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DESIGN FOR ALUMINUM RAILING

FOR

**18-29 851 MERIDIAN AVE, MIAMI
BEACH, FL**



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ALUMINUM RAILING DESIGN

STRUCTURAL CALCULATIONS

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1.) MATERIALS

1.a) Members: Aluminum Alloy 6061-T6

Reference: Aluminum Design
Manual 2005 Edition Table 2-22
6061 - T6

Allowable Stress for components:

Bending:

-Round or oval tubes:

$F_b = 24000 \text{ psi}$ Unwelded Metal

$F_b = 10500 \text{ psi}$ Welded Metal

-Symetric Shapes:

$F_b = 19000 \text{ psi}$ Unwelded Metal

$F_b = 12000 \text{ psi}$ Welded Metal

Shear

$F_s = 12000 \text{ psi}$ Unwelded Metal

$F_s = 5000 \text{ psi}$ Welded Metal

Elasticity Modulus $E = 10100 \text{ Ksi}$

1.b) Welding: Aluminum Filler Alloy 5356

Allowable Stress for Welding:

$F_w = 7000 \text{ psi}$

2.) DESIGN INFORMATION

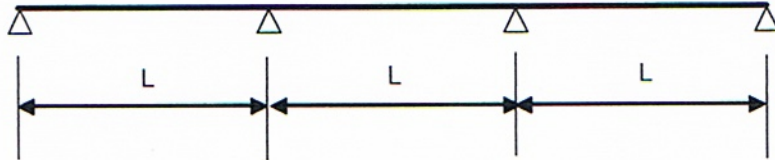
- Florida Building Code 2014
- Aluminum Design Manual, 2005
- Minimum Design Loads for Building and Others Structures, ASCE 7- 10

3.) DESIGN LOADS

- Handrail Design Loads: (FBC 2014)
 - Concentrated Load = 200 lbs applied at any point in any direction.
 - Uniform Load = 50 plf applied in any direction
- Guardrail System Loads: (FBC 2014)
 - Uniform Hor. Load= 25 psf over the gross area of the guard, including the area of any openings in the guard.

4.) HANDRAIL DESIGN

Consider three equal continuous Span $L_w := 4\text{ ft}$ (Maximum Span)



4.a) Maximum Moment:

Concentrated Load $P := 200\text{ lb}$

$$M_{pmax} := \frac{P \cdot L}{5} \quad \boxed{M_{pmax} = 160\text{ ft}\cdot\text{lb}}$$

Uniform Load $\omega := 50\text{ plf}$

$$M_{\omega max} := 0.1012 \omega \cdot L^2 \quad \boxed{M_{\omega max} = 80.96\text{ ft}\cdot\text{lb}}$$

$$M_{max} := \max(M_{pmax}, M_{\omega max}) \quad \boxed{M_{max} = 160\text{ ft}\cdot\text{lb}}$$

4.b) Maximum Shear:

Concentrated Load $P := 200\text{ lb}$

$$V_{pmax} := P \quad \boxed{V_{pmax} = 200\text{ lb}}$$

Uniform Load $\omega := 50\text{ plf}$

$$V_{\omega max} := 0.6 \omega \cdot L \quad \boxed{V_{\omega max} = 120\text{ lb}}$$

$$V_{max} := \max(V_{pmax}, V_{\omega max}) \quad \boxed{V_{max} = 200\text{ lb}}$$

4.c) Section Required:

Bending Design: $F_b := 12000 \cdot \text{psi}$

Section Modulus Required:

$$S_{hr} := \frac{M_{\max}}{F_b} \quad \boxed{S_{hr} = 0.16 \cdot \text{in}^3}$$

Shear Design: $F_s := 5000 \cdot \text{psi}$

Section Modulus Required:

$$A_{hr} := \frac{1.5V_{\max}}{F_s} \quad \boxed{A_{hr} = 0.06 \cdot \text{in}^2}$$

4.d) Section Provided:

ALUMINUM DIXIE CAP 2 5/8"

Section Provided:

$$S_{\text{prov}} := 0.39 \cdot \text{in}^3 \quad S_{\text{prov}} = 0.39 \cdot \text{in}^3$$

