cycle Length: 140									
Actuated Cycle Length: 140									
Offset: 131 (94%), Referenc	ed to pha	se 2:SBT	and 6:NB	T, Start o	f Green				
Natural Cycle: 100									
Control Type: Actuated-Coo	rdinated								
Solits and Phases: 1. Indi	an Crook	Drive & A	4th Street						
									_
🕈 Ø2 (R) 📕									



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Movement	WBL	WBR	NBT	NBR	SBL	SBT		
Lane Configurations	ካካ	11	**		-	***		
Traffic Volume (vph)	210	812	1161	0	0	1200		
Future Volume (vph)	210	812	1161	0	0	1200		
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900		
Total Lost time (s)	4.0	6.0	6.0			6.0		
Lane Util. Factor	0.97	0.88	0.95			0.91		
Frt	1.00	0.85	1.00			1.00		
Flt Protected	0.95	1.00	1.00			1.00		
Satd. Flow (prot)	3433	2787	3539			5085		
Flt Permitted	0.95	1.00	1.00			1.00		
Satd. Flow (perm)	3433	2787	3539			5085		
Peak-hour factor, PHF	0.94	0.94	1.00	0.94	0.94	0.94		
Adj. Flow (vph)	223	864	1161	0	0	1277		
RTOR Reduction (vph)	0	368	0	0	0	0		
Lane Group Flow (vph)	223	496	1161	0	0	1277		
Turn Type	Prot	custom	NA			NA		
Protected Phases	7	57	6			2		
Permitted Phases								
Actuated Green, G (s)	21.1	36.8	91.2			108.9		
Effective Green, g (s)	21.1	32.8	91.2			108.9		
Actuated g/C Ratio	0.15	0.23	0.65			0.78		
Clearance Time (s)	4.0		6.0			6.0		
Vehicle Extension (s)	2.5		1.0			1.0		
Lane Grp Cap (vph)	517	652	2305			3955		
v/s Ratio Prot	0.06	c0.18	c0.33			0.25		
v/s Ratio Perm								
v/c Ratio	0.43	0.76	0.50			0.32		
Uniform Delay, d1	54.0	50.0	12.7			4.6		
Progression Factor	1.00	1.00	1.00			1.00		
Incremental Delay, d2	0.4	5.0	0.8			0.2		
Delay (s)	54.4	55.0	13.4			4.8		
Level of Service	D	D	В			А		
Approach Delay (s)	54.9		13.4			4.8		
Approach LOS	D		В			А		
Intersection Summary								
HCM 2000 Control Delay			23.1	H	CM 2000	Level of Service	ce C	
HCM 2000 Volume to Capac	city ratio		0.60					
Actuated Cycle Length (s)			140.0	S	um of losi	t time (s)	22.0	
Intersection Capacity Utilizat	tion		70.5%	IC	CU Level	of Service	С	
Analysis Period (min)			15					

c Critical Lane Group

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Lane Group	WBL	WBR	NBT	NBR	SBL	SBT	Ø5	Ø8	
Lane Configurations	ሻሻ	77	<b>^</b>			<u> </u>			
Traffic Volume (vph)	210	812	1161	0	0	1200			
Future Volume (vph)	210	812	1161	0	0	1200			
Confl. Peds. (#/hr)									
Confl. Bikes (#/hr)									
Peak Hour Factor	0.94	0.94	1.00	0.94	0.94	0.94			
Growth Factor	100%	100%	100%	100%	100%	100%			
Heavy Vehicles (%)	2%	2%	2%	2%	2%	2%			
Bus Blockages (#/hr)	0	0	0	0	0	0			
Parking (#/hr)									
Mid-Block Traffic (%)	0%		0%			0%			
Shared Lane Traffic (%)									
Turn Type	Prot	custom	NA			NA			
Protected Phases	7	57	6			2	5	8	
Permitted Phases									
Detector Phase	7	57	6			2			
Switch Phase									
Minimum Initial (s)	7.0		5.0			5.0	7.0	1.0	
Minimum Split (s)	24.0		34.0			34.0	13.0	25.0	
Total Split (s)	26.0		74.0			89.0	15.0	25.0	
Total Split (%)	18.6%		52.9%			63.6%	11%	18%	
Yellow Time (s)	2.0		4.0			4.0	4.0	4.0	
All-Red Time (s)	2.0		2.0			2.0	2.0	2.0	
Lost Time Adjust (s)	0.0		0.0			0.0			
Total Lost Time (s)	4.0		6.0			6.0			
Lead/Lag	Lead		Lag				Lead	Lag	
Lead-Lag Optimize?	Yes		Yes				Yes	Yes	
Recall Mode	None		C-Max			C-Max	None	None	
Intersection Summary									
Cycle Length: 140									
Actuated Cycle Length: 140									
Offset: 87 (62%), Referenced	to phase	e 2:SBT a	nd 6:NBT	, Start of	Green				
Natural Cycle: 100									
Control Type: Actuated-Coord	dinated								
Culito and Dhaspay 1. India	n Crack		1th Ctreat						
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**Future with Project** 

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Movement	WBL	WBR	NBT	NBR	SBL	SBT		
Lane Configurations	ካካ	11	<b>*</b> *			<b>**</b> *		
Traffic Volume (vph)	157	296	634	0	0	1905		
Future Volume (vph)	157	296	634	0	0	1905		
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900		
Total Lost time (s)	4.0	6.0	6.0			6.0		
Lane Util. Factor	0.97	0.88	0.95			0.91		
Frpb, ped/bikes	1.00	1.00	1.00			1.00		
Flpb, ped/bikes	1.00	1.00	1.00			1.00		
Frt	1.00	0.85	1.00			1.00		
Flt Protected	0.95	1.00	1.00			1.00		
Satd. Flow (prot)	3433	2787	3539			5085		
Flt Permitted	0.95	1.00	1.00			1.00		
Satd. Flow (perm)	3433	2787	3539			5085		
Peak-hour factor, PHF	0.94	0.94	1.00	0,94	0,94	0.94		
Adi, Flow (vph)	167	315	634	0	0	2027		
RTOR Reduction (vph)	0	273	0	0	0	0		
ane Group Flow (vph)	167	42	634	0	0	2027		
Confl. Peds. (#/hr)	14		001	Ű	Ű	2021		
Turn Type	Prot	custom	NA			NA		
Protected Phases	7	5.7	6			2		
Permitted Phases		01	U			-		
Actuated Green G (s)	11 7	22.7	105.3			118.3		
Effective Green, a (s)	11.7	18.7	105.3			118.3		
Actuated g/C Ratio	0.08	0.13	0.75			0.84		
Clearance Time (s)	4.0	0.10	6.0			6.0		
Vehicle Extension (s)	2.5		1.0			1.0		
ane Grn Can (vnh)	286	372	2661			4296		
uls Ratio Prot	c0.05	0.02	0.18			-1230 c0.40		
/s Ratio Perm	00.00	0.02	0.10			00.40		
v/c Ratio	0 58	0 11	0 24			0.47		
Iniform Delay, d1	61.8	53.4	5.24			28		
Progression Factor	1 00	1 00	1.00			1.00		
Incremental Delay, d2	2.5	0.1	0.2			0.4		
Delay (s)	64.3	53.5	5.5			3.2		
evel of Service		00.0 D	Δ			Δ		
Approach Delay (s)	57 2	U	55			32		
Approach LOS	E		A			A		
Intersection Summary								
HCM 2000 Control Delay			11.9	Н	CM 2000	Level of Service	В	
HCM 2000 Volume to Capa	acity ratio		0.53					
Actuated Cycle Length (s)			140.0	S	um of lost	t time (s)	22.0	
Intersection Capacity Utilization	ation		51.0%	IC	U Level o	of Service	А	
Analysis Period (min)			15					
c Critical Lane Group								