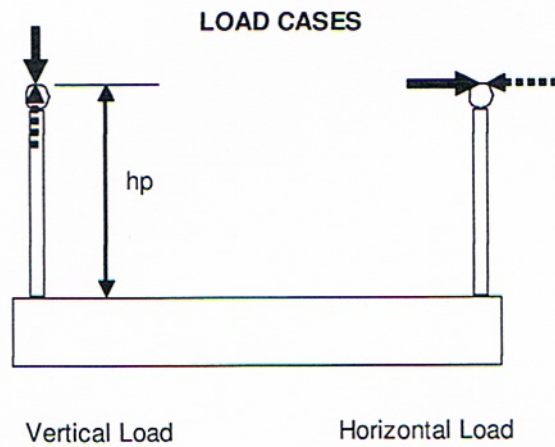
$$A_{\text{prov}} := 0.834 \cdot \text{in}^2 \quad A_{\text{prov}} = 0.83 \cdot \text{in}^2$$

Control := if (Shr > Sprov, "NOT O.K.", "O.K.") Control = "O.K."

~~Control~~ := if (Ahr > Apro, "NOT O.K.", "O.K.") Control = "O.K."

USE ALUMINUM DIXIE CAP 2 5/8"

5.) POST DESIGN



5.a) Maximum Reaction

Concentrated Load $R_{pmax} := P$ $R_{pmax} = 200 \text{ lb}$

Uniform Load $R_{\omega max} := \omega \cdot L$ $R_{\omega max} = 200 \text{ lb}$

$R_{max} := \text{if}(R_{pmax} > R_{\omega max}, R_{pmax}, R_{\omega max})$ $R_{max} = 200 \text{ lb}$

5.b) Maximum Moment

$h_p := 42 \cdot \text{in}$

$M_{post} := R_{max} \cdot h_p$ $M_{post} = 8400 \text{ lb} \cdot \text{in}$

5.c) Maximum Shear

$V_{post} := R_{max}$ $V_{post} = 200 \text{ lb}$

5.d Section Required:

Bending:

$$F_b := 12000 \cdot \text{psi}$$

$$F_v := 5000 \cdot \text{psi}$$

$$S_{\text{postreq}} := \frac{M_{\text{post}}}{F_b}$$

$$S_{\text{postreq}} = 0.7 \cdot \text{in}^3$$

Shear:

$$A_{\text{postreq}} := 1.5 \frac{V_{\text{post}}}{F_v}$$

$$A_{\text{postreq}} = 0.06 \cdot \text{in}^2$$

5.d Section Provided:

Square Tube Section $b := 2 \cdot \text{in}$ $t := \frac{1}{4} \cdot \text{in}$

Square Section Tube exterior $L := 2 \cdot \text{in}$ $tw := \frac{1}{4} \cdot \text{in}$

$$I_{\text{pt}} := \frac{1}{12} [t^4 - (t - 2tw)^4] \quad I_{\text{pt}} = 0.911 \quad \text{in}^4$$

$$S_{\text{pt}} := \frac{I_{\text{pt}}}{\frac{t}{2}} \quad S_{\text{pt}} = 0.911 \quad \text{in}^3$$

$$A_{\text{pt}} := t^2 - (t - 2 \cdot tw)^2 \quad A_{\text{pt}} = 1.75 \quad \text{in}^2$$

$$A_{\text{ptw}} := 2 \cdot t \cdot tw \quad A_{\text{ptw}} = 1 \quad \text{in}^2$$

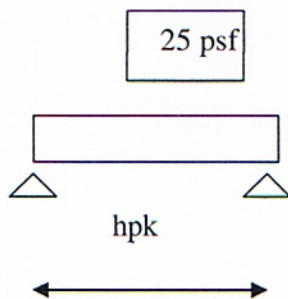
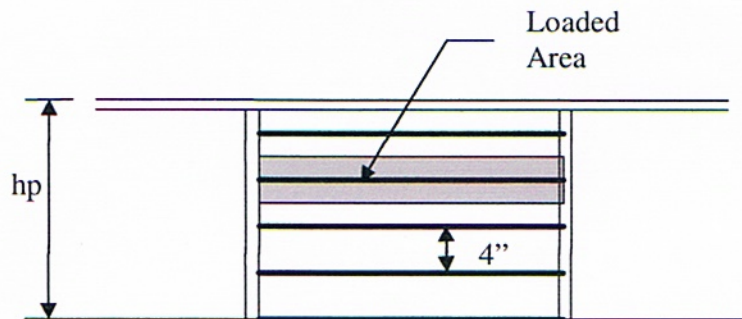
$$S_{\text{prov}} = 0.75 \text{ in}^3 \quad A_{\text{prov}} = 0.75 \text{ in}^2$$