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Lane Group	WBL	WBR	NBT	NBR	SBL	SBT	Ø5	Ø8	
Lane Configurations	ሻሻ	11	**			***			
Traffic Volume (vph)	157	296	634	0	0	1905			
Future Volume (vph)	157	296	634	0	0	1905			
Confl. Peds. (#/hr)	14								
Confl. Bikes (#/hr)									
Peak Hour Factor	0.94	0.94	1.00	0.94	0.94	0.94			
Growth Factor	100%	100%	100%	100%	100%	100%			
Heavy Vehicles (%)	2%	2%	2%	2%	2%	2%			
Bus Blockages (#/hr)	0	0	0	0	0	0			
Parking (#/hr)									
Mid-Block Traffic (%)	0%		0%			0%			
Shared Lane Traffic (%)									
Turn Type	Prot	custom	NA			NA			
Protected Phases	7	57	6			2	5	8	
Permitted Phases									
Detector Phase	7	57	6			2			
Switch Phase									
Minimum Initial (s)	7.0		5.0			5.0	7.0	1.0	
Minimum Split (s)	24.0		34.0			34.0	13.0	25.0	
Total Split (s)	26.0		74.0			89.0	15.0	25.0	
Total Split (%)	18.6%		52.9%			63.6%	11%	18%	
Yellow Time (s)	2.0		4.0			4.0	4.0	4.0	
All-Red Time (s)	2.0		2.0			2.0	2.0	2.0	
Lost Time Adjust (s)	0.0		0.0			0.0			
Total Lost Time (s)	4.0		6.0			6.0			
Lead/Lag	Lead		Lag				Lead	Lag	
Lead-Lag Optimize?	Yes		Yes				Yes	Yes	
Recall Mode	None		C-Max			C-Max	None	None	
Intersection Summary									
Cycle Length: 140									
Actuated Cycle Length: 140									
Offset: 131 (94%), Reference	ced to pha	se 2:SBT	and 6:NB	T, Start o	f Green				
Natural Cycle: 100									
Control Type: Actuated-Coc	ordinated								
Splits and Phases: 1. Ind	ian Creek	Drive & 4	4th Street						
		51110 Q T							
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Movement	WBL	WBR	NBT	NBR	SBL	SBT			
Lane Configurations	ካካ	77	<b>^</b>			<b>**</b> *			
Traffic Volume (vph)	231	835	1172	0	0	1198			
Future Volume (vph)	231	835	1172	0	0	1198			
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900			
Total Lost time (s)	4.0	6.0	6.0			6.0			
Lane Util. Factor	0.97	0.88	0.95			0.91			
Frt	1.00	0.85	1.00			1.00			
Flt Protected	0.95	1.00	1.00			1.00			
Satd. Flow (prot)	3433	2787	3539			5085			
Flt Permitted	0.95	1.00	1.00			1.00			
Satd. Flow (perm)	3433	2787	3539			5085			
Peak-hour factor, PHF	0.94	0.94	1.00	0.94	0.94	0.94			
Adj. Flow (vph)	246	888	1172	0	0	1274			
RTOR Reduction (vph)	0	358	0	0	0	0			
Lane Group Flow (vph)	246	530	1172	0	0	1274			
Turn Type	Prot	custom	NA			NA			
Protected Phases	7	57	6			2			
Permitted Phases									
Actuated Green, G (s)	21.7	39.1	88.9			108.3			
Effective Green, g (s)	21.7	35.1	88.9			108.3			
Actuated g/C Ratio	0.15	0.25	0.64			0.77			
Clearance Time (s)	4.0		6.0			6.0			
Vehicle Extension (s)	2.5		1.0			1.0			
Lane Grp Cap (vph)	532	698	2247			3933			
v/s Ratio Prot	0.07	c0.19	c0.33			0.25			
v/s Ratio Perm									
v/c Ratio	0.46	0.76	0.52			0.32			
Uniform Delay, d1	53.8	48.5	13.9			4.8			
Progression Factor	1.00	1.00	1.00			1.00			
Incremental Delay, d2	0.5	4.5	0.9			0.2			
Delay (s)	54.3	53.1	14.8			5.0			
Level of Service	D	D	В			А			
Approach Delay (s)	53.3		14.8			5.0			
Approach LOS	D		В			А			
Intersection Summary									
HCM 2000 Control Delay			23.5	Н	CM 2000	Level of Servi	ce	С	
HCM 2000 Volume to Capac	ity ratio		0.62						
Actuated Cycle Length (s)			140.0	S	um of lost	t time (s)		22.0	
Intersection Capacity Utilizati	ion		71.6%	IC	U Level o	of Service		С	
Analysis Period (min)			15						

c Critical Lane Group

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Lane Group	WBL	WBR	NBT	NBR	SBL	SBT	Ø5	Ø8	
Lane Configurations	ሻሻ	11	<b>^</b>			<b>^</b>			
Traffic Volume (vph)	231	835	1172	0	0	1198			
Future Volume (vph)	231	835	1172	0	0	1198			
Confl. Peds. (#/hr)									
Confl. Bikes (#/hr)									
Peak Hour Factor	0.94	0.94	1.00	0.94	0.94	0.94			
Growth Factor	100%	100%	100%	100%	100%	100%			
Heavy Vehicles (%)	2%	2%	2%	2%	2%	2%			
Bus Blockages (#/hr)	0	0	0	0	0	0			
Parking (#/hr)									
Mid-Block Traffic (%)	0%		0%			0%			
Shared Lane Traffic (%)									
Turn Type	Prot	custom	NA			NA			
Protected Phases	7	57	6			2	5	8	
Permitted Phases									
Detector Phase	7	57	6			2			
Switch Phase									
Minimum Initial (s)	7.0		5.0			5.0	7.0	1.0	
Minimum Split (s)	24.0		34.0			34.0	13.0	25.0	
Total Split (s)	26.0		74.0			89.0	15.0	25.0	
Total Split (%)	18.6%		52.9%			63.6%	11%	18%	
Yellow Time (s)	2.0		4.0			4.0	4.0	4.0	
All-Red Time (s)	2.0		2.0			2.0	2.0	2.0	
Lost Time Adjust (s)	0.0		0.0			0.0			
Total Lost Time (s)	4.0		6.0			6.0			
Lead/Lag	Lead		Lag				Lead	Lag	
Lead-Lag Optimize?	Yes		Yes				Yes	Yes	
Recall Mode	None		C-Max			C-Max	None	None	
Intersection Summary									
Cycle Length: 140									
Actuated Cycle Length: 140									
Offset: 87 (62%), Referenced	l to phase	e 2:SBT a	nd 6:NBT	, Start of	Green				
Natural Cycle: 100									
Control Type: Actuated-Coord	dinated								
Solits and Phases: 1. India	n Creek	Drive & 4	4th Street						
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# **ATTACHMENT D**