USE 2" x 2" x 1/4" Aluminum Tube

6.) PICKET DESIGN:

$$hpk := 48 \cdot \text{in}$$

$$hpk = 48 \cdot \text{in}$$



$$\text{psf} := \frac{\text{lb}}{\text{ft}^2}$$

$$w := 25 \cdot \text{psf} \cdot 4.75 \cdot \text{in} \quad w = 0.82 \cdot \frac{\text{lb}}{\text{in}}$$

$$M_{\text{maxpk}} := \frac{1}{8} \cdot w \cdot hpk^2$$

$$M_{\text{maxpk}} = 237.5 \cdot \text{lb} \cdot \text{in}$$

$$V_{\text{maxpk}} := \frac{w \cdot hpk}{2}$$

$$V_{\text{maxpk}} = 19.79 \cdot \text{lb}$$

Section Required:

Bending Design: $F_b := 12000 \cdot \text{psi}$ $F_v := 5000 \cdot \text{psi}$

Section Modulus Required: $\frac{\text{psi}}{\text{in}^2} := \frac{\text{lb}}{\text{in}^2}$

$S_{pkreq} := \frac{M_{maxpk}}{F_b}$ $S_{pkreq} = 0.02 \cdot \text{in}^3$

Shear Design:

Area Required:

$A_{pkreq} := \frac{1.5 \cdot V_{maxpk}}{F_v}$ $A_{pkreq} = 0.006 \cdot \text{in}^2$

Section Provided:

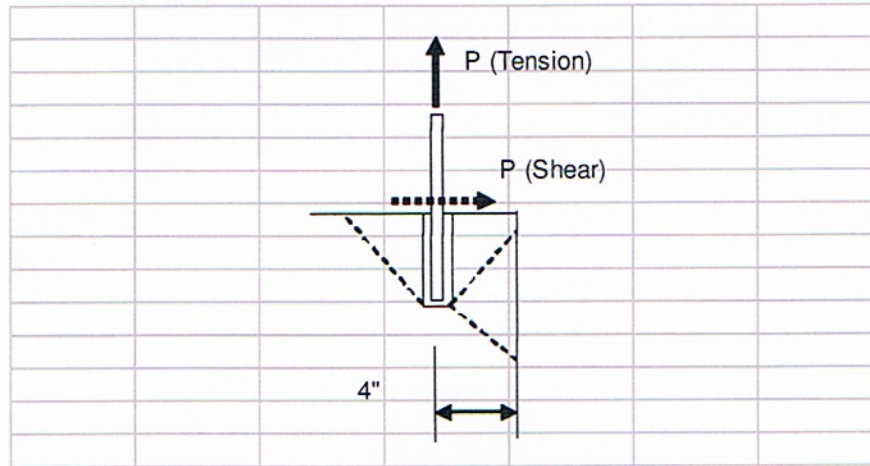
ALUMINUM TUBE 1"X2"X1/8" ALUMINUM TUBE

$S_{pt} = 0.114 \text{ in}^3$ $A_{pt} = 0.312 \text{ in}^2$

USE ALUMINUM TUBE PICKET 1"X2"X1/8"

7.) ANCHORAGE, WELDING AND CONNECTIONS.

7.a) POST ANCHORAGE TO CONCRETE



Concrete Strength: $f_c := 3000\text{-psi}$

Minimum Embedment: $emb := 4\text{-in}$

Hole Diameter: $hd := 2\text{-in}$

Post Height: $h_p := 42\text{-in}$

Horizontal or Vertical Load: $P := 200\text{-lb}$

Minimum Edge Distance: $dedge := 4\text{-in}$

a) Concrete Breakout (Tension)

$$A_{No} := 9 \cdot emb^2 \quad A_{No} = 144 \cdot in^2$$

$$A_N := 3 \cdot emb \cdot (1.5 \cdot emb + dedge) \quad A_N = 120 \cdot in^2$$

$$A_{Nfinal} := \min(A_{No}, A_N) \quad A_{Nfinal} = 120 \cdot in^2$$

$$\psi_2 := \text{if} \left(dedge < 1.5 \cdot emb, 0.7 + 0.3 \cdot \frac{dedge}{1.5 \cdot emb}, 1 \right) \quad \psi_2 = 0.9$$

$$\psi_3 := 1.4$$

$$N_b := 17 \text{lb} \cdot in^{.5} \cdot in^{-0.5} \cdot \sqrt{f_c} \cdot emb^{1.5} \quad N_b = 7449.03 \text{ lb}$$