**Trip Generation** 

#### Glimmer Usage Report for 2018

Function Room	Start Date	Event Name	Gtd Attn.	Event Classification
Glimmer Ballroom	01/04/18	Textron Global Leadership Meeting	325	Plated Dinner
Glimmer Ballroom	01/05/18	Textron Global Leadership Meeting	300	General Session
Glimmer Ballroom	01/09/18	2018 WinField United Ultimate Field Trip	1200	Lunch Buffet
Glimmer Ballroom	01/10/18	2018 WinField United Ultimate Field Trip	1200	Lunch Buffet
Glimmer Ballroom	01/11/18	2018 WinField United Ultimate Field Trip	1150	Lunch Buffet
Glimmer Ballroom	01/12/18	2018 WinField United Ultimate Field Trip	1000	Breakfast Buffet
Glimmer Ballroom	01/17/18	NATPE Market & Conference 2018	350	General Session
Glimmer Ballroom	01/26/18	2018 WinField United Catalyst Conference	400	Reception
Glimmer Ballroom	02/01/18	Context Summits Miami 2018	1200	Lunch Buffet
Glimmer Ballroom	02/02/18	UISCA 2018 Annual Meeting	430	Plated Dinner
Glimmer Ballroom	02/09/18	Antiv Retreat	215	General Session
Glimmer Ballroom	02/21/18	AppDynamics 2018 SKO	775	Lunch Buffet
Glimmer Ballroom	02/23/18	2018 McDermott Partners' Meeting	555	Plated Lunch
Glimmer Ballroom	02/27/18	Staffing Industry Analysts Executive Forum	1000	General Session
Glimmer Ballroom	02/28/18	Staffing Industry Analysts Executive Forum	1000	General Session
Glimmer Ballroom	03/01/18	Staffing Industry Analysts Executive Forum	700	General Session
Glimmer Ballroom	03/03/18	2018 LoanDepot	260	Meeting/Session
Glimmer Ballroom	03/05/18	McDermott Will & Emery 2018 HPE Symposium	400	Meeting
Glimmer Ballroom	03/06/18	McDermott Will & Emery 2018 HPE Symposium	400	Meeting
Glimmer Ballroom	03/08/18	Credit Suisse Equity Trading Forum 2018	375	Plated Dinner
Glimmer Ballroom	03/09/18	Credit Suisse Equity Trading Forum 2018	315	General Session
Glimmer Ballroom	03/16/18	Big Smoke	700	General Session
Glimmer Ballroom	03/26/18	Spring Alliance POA	3/5	General Session
Climmer Ballroom	04/03/18	VOLVO - Customer Service Program	695	Luiicii Builet
Glimmer Ballroom	04/04/18		1100	Lunch Buffet
Glimmer Ballroom	04/18/18	FICO World 2018	1100	Lunch Buffet
Glimmer Ballroom	04/19/18	FICO World 2018	900	Continental Breakfast
Glimmer Ballroom	04/21/18	The Cushman School Gala	375	Plated Dinner
Glimmer Ballroom	04/28/18	Performance Excellence Awards	750	Cocktail Reception
Glimmer Ballroom	04/30/18	LAC	180	Lunch Buffet
Glimmer Ballroom	05/01/18	2018 Global Sales Conference	640	Lunch Buffet
Glimmer Ballroom	05/02/18	2018 Global Sales Conference	660	Lunch Buffet
Glimmer Ballroom	05/10/18	International Factoring Association	600	Meeting
Glimmer Ballroom	05/11/18	International Factoring Association	400	Meeting
Glimmer Ballroom	05/22/18	2018 Chairman's Circle	570	Heavy Reception
Glimmer Ballroom	05/23/18	2018 Chairman's Circle	570	Lunch Buffet
Glimmer Ballroom	05/24/18	2018 Chairman's Circle	525	Lunch Buffet
Glimmer Ballroom	06/19/18	Vista Consulting Group - 2018 BPSS Product & Tech Leadership	400	General Session
Glimmer Ballroom	06/20/18	Vista Consulting Group - 2018 BPSS Product & Tech Leadership	375	General Session
Glimmer Ballroom	06/21/18		290	General Session
Glimmer Ballroom	06/25/18	CEMA 2018 Annual Conference	950	Conoral Socian
Glimmer Ballroom	06/27/18	CEMA 2018 Annual Conference	950	General Session
Glimmer Ballroom	06/28/18		400	Plated Dinner
Glimmer Ballroom	06/30/18	National Association of Chanter 13 Trustees	500	Heavy Reception
Glimmer Ballroom	07/15/18	South Atlantic & Gulf District II A	650	Heavy Reception
Glimmer Ballroom	07/16/18	South Atlantic & Gulf District ILA	600	Beverage Service
Glimmer Ballroom	07/17/18	South Atlantic & Gulf District ILA	600	General Session
Glimmer Ballroom	07/18/18	South Atlantic & Gulf District ILA	1000	Plated Dinner
Glimmer Ballroom	07/19/18	South Atlantic & Gulf District ILA	600	Beverage Service
Glimmer Ballroom	07/24/18	ONC Regional Mtg East/Central	200	General Session
Glimmer Ballroom	07/25/18	ONC Regional Mtg East/Central	200	General Session
Glimmer Ballroom	07/26/18	ONC Regional Mtg East/Central	200	General Session
Glimmer Ballroom	08/04/18	GGT 2018	300	Beverage Service
Glimmer Ballroom	09/18/18	CrowdStrike 2018 FalCon	700	Lunch Buffet
Glimmer Ballroom	09/19/18	CrowdStrike 2018 FalCon	650	Lunch Buffet
Glimmer Ballroom	10/01/18	TeamMate User Forum 2018	740	Heavy Reception
Glimmer Ballroom	10/02/18	TeamMate User Forum 2018	675	Lunch Buffet
Climmer Ballroom	10/03/18	Cushman & Wakafield 2019 TAC Conference	200	Conoral Socian
Glimmer Ballroom	10/04/18	TITLE Boxing Club 2018 Convention	320	General Session
Glimmer Ballroom	10/00/18	TITLE Boxing Club 2018 Convention	320	General Session
Glimmer Ballroom	10/16/18	CITI National Expo 2018	300	General Session
Glimmer Ballroom	10/17/18	CITI National Expo 2018	300	General Session
Glimmer Ballroom	10/18/18	CITI National Expo 2018	300	General Session
Glimmer Ballroom	10/23/18	CCH Connections	925	Lunch Buffet
Glimmer Ballroom	10/24/18	CCH Connections	900	Breakfast Buffet
Glimmer Ballroom	10/25/18	Bauer World 2018	425	Heavy Reception
Glimmer Ballroom	10/29/18	Guy Carpenter	250	Continuous Beverage Service

#### Glimmer Usage Report for 2018

Function Room	Start Date	Event Name	Gtd Attn.	Event Classification
Glimmer Ballroom	10/30/18	Guy Carpenter	250	Breakfast Buffet
Glimmer Ballroom	11/01/18	SPECTRUM 2018	240	General Session
Glimmer Ballroom	11/02/18	SPECTRUM 2018	240	General Session
Glimmer Ballroom	11/03/18	SPECTRUM 2018	240	General Session
Glimmer Ballroom	11/04/18	SPECTRUM 2018	240	General Session
Glimmer Ballroom	11/06/18	Hewlett Packard Enterprise FastStart 2019	381	Beverage Service
Glimmer Ballroom	11/07/18	Hewlett Packard Enterprise FastStart 2019	381	General Session
Glimmer Ballroom	11/09/18	2018 Phonak Marvel Launch Event	500	Lunch Buffet
Glimmer Ballroom	11/10/18	2018 Phonak Marvel Launch Event	500	Breakfast Buffet
Glimmer Ballroom	11/12/18	Clinique North America Regional Meeting	160	Reception
Glimmer Ballroom	11/13/18	Clinique North America Regional Meeting	200	Dinner Buffet
Glimmer Ballroom	11/14/18	Clinique North America Regional Meeting	200	Breakfast Buffet
Glimmer Ballroom	11/26/18	Limitless Mastercard LAC Innovation Forum 2018	150	Meeting
Glimmer Ballroom	12/03/18	Distech Connect 2018	450	Beverage Service
Glimmer Ballroom	12/04/18	Distech Connect 2018	425	Plated Dinner
Glimmer Ballroom	12/05/18	Distech Connect 2018	450	General Session
Glimmer Ballroom	12/07/18	ALTS Capital Publishing, Inc.	215	Meeting
Glimmer Ballroom	12/10/18	Global Financial Reporting and Valuation Conference 2018	325	General Session
Glimmer Ballroom	12/11/18	Global Financial Reporting and Valuation Conference 2018	325	General Session
Glimmer Ballroom	12/14/18	Alcora Corporation Holiday Party	450	Dinner Buffet
Glimmer Ballroom	12/16/18	2018 IEEE Conference of Decision and Control (CDC)	950	Reception
Glimmer Ballroom	12/18/18	2018 IEEE Conference of Decision and Control (CDC)	288	Cocktail Reception
		93	49570	total attendees/year for Glimmer
			533	avg.# attendess/event (93)