$$N_{cb} := \frac{A_{Nfinal}}{A_{No}} \cdot \psi_2 \cdot \psi_3 \cdot N_b$$

$$N_{cb} = 7821.48 \text{ lb}$$

$$P_u := 1.6 \cdot P$$

$$P_u = 320 \text{ lb}$$

$$\phi := 0.75$$

$$\phi N_{cb} := \phi \cdot N_{cb}$$

$$\phi N_{cb} = 5866 \text{ lb}$$

$$\text{Control} := \text{if}(P_u > \phi \cdot N_{cb}, \text{"NOT O.K."}, \text{"O.K."})$$

$$\text{Control} = \text{"O.K."}$$

b) Pullout Strength of Anchor in Tension

$$\text{Weld Size } \underset{\sim}{w}_t := \frac{1}{8} \cdot \text{in} \quad \underset{\sim}{f}_c := 3000 \cdot \text{psi}$$

$$\underset{\sim}{b}_w := 2 \cdot \text{in} \quad \text{Effective Weld Size } t_{eff} := 0.707 \cdot t \quad t_{eff} = 0.09 \cdot \text{in}$$

$$A_{brg} := 4 \cdot b \cdot t_{eff} \quad A_{brg} = 0.71 \cdot \text{in}^2 \quad \psi_4 := 1.4$$

$$N_{pn} := \psi_4 \cdot A_{brg} \cdot 8 \cdot f_c \quad N_{pn} = 23755.2 \text{ lb}$$

$$\text{Control} := \text{if}(P_u > \phi \cdot N_{pn}, \text{"NOT O.K."}, \text{"O.K."})$$

$$\text{Control} = \text{"O.K."}$$

b) Concrete Breakout (Shear)

$$\text{Bolt Diameter: } d_o := 2.0 \cdot \text{in}$$

$$A_{Vo} := 4.5 \cdot d_{edge}^2$$

$$A_{Vo} = 72 \cdot \text{in}^2$$

$$A_V := A_{Vo}$$

$$A_V = 72 \cdot \text{in}^2$$

Assume Depth of Support > 1.5d_{edge}

$$\psi_6 := 1 \quad \psi_7 := 1.4$$

$$l_o := \min(\text{emb}, 8 \cdot d_o) \quad l_o = 4 \cdot \text{in}$$

$$V_b := 7 \cdot \text{lb}^{0.5} \cdot \text{in}^{-1} \cdot \left[\left(\frac{l_o}{d_o} \right)^{0.2} \cdot \sqrt{d_o} \cdot \sqrt{f_c} \cdot d_{edge}^{1.5} \right] \quad V_b = 4982.76 \text{ lb}$$

$$V_{cb} := \frac{A_V}{A_{Vo}} \cdot \psi_6 \cdot \psi_7 \cdot V_b$$

$$V_{cb} = 6975.86 \text{ lb}$$

$$V_u := 1.6 \cdot P$$

$$V_u = 320 \text{ lb}$$

$$\underset{\sim}{\phi} := 0.75$$

$$\text{Control} := \text{if}(V_u > \underset{\sim}{\phi} \cdot V_{cb}, \text{"NOT O.K."}, \text{"O.K."})$$

$$\text{Control} = \text{"O.K."}$$

USE 3" HOLE DIAMETER. 4" MIN. EDGE DISTANCE AND 4" MIN. EMB.
USE 1/8" WELD SIZE AROUND BOTTOM END OF POST.

7.b) POST - BOTTOM RAILING CONNECTION

Try 1/8" Weld Aluminum Filler Alloy 5356

$F_w := 7000 \cdot \text{psi}$

$$\text{Effective Width} = \frac{1}{8} \cdot 0.707 \text{ in} = 0.09 \cdot \text{in}$$

$$\text{Area of Welding} \quad A_w := \left(2 \cdot \frac{7}{8} \cdot \text{in} + 1.75 \cdot \text{in} \right) \cdot 0.088 \cdot \text{in} \quad A_w = 0.308 \cdot \text{in}^2$$

$$\text{Allowable Shear} \quad V_{\text{allow}} := A_w \cdot F_w \quad V_{\text{allow}} = 2156 \text{ lb} \quad > 200 \text{ lb O.K.}$$

USE 1/8" WELD SIZE ALUMINUM FILLER ALLOY 5356