Glimmer Ballroom = 18,786 s.f. =

35.2451 s.f. per attendee (per event)

Fontainebleau Banquet Summary 2016 - 2018

	<u>2016</u>	<u>2017</u>	<u>2018</u>	<u>Total</u>	<u>%</u>
Total Banquet Covers					
Local Events	10,945	7,219	8,324	26,488	3.3%
Group In-House	275,346	218,081	283,586	777,013	96.7%
Total	286,291	225,300	291,910	803,501	100.0%

#### FONTAINEBLEAU MIAMI BEACH

#### F&B Summary 2018

Time: December

## **F&B BY OUTLET**

			Month to Date			Year to Date						
	Actual	Budget	Prior Year	Var + (-)	%	Actual	Budget	Prior Year	Var + (-)	%		
F&B SUMMARY												
Food Revenue					15.9 %					-7.4 %		
Beverage Revenue					9.4 %					-5.3 %		
Other F&B Revenue					28.3 %					4.9 %		
Total Revenue					13.5 %					-5.6 %		
Covers/Checks	180,846	185,859	163,458	-5,013	-2.7 %	2,063,622	2,167,285	1,888,060	-103,663	-4.8 %		
Avg. Food Cvr/Chk					19.2 %					-2.7 %		
Avg. Beverage Cvr/Chk					12.4 %					-0.5 %		
Avg. Total Cvr/Chk					16.6 %					-0.9 %		
Cost of Sales - Food					3.8 %					-7.6 %		
Cost of Sales - Beverage					6.9 %					-1.4 %		
Cost of Sales - Other					-40.6 %					9.9 %		
Cost of Sales					3.6 %					-5.1 %		
Cost of Food %					-10.5 %					-0.2 %		
Cost of Beverage %					-2.3 %					4.1 %		
Cost of Other %					-53.7 %					4.7 %		
Total Payroll, Taxes & Benefits					22.0 %					-2.3 %		
Other Operating Expenses					36.0 %					5.1 %		
Total Expenses					22.2 %					-0.5 %		
Profit					- <b>3.8</b> %					-13.8 %		
Margin												

#### <u>StripSteak</u>

Food Revenue					-16.9 %					-3.0 %
Beverage Revenue					-17.8 %					-10.9 %
Other F&B Revenue					87.8 %					-0.6 %
Total Revenue					-16.3 %					-5.7 %
Covers	6,707	8,500	6,936	-1,793	-21.1 %	73,551	80,003	71,085	-6,452	-8.1 %
Avg. Food Cover					5.3 %					5.5 %
Avg. Beverage Cover					4.2 %					-3.1 %
Avg. Total Cover					6.0 %					2.6 %
Cost of Sales - Food					-15.6 %					-5.4 %
Cost of Sales - Beverage					-12.6 %					-11.7 %
Cost of Sales - Other					-100.0					-23.8 %
Cost of Sales					-15.5 %					-7.2 %
Cost of Food %					1.6 %					-2.5 %
Cost of Beverage %					6.3 %					-0.9 %
Cost of Other %					-100.0					-23.3 %
Total Payroll, Taxes & Benefit					6.9 %					-7.4 %
Other Operating Expenses					5.9 %					1.0 %
Total Expenses					-2.5 %					-5.5 %
Profit					-67.0 %					-6.5 %
Margin										

#### Hakkasan

<u>nakkasali</u>					
Food Revenue					-4.7 %
Beverage Revenue					-6.4 %
Other F&B Revenue					770.7 %
Total Revenue					-4.1 %
Covers	9,363	9,521	9,116	-158	-1.7 %
Avg. Food Cover					-3.1 %
Avg. Beverage Cover					-4.8 %

				-10.4 %
				-10.8 %
				117.3 %
				-10.4 %
90,666	99,402	88,871	-8,736	-8.8 %
				-1.8 %
				-2.3 